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# Current understanding of cellulose ethers impact on the hydration of $C_3A$ and $C_3A$ -sulphate systems

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#### ABSTRACT

The impact of cellulose ethers (CE) on  $C_3A$  hydration was examined to support the understanding of the retarding effect of CE on cement hydration. In this sense, we successively studied the CE adsorption on ettringite and calcium hydroaluminates, and then the CE influence during  $C_3A$  hydration in presence or absence of calcium sulphate. We emphasized a phase-specific adsorption of CE depending on CE chemistry. Besides, in addition of CE, we highlighted a gradual slowing down of  $C_3A$  dissolution as well as ettringite and calcium hydroaluminates precipitation. Again, a great impact of CE chemistry and CE adsorption behaviour were noticed. Thus, HECs induce always a stronger adsorption on calcium hydroaluminates and a longer C3A hydration delays than HPMCs.

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### 1. Introduction

Cellulose ethers (CE) are commonly introduced into factory-made mortar formulations in order to induce a substantial increase of water retention capacity as well as to improve the workability of fresh material as well as the adherence to the substrate. Hence, these molecules contribute to good mechanical strength of the hardened material. However, as a side effect, CE may also induce a more or less important slowing down of cement hydration. Preliminary studies highlight that there was no significant degradation of CE [1]. Therefore, the mechanism of hydration delay induced by CE cannot be explained thanks to the impact of hydroxy carboxylic acids generated during their alkaline degradation. Moreover, recent insights emphasize a great influence of CE during C<sub>3</sub>S hydration [2]. Firstly, it seems that the influence of CE on C<sub>3</sub>S dissolution kinetic was quite negligible. All things considered, it was assumed that CE strongly act on C-S-H precipitation by means of: a decrease of the amount of initial C-S-H nuclei, a delay in order to obtain a continuous C-S-H shell around the C<sub>3</sub>S grain, and finally a formation of a thicker and more permeable C-S-H layer.

The tricalcium aluminate  $(C_3A)$  is one of the most reactive major components of clinker.  $C_3A$  strongly reacts with water to form calcium hydroaluminates (*i.e.* Afm-type phase and the more thermodynamically stable hydrogarnet), whereas addition of calcium sulphate leads to the precipitation of ettringite with a slower rate. On further examination, the presence of sulphates allows to regulate the kinetics

Thus, this paper is devoted to determine the influence of CE chemistry on the kinetics and mechanism of  $C_3A$  hydration. We studied increasing complexity mineral systems (pure  $C_3A$  admixed or not, and then  $C_3A$ -sulphate system admixed or not) in order to bring original experimental data as well as to support a sound knowledge on  $CE-C_3A$  interactions. In this context, to follow an analytic approach, we successively examined the CE adsorption on ettringite and calcium hydroaluminates, as well as the influence of CE during  $C_3A$  hydration in different systems.

### 2. Materials and methods

### 2.1. Mineral compounds

The investigated mineral compounds were supplied by Lafarge and Italcementi companies. The pure anhydrous or hydrated phases were prepared at laboratory scale, with the help of industrial partners. C<sub>3</sub>A

of  $C_3A$  hydration to avoid the "flash-setting" of cement. Thus, the reactivity of  $C_3A$ -sulphate system appears crucial so as to control and predict the workability of fresh cement material. But mechanisms and parameters controlling the reactivity of  $C_3A$  hydration are not yet fully elucidated, even if recent work significantly improve our knowledge on this topic [3,4]. Besides, very few studies dealt with the hydration behaviour of  $C_3A$  in presence of CE. Using soft X-ray transmission microscopy, Silva underlined that CE may slightly affect the aspect of  $C_3A$  hydration [5]. It was observed that the single CE molecule studied lead to retard the kinetics of  $C_3A$  hydration from the few minutes after mixing. However, Silva does not succeed from these microscopic images to state whether the delay is mainly caused by CE adsorption onto cementitious grains, by slowing down ionic diffusion or by chemical interactions.

