

Interaction Between Lead Iron Niobate/Tungstate Ceramics and Silver/Palladium Metals

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Abstract: The interactions between ferroelectric $\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$ (PFN)/ $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$ (PFW) perovskite ceramics and silver/palladium metals were systematically investigated through the phase formation and microstructural variation. Silver did not react with PFN/PFW ceramics after heating to 900 °C, and perovskite grains were only distributed among the matrix of silver. After being heated with 70Ag/30Pd at 900 °C, no perovskite phases were significantly altered; however, in the PFN-rich ceramics, the palladium content in the alloy decreased along with the formation of PdO. Pure palladium was found to have the highest reactivity with PFN/PFW ceramics. The reactions between palladium and ceramics occurred vigorously from 850 °C and resulted in markedly different microstructures. Palladium caused PFW to decompose into PbWO_4 and Pb_2WO_5 , and also led to the dissociation of PFN/PFW ceramics to produce pyrochlore phases and Fe_2O_3 . The reactivity of palladium with perovskite phases was positively correlated with the PFN content in specimens. In addition, increasing the PFN content also tended to postpone the reduction process of PdO to palladium. © 1997 Elsevier Science Limited and Techna S.r.l. All rights reserved

1 INTRODUCTION

The multilayer ceramic capacitor (MLC) industry has been growing rapidly in the past few decades as a result of the requirement for miniaturization of electronic circuits. During the fabrication of MLCs, the dielectric ceramic layers are co-fired with the metal electrode layers at elevated temperatures. After co-firing, satisfactory physical integrity between the two kinds of layers is required. The incompatibility between ceramics and electrodes, shown by effects such as delamination or separation, will cause the formation of cracks when the parts are subjected to thermal stress during soldering for surface mount applications.^{1,2} Furthermore, the chemical interactions of ceramics with electrode metals have adverse effects on the electric performance of MLCs with regard to the insulation resistivity and dielectric char-

acteristics of dielectric ceramics.³ Therefore, research into the potential interactions between ceramics and electrode metals becomes a crucial issue for MLCs.

Relaxor ferroelectric lead iron niobate [$\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$, abbreviated to PFN] and lead iron tungstate [$\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$, abbreviated to PFW] are two well-known, important dielectric materials for MLC applications.^{4–11} These two materials react at elevated temperatures to form complete solid solutions which exhibit the perovskite structure. When the content of PFN in the solid solution is increased, the dielectric constant maximum becomes sharper, and the Curie temperature is raised, associated with an increase in sintering temperature.¹² Adjusting the composition to be 0.7PFN–0.3PFW can shift the Curie temperature to be near room temperature, and this material can be sintered at temperatures as low as 900 °C.¹² In light of the advantages of low-temperature sintering characteristics and high

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permittivity, the PFN/PFW-based system has been applied in MLCs where the inexpensive silver/palladium alloy is used as inner electrodes for cost saving. In spite of the application of PFN/PFW ceramics to MLCs, the interaction between the ceramics and electrodes with regard to the reactivity and stability of ceramics with electrode metals has not yet been thoroughly investigated.

The primary purpose of this study is to elucidate the interaction between the PFN/PFW ceramics and silver/palladium metals. The phase formation and the microstructural variation during the reaction were investigated. The PFN/PFW ratio in the perovskite compounds was varied in order to examine the influence of composition on the stability of perovskite compounds with metals. Moreover, the effects of the composition of ceramics on the oxidation and reduction reactions of metals were also studied.

2 EXPERIMENTAL

Proportionate amounts of reagent-grade starting materials (PbO , Fe_2O_3 , Nb_2O_5 and WO_3) were mixed according to the composition of $(1-x)\text{PFW}-x\text{PFN}$ at $x = 0, 0.3, 0.7$ and 1 . The specimens with a composition of $x = 0, 0.3, 0.7$ and 1 are designated as PFW, PF3, PF7 and PFN, respectively. These raw materials were ball-milled for 48 h with ethyl alcohol, using zirconia balls. After being dried in a rotary evaporator, the mixed powders were uniaxially pressed into disks of 8 mm in diameter under 196 MPa. For synthesizing PFW, the precursors were calcined at 870°C for 2 h. For the other three specimens, the mixed powders were heated at 900°C for 2–4 h. After the complete perovskite phases were formed in the specimens, the obtained ceramic powders were mixed, respectively, with an equal weight of metal powders. Pure silver, pure palladium, and a mixture of silver and palladium (with 70 mol% of silver) were used. The mixtures of ceramic and metal powders were heated for 2 h at temperatures ranging from 800°C to 900°C . The compounds present in the specimens were identified via X-ray powder diffraction (XRD) analysis using $\text{CuK}\alpha$ radiation. Microstructural evolution of the specimens was studied via a scanning electron microscope (SEM) coupled with energy dispersive X-ray spectroscopy (EDS). Differential thermal analysis (DTA) and thermogravimetry analysis (TGA) were performed to examine the oxidation/reduction reactions of metals and the weight change of specimens during heating in air.