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**Table 1**Molecular parameters of the selected cellulose ethers.

Admixtures	M <sub>w</sub> (Dalton)	OC <sub>2</sub> H <sub>4</sub> OH (%)	OC <sub>3</sub> H <sub>6</sub> OH (%)	OCH <sub>3</sub> (%)	DS	MS
HPMC U2	955,000	_	10.65	27.5	1.82	0.29
HPMC P1	175,000	-	19	27.5	1.95	0.56
HEC H1	175,000	48.5	-	-	-	2
HEC N1	175,000	56	-	-	-	2.5
HEC N7	1,335,000	56	-	-	-	2.5

was obtained by burning the appropriate amount of calcium carbonate and alumina, whereas the ettringite was synthesized from calcium oxide and aluminium sulphate 16-hydrate. Several characterisations were carried out in order to quantify the phase assemblage of the investigated mineral systems. X-ray diffraction (XRD) analysis (Siemens, D 5000, Germany) allowed to quantify the phase composition by means of Rietveld method (Siroquant V2.5 software).

### 2.2. Organic products

Among the wide variety of existing CE, three types are mainly used in mortar manufacturing: hydroxypropylmethyl cellulose (HPMC), hydroxyethylmethyl cellulose (HEMC) and hydroxyethyl cellulose (HEC). The chemical structure of HEC is entirely determined by two parameters *i.e.* the molecular weight ( $M_{\rm w}$ ) and the hydroxyethyl content (% OC<sub>2</sub>H<sub>4</sub>OH). Conversely, HPMC and HEMC are determined by three structural parameters *i.e.* the molecular weight, the methoxyl content (% OCH<sub>3</sub>), and the hydroxypropyl (in HPMC, % OC<sub>3</sub>H<sub>6</sub>OH) or hydroxyethyl (in HEMC, % OC<sub>2</sub>H<sub>4</sub>OH) content.

Besides, a CE molecule was also determined by two structural parameters named DS and MS. Indeed, the amount of substituent groups on the anhydroglucose units can be designated by wt.% or by the average number of substituent groups attached to the ring, a concept known to cellulose chemists as "degree of substitution" noted DS. The DS corresponds to the average number of hydroxyl groups per anhydroglucose unit rings substituted by etherifying groups to become a hydroxyethyl, hydroxypropyl or methoxyl group. The molar substitution (MS) reports the number of moles of hydroxypropyl groups per mole of anhydroglucose.

The molecular weight ( $M_{\rm w}$ ) distribution was performed by Size Exclusion Chromatography (SEC) using 8 polymaltotrioses as standard samples. A very minor population of oligomers ( $M_{\rm w}$ <500 Da) is only detected for HECs. The substitution degree was investigated by Near Infra-Red spectroscopy (NIR). All details concerning SEC and NIR protocols were previously described [6]. CE characterization results are detailed in Table 1.

### 2.3. Brief overview of the experimental methods

In this paper, we applied a similar experimental methodology that the approach proposed for the study of CE-C<sub>3</sub>S interactions. As a result, steps of each protocol are precisely detailed in a previous paper [2]. In short, we can just recall the main items of the experimental techniques. Firstly, adsorption data of CE on aluminate phases was based on the dosage of CE into supernatant thanks to a phenol-sulfuric acid method. The concept is to put in contact a given [CE] with a well-characterized mineral phase. After 2 h of exposure time, under nitrogen atmosphere and constant magnetic stirring, [CE] in the supernatant was determined. The amount of polymer adsorbed on the mineral phase was finally easily calculated [2]. Besides, conductometry is a powerful tool for monitoring C<sub>3</sub>A hydration kinetics because of this method provides easily rather detailed information on the different steps of the hydration reaction [3,4]. In fact, conductometry appears as a convenient comparative method as long as the relative concentrations of all ingredients are kept constant and only one variable is changed at a time (in this case, the chemistry of CE). C<sub>3</sub>A hydration was performed in a limewater solution ([Ca(OH)<sub>2</sub>] = 20 mM) with a liquid to solid ratio equal to 20. The surface area of the mineral phases was analyzed by nitrogen adsorption in a Micromeritics ASAP 2000 nitrogen adsorption apparatus. The samples measured were degassed at 100 °C before the measurements. The surface area was determined by the multipoint BET method using the adsorption data. Results are reported in Table 2. The determination of calcium, aluminium and sulphate concentration was obtained using ionic chromatography. This was performed on a Dionex apparatus composed of a GP50 pump, a CS12A column for cation analysis, an AS11HC column for anions, a CD conductometric detector and an UV-visible detector. The analysis conditions are given in [2].

### 3. Adsorption of cellulose ethers on ettringite and calcium hydroaluminates

As C<sub>3</sub>A reacts instantaneously with water to form calcium hydroaluminates, it is impossible to quantify the adsorption of CE on only C<sub>3</sub>A surface. On the contrary, we assume that the hydrated pure phases (i.e. ettringite and calcium hydroaluminates) were in quite stable equilibrium with the liquid phase. In this sense, in order to limit as far as we can any solid dissolution, adsorption experiments were performed with a solution previously ion-saturated in respect of each mineral phase investigated. We must also underline that, while ettringite is a pure phase synthesized at laboratory scale, the "calcium hydroaluminates" sample is simply obtained by hydrating pure C<sub>3</sub>A in water (without gypsum, liquid to solid ratio equal to 20) during 1 h. We followed the C<sub>3</sub>A hydration by conductometry, and then we characterized the solid by SEM (Fig. 1), XRD and BET measurement. All results emphasize that C<sub>2</sub>AH<sub>8</sub>-C<sub>4</sub>AH<sub>13</sub> but also C<sub>3</sub>AH<sub>6</sub> hydrogarnet structure, are the major phases composing this sample called "hydroaluminates".

The content of CE adsorbed was quantified per mass of mineral phase introduced (Fig. 2). A very disparate CE-adsorption behaviour is noticed as a function of the hydrated aluminate phases. In fact, whereas an important CE adsorption on calcium hydroaluminates is observed, no significant adsorption on ettringite is emphasized. In other words, CE adsorption appears phase-specific or more rigorously the considered phases (ettringite versus "hydroaluminates") are CE-adsorption specific. Moreover, a great impact of CE chemistry on calcium hydroaluminates adsorption is highlighted. Obviously, HECs (i.e. H1, N1 and N7) show an elevated adsorption on calcium hydroaluminates always higher than 75 wt.%. although HPMCs (i.e. U2 and P1) induce a weak adsorption always lower than 20 wt.%. Finally, the surface area of mineral phases was also determined prior to experiment (Table 2). This leads to determine the content of CE adsorbed per square meter of calcium hydroaluminates introduced. We note that HECs adsorption on calcium hydroaluminates is always higher to 200 μg/m<sup>2</sup> although HPMCs adsorption is around 50  $\mu g/m^2$ . HECs adsorption on calcium hydroaluminates appears at least 4 times higher than HPMCs adsorption. All things considered, we demonstrate that significant CE adsorption can occur and markedly depends on both CE chemistry and substrate phase (i.e. calcium hydroaluminates or ettringite).

### 4. Hydration of pure C<sub>3</sub>A in diluted limewater

We began with the study of the non admixed pure  $C_3A$  in diluted media. The reaction was monitored by conductometry and ionic

**Table 2**Surface area measured of the mineral phases studied.

Mineral phases	Surface area (m <sup>2</sup> g <sup>-1</sup> )
C <sub>3</sub> A	$0.51 \pm 0.01$
Gypsum	$0.53 \pm 0.02$
Ettringite	$7.79 \pm 0.07$
C <sub>3</sub> A hydrated 30 min (called "hydroaluminates")	$5.26 \pm 0.09$