3 RESULTS AND DISCUSSION

3.1 Interaction between PFN/PFW ceramics and silver

Four kinds of perovskite powders (PFW, PF3, PF7 and PFN) were heated with silver up to 900°C . The XRD analysis performed on the heated specimens revealed that all of the perovskite patterns remained unchanged after heating. Figure 1 illustrates the XRD patterns of the 900°C -heated mixtures of perovskite phases and silver. As shown in this figure, the diffraction patterns of the perovskite phase and silver can be clearly distinguished, and no other compound was formed. From the results of SEM, the grains of perovskite phase were found to distribute among the matrix of silver; moreover, the original morphology of perovskite grains was maintained. The micrographs of the specimens of PFW and PF3 mixed with silver after heating to 900°C are shown in Fig. 2. These XRD and SEM results indicate that silver can stably coexist with PFN/PFW perovskite phases up to 900°C without the occurrence of chemical reactions.

3.2 Interaction between PFN/PFW ceramics and silver/palladium

When the mixtures of perovskite compounds and silver/palladium were heated from 800°C to 900°C , no significant changes in the diffraction patterns of perovskite phases were observed. The XRD results of the 900°C -heated specimens are shown in Fig. 3. In pure PFW, the 70Ag/30Pd alloy was formed and exhibited a distinct diffraction pattern. As the PFN content in ceramics was increased, the diffraction peaks of silver/palladium became broadened and smeared into those of perovskite phases. In addition, a small amount of PdO was found in PF7 and PFN. Due to the formation of PdO , the palladium content in the alloy was lowered, resulting in an increase of the lattice constant with the diffraction peaks shifting to the low angle side.¹³ The broadening of the diffraction peaks of silver/palladium and the formation of PdO imply that a partial interaction occurred between PFN-rich ceramics and silver/palladium. In contrast, PFW was chemically stable with silver/palladium. The microstructural observation supported this inference. As seen in Fig. 4(a), the PFW grains were distributed in the metal matrix without changing their morphology. On the other hand, in the PFN specimen [see Fig. 4(b)], although the PFN grains can be still recognized, the matrix of metal became discontinuous with the formation

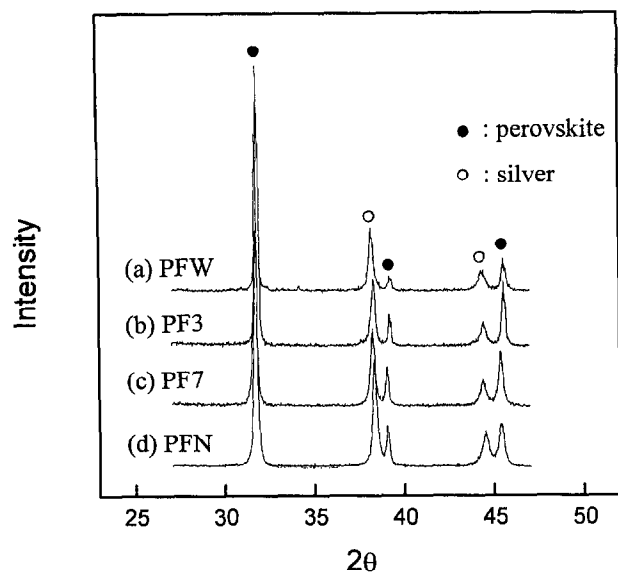


Fig. 1. X-ray diffraction patterns for the specimens of silver mixed with (a) PFW, (b) PF3, (c) PF7 and (d) PFN ceramics after heating at 900 °C for 2 h.

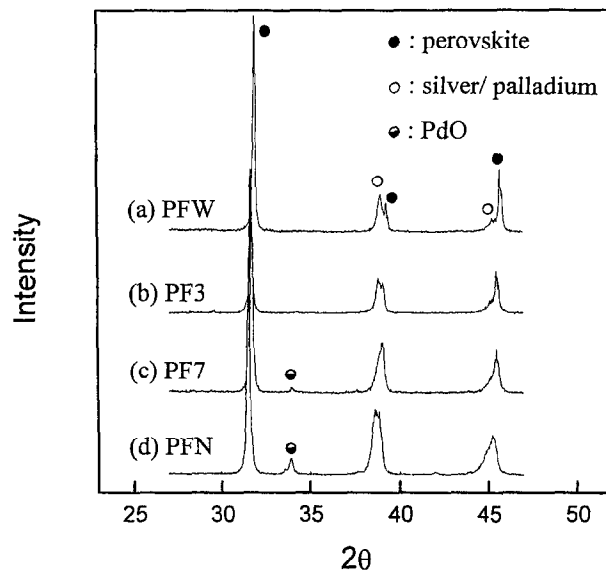