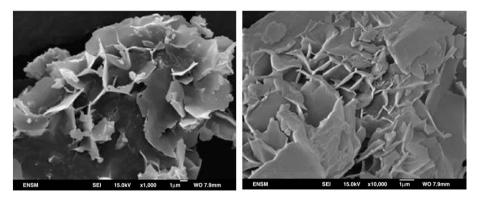


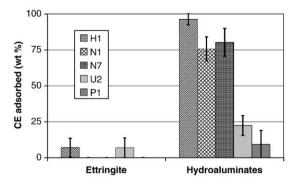
Fig. 1. SEM observation of calcium hydroaluminates faceplate after C<sub>3</sub>A grain hydration during 1 h in water (liquid to solid ratio equal to 20).

chromatography (Fig. 3). We emphasized that the conductivity curve perfectly reflects the calcium concentration evolution. Furthermore, the aluminium concentration evolves in the opposite way than the calcium concentration. The conductivity drop observed can be induced by the amphoteric nature of aluminium ion acting as an acid and thus forming aluminate ions by depleting the hydroxide concentration. Observably, three different stages were distinguished (Fig. 3).

The first stage corresponds to the decrease of the conductivity. In the same time, the calcium concentration decreases while the aluminium concentration increases. XRD experiment was also performed in order to identify phases which successively precipitated. According to the literature [3,7], we assume that this first stage highlights  $C_3A$  dissolution with simultaneously calcium hydroaluminates precipitation. The calcium to aluminium ratio is equal to 1.5 during  $C_3A$  dissolution. As the calcium concentration decreases while the aluminium concentration increases, it appears that the calcium to aluminium ratio of calcium hydroaluminates which precipitate should be higher than 1.5. Minard proposed in order to explain the different stoichiometry of calcium hydroaluminates that a solid solution  $C_xAH_y$  probably exists in which  $C_2AH_8$  and  $C_4AH_{13}$  are two limits [7].

During the second stage, a plateau is observed for all parameters monitored: conductivity, aluminium and calcium concentration. This indicates that a steady-state of  $C_3A$  hydration reaction occurs. Therefore, hydration products which precipitate during this period have globally a calcium to aluminium ratio very close to the one releases during  $C_3A$  dissolution, *i.e.* 1.5. Moreover, any hydrogarnet  $C_3AH_6$  was detected by XRD during this second stage. As a result, the stoichiometric ratio of 1.5 corresponds to the precipitation of 1 mol of  $C_2AH_8$  and 1 mol of  $C_4AH_{13}$ , for the dissolution of 2 mol of  $C_3A$ .

Finally, XRD experiments put clearly in evidence the precipitation of hydrogarnet  $C_3AH_6$  during the third stage. The precipitation of  $C_3AH_6$  induces an increase of the calcium concentration (to reach a

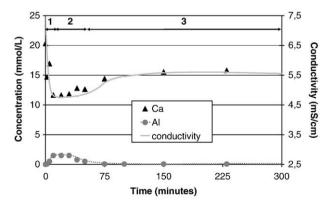


**Fig. 2.** CE adsorption on ettringite and hydroaluminates expressed in wt.% after a 2 h-exposure time (initial concentration of CE equal to 15 mg/g of pure mineral phase introduced, L/S = 20).

plateau) and the progressive consumption of all aluminium ions of the solution.

### 5. Influence of cellulose ethers on C<sub>3</sub>A hydration in absence of gypsum

We examined the C<sub>3</sub>A hydration in limewater without calcium sulphate and in addition of CE. So as to exhibit how CE can act during calcium hydroaluminates precipitation, we focused on HEC H1 which induces the stronger slowing down behaviour. The monitoring of the conductivity as well as calcium and aluminium ions allowed to bring interesting data. More precisely, two main stages were clearly put in evidence during C<sub>3</sub>A hydration without calcium sulphate and in presence of H1 (Fig. 4). During the first stage we observed a slower rate of calcium ions decrease (Fig. 4), in comparison with pure C<sub>3</sub>A hydration without calcium sulphate and CE (Fig. 3). Furthermore, the rise of aluminium concentration reaches 10 mmol/L at the end of the first stage (Fig. 4), a value 5 times higher than the maximum of aluminium concentration attained in the case of pure C<sub>3</sub>A hydration without calcium sulphate and CE (Fig. 3). This indicates both a slowing down of C<sub>3</sub>A dissolution and calcium hydroaluminates precipitation. Besides, as the calcium concentration decreases whereas the aluminium concentration rises, we assume that the calcium to aluminium ratio of calcium hydroaluminates which precipitate should be higher than 1.5. Finally, when the first period is finished, even if the hydroaluminates precipitation is doubtless put in evidence by SEM observation of C<sub>3</sub>A grain, the amount of calcium hydroaluminates is not enough to be detected by XRD. Then, the beginning of the second period corresponds to the start of the aluminium concentration reducing while the calcium concentration remains constant. Thus, we assume that this second period highlights a very progressive C<sub>3</sub>AH<sub>6</sub> precipitation (confirmed by XRD characterization). To sum up, H1



**Fig. 3.** C<sub>3</sub>A hydration in limewater without calcium sulphate: conductivity curve, calcium and aluminium concentration  $(L/S = 20, [Ca(OH)_2 = 20 \text{ mM}])$ .

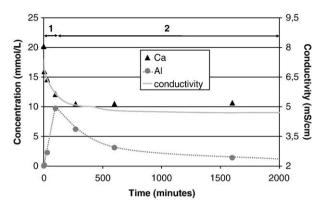


Fig. 4. Impact of HEC H1 on  $C_3A$  hydration in limewater without calcium sulphate: conductivity curve, calcium and aluminium concentration  $(L/S = 20, [Ca(OH)_2 = 20 \text{ mM}])$ .

doubtless induces a strong slowing down of both  $C_3A$  dissolution and calcium hydroaluminates precipitation.

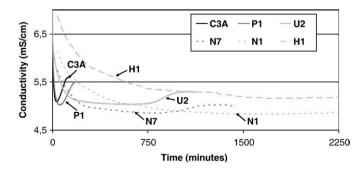
Afterwards, we showed that the slowing down of  $C_3A$  hydration hardly depends on the chemical nature of the CE applied (Fig. 5). In fact, a gradual effect on the delay was doubtless observed as a function of the type of CE molecule introduced. Obviously, we noticed that HECs (*i.e.* H1, N1 and N7) induce a stronger slowing down than HPMCs (*i.e.* U2 and P1). Thus, we demonstrated that CE chemistry plays a major role on the retardation of  $C_3A$  hydration without calcium sulphate. Moreover, we noticed that the higher the CE adsorption on calcium hydroaluminates (Fig. 2), the stronger the delay of the precipitation of calcium hydroaluminates (Fig. 5).

All things considered, we perfectly showed that CE can induce a slowing down of both  $C_3A$  dissolution and calcium hydroaluminates precipitation. This delay seems to be mainly caused by CE adsorption, on at least hydroaluminates, because of the higher the CE adsorption on calcium hydroaluminates (Fig. 2), the stronger the delay of the precipitation of calcium hydroaluminates (Fig. 5). As a result, CE chemistry appears as an important controlling factor since we noticed that the retardation of  $C_3A$  hydration without calcium sulphate is well-correlated to the CE-adsorption capacity on calcium hydroaluminates while this CE-adsorption mainly depends on CE structural parameters.

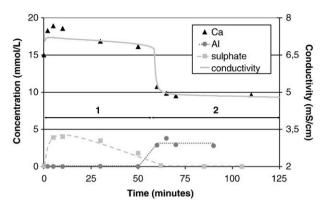
### 6. Hydration of C<sub>3</sub>A-gypsum system in diluted limewater

Firstly, we studied the hydration behaviour of the non admixed  $C_3A$ -gypsum system in diluted media. The solution conductivity as well as calcium, aluminium and sulphate concentrations were followed during the conductometry experiments. Two periods were clearly observed (Fig. 6).

The first hydration period of  $C_3A$ -gypsum system corresponds to the presence of sulphate ions into solution. Based on different works [3,4,7],



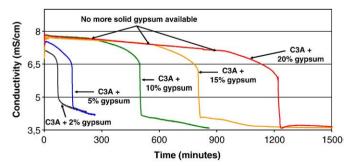
**Fig. 5.** Impact of CE on  $C_3A$  hydration in limewater without calcium sulphate: conductivity curves  $(L/S = 20, [Ca(OH)_2 = 20 \text{ mM}])$ .



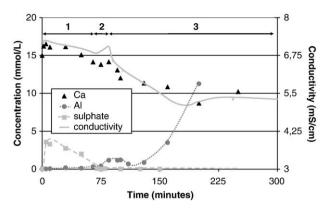
**Fig. 6.**  $C_3A$  hydration in limewater with calcium sulphate: conductivity curve, calcium, sulphate and aluminium concentration  $(2 \text{ wt}\% \text{ of gypsum}, L/S = 20, [Ca(OH)_2 = 20 \text{ mM}])$ .

this period refers to gypsum and C<sub>3</sub>A dissolution where as the ettringite formation takes place. During this first stage we notice a continuously decrease of calcium ions while no aluminium ions are detected into solution. Moreover, the sulphate concentration rises until a plateau at the beginning of the reaction, despite the fact that these ions were consumed to precipitate ettringite. This plateau is very short (around 5 min) when only 2 wt.% of gypsum is initially added to C<sub>3</sub>A. In fact, although sulphate ions were consumed by the reaction to form ettringite, they were instantaneously replaced by the dissolution of gypsum to obtain a quite constant concentration of sulphate into solution. This quasi-steady state lasts as long as gypsum dissolution occurs, i.e. as long as solid gypsum remains in solution. Hence, the higher the initial amount of gypsum added initially to C<sub>3</sub>A, the longer the duration of this period during which the gypsum dissolution occurs. Therefore we can easily increase the duration of the quasi-steady state, between gypsum dissolution and ettringite precipitation, by increasing the initial amount of calcium sulphate added to C<sub>3</sub>A (Fig. 7). An initial linear evolution of conductivity, sign of the quasi-steady state instatement, is clearly highlighted from an addition of 10 wt.% of gypsum. At the end of this linear evolution, or in other words when no more solid gypsum is available, the sulphate concentration starts to decrease because of ettringite precipitation. From this time, a slightly decrease of conductivity and sulphate ions is noticed. That means that sulphate ions consumed in order to precipitate ettringite only come from sulphate ions previously stored up into solution during the gypsum dissolution. To summarize, during the first period of C<sub>3</sub>A-gypsum hydration corresponding to the presence of sulphate ions into solution, two main steps of ettringite precipitation is distinguished depending of the presence or not of solid gypsum.

The second hydration period of C<sub>3</sub>A-gypsum system starts when sulphate ions are entirely consumed. In fact, at the beginning of this second period, a fall of both conductivity and calcium ions occurs. In the same time, the sulphate concentration reaches zero, while aluminium



**Fig. 7.**  $C_3A$  hydration in limewater with various calcium sulphate weight ratio: conductivity curves (various amount of gypsum, L/S = 20,  $[Ca(OH)_2 = 20 \text{ mM}]$ ).



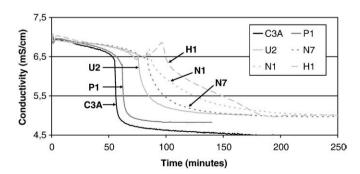
**Fig. 8.** Impact of HEC H1 on  $C_3A$  hydration in limewater with calcium sulphate: conductivity curve, calcium, sulphate and aluminium concentration (2 wt% of gypsum, L/S = 20,  $[Ca(OH)_2 = 20 \text{ mM}]$ ).

ions start to appear into the solution. According to Minard et al.'s works [3,7], these observations obviously emphasize that, when the ettringite precipitation stops because of the exhaustion of sulphate ions, a huge calcium hydroaluminates precipitation takes place. In fact, the reactions observed simply match to the hydration of  $C_3A$  in limewater without gypsum. Thus, the second period corresponds to the  $C_3A$  dissolution and the calcium hydroaluminates precipitation, which is at the origin of the strong drop of conductivity since consuming calcium ions and releasing aluminium ions into solution.

## 7. Influence of cellulose ethers on $C_3A$ hydration in presence of gypsum

To improve our understanding of the mechanism at the origin of this slowing down behaviour induced by CE, we studied H1 admixed  $C_3$ A-gypsum system. We firstly focused on a system containing 2 wt.% of gypsum. Three stages were discriminated (Fig. 8).

The first stage corresponds to the ettringite precipitation from sulphate ions of the solution without any gypsum dissolution. This part of the hydration is similar with the non admixed system (Fig. 7). However, the time necessary to consume all sulphate ions is 10 min higher compared to the non admixed system. Therefore, we assumed that CE may induce a weak slowing down of C<sub>3</sub>A dissolution and ettringite precipitation when all the calcium sulphate is dissolved. When sulphate ions are exhausted, although the instantaneous and massive precipitation of calcium hydroaluminates should happen, conversely we emphasized a rise of calcium concentration and conductivity. In fact, it seems that the calcium hydroaluminates precipitation is blocked. In presence of CE, the system seems to need a higher critical supersaturation level in order to precipitate calcium hydroaluminates. As there is no more sulphate to form ettringite, the



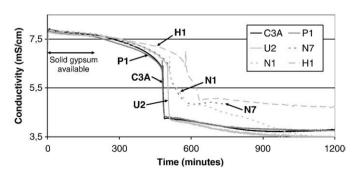
**Fig. 9.** Impact of CE on  $C_3A$  hydration in limewater with calcium sulphate: conductivity curves (2 wt.% of gypsum, L/S = 20, [Ca(OH)<sub>2</sub> = 20 mM]).

only reaction which can happen is  $C_3A$  dissolution. So, during this second stage, we observed only the  $C_3A$  dissolution so as to reach a higher critical supersaturation with respect to calcium hydroaluminates. Moreover, as this second period reflects only the  $C_3A$  dissolution, the slope of the conductivity curve during this stage is directly proportional to the rate of  $C_3A$  dissolution. As a result, on Fig. 9, we highlighted that the stronger the delay on both ettringite precipitation and  $C_3A$  dissolution (i.e. the longer the duration to consume all sulphate ions), the slower the  $C_3A$  dissolution rate (i.e. the lower the conductivity slope during the second stage where only  $C_3A$  dissolution occurs).

Finally, when the critical supersaturation of the liquid phase is enough elevated, the conductivity and calcium ions decrease while aluminium concentration starts to rise. Similarly to the second period of the non admixed C<sub>3</sub>A-gypsum system, this third stage of H1 admixed C<sub>3</sub>A-gypsum system indicates a precipitation of calcium hydroaluminates. However, the decrease of the conductivity slope and calcium concentration is weak in comparison with the non admixed system (Fig. 7). Thus, the rate of calcium hydroaluminates precipitation seems to be significantly slowing down in presence of H1.

The impact of CE chemistry in the hydration of C<sub>3</sub>A-gypsum system in diluted limewater was also performed using different gypsum to C<sub>3</sub>A weight ratio equal to 2 and 10 wt.% (Figs. 9 and 10). Results highlight a gradual effect on the slowing down of both ettringite and calcium hydroaluminates precipitation. The CE chemistry seems to play a major role since whatever the gypsum ratio added. Noticeably, we always remarked that HECs (*i.e.* H1, N1 and N7) induce a stronger slowing down than HPMCs (*i.e.* U2 and P1).

On one hand, we examined the influence of CE on ettringite precipitation. In presence of 10 wt.% of gypsum (Fig. 10), we can discriminate the two steps of ettringite precipitation previously described in paragraph 6. Conversely, with the presence of 2 wt.% of gypsum (Fig. 9), we only distinguish the second step of ettringite precipitation (i.e. the ettringite precipitation thanks to sulphate ions coming from the solution), because of the small amount of gypsum initially added to C<sub>3</sub>A is quickly dissolved during the first minutes of hydration. Besides, during the first step (i.e. the pseudo steady-state instatements where all sulphate ions are consumed by ettringite formation are replaced into solution by gypsum dissolution) no significant impact of CE is put in evidence. However, whatever the gypsum ratio added, a strong impact of CE is emphasized during the second step of ettringite precipitation. Observably, the slope of conductivity curves during the second step of ettringite precipitation as well as the duration to reach the beginning of the second period of hydration (i.e. the duration to reach the time where all sulphate ions are consumed) is more important in presence of CE (Figs. 9 and 10). In other words a significant slowing down of both ettringite precipitation



**Fig. 10.** Impact of CE on  $C_3A$  hydration in limewater with calcium sulphate: conductivity curves (10 wt.% of gypsum, L/S = 20, [Ca(OH)<sub>2</sub> = 20 mM]).

and C<sub>3</sub>A dissolution rate, depending on CE chemistry, is perceived. This delay occurs whatever the gypsum ratio added, but CE act only during the second step of ettringite precipitation (*i.e.* where the solid gypsum are entirely dissolved). It was also very interesting to underline that CE can reduce the ettringite precipitation rate although no significant adsorption of CE on ettringite was observed (Fig. 2).

On the other hand, we also studied the influence of CE on calcium hydroaluminates precipitation during the second hydration period of  $C_3A$ -gypsum, when sulphate ions are exhausted. In coherence with results illustrated in paragraph 5, a more or less slowing down of calcium hydroaluminates is emphasized as a function of CE chemistry. For HPMCs admixed system, we observe a strong drop of conductivity, sign of a massive and instantaneous precipitation of calcium hydroaluminates (Figs. 9 and 10) comparable to non admixed system. On the contrary, for HECs admixed system, we highlight a slower rate of calcium hydroaluminates precipitation. Moreover, it appears that the stronger the CE-adsorption on calcium hydroaluminates (Fig. 2), the stronger the slowing down of calcium hydroaluminates (Fig. 9).

### 8. Conclusion

Significant slowing down of  $C_3A$  hydration is put in evidence in diluted media. In particular, very low molecular mass CE (e.g. H1 molecule) are enable to strongly delay the  $C_3A$  hydration although no rise of viscosity is observed regarding the high L/S used. As a result, all things point to say that the retardation caused by CE cannot be explained thanks to the ionic motion hindrance assumption.

Furthermore, we demonstrate that CE adsorption is phase-specific. As a matter of fact an important CE adsorption on calcium hydroaluminates is emphasized, while no significant adsorption on ettringite is noticed. Moreover a great impact of CE chemistry on calcium hydroaluminates is highlighted because of HECs adsorption on this phase appears at least 4 times higher than HPMCs adsorption.

CE leads also to a gradual slowing down of the C<sub>3</sub>A hydration depending on CE chemistry. For all experimental conditions, we remark that HECs induce a higher delay than HPMCs. Based on these observations, substitutions groups (nature and content) seems to be

more important controlling factors on  $C_3A$  hydration rather than molecular mass. In fact, without calcium sulphate, we show that CE can reduce both the  $C_3A$  dissolution as well as the calcium hydroaluminates precipitation. It seems that the higher the CE adsorption on calcium hydroaluminates, the stronger the slowing down of calcium hydroaluminates precipitation. In addition of calcium sulphate, results emphasized that whatever the amount of gypsum added, CE induce a weak slowing down of  $C_3A$  dissolution, ettringite precipitation and then a strong reduce of calcium hydroaluminates precipitation.

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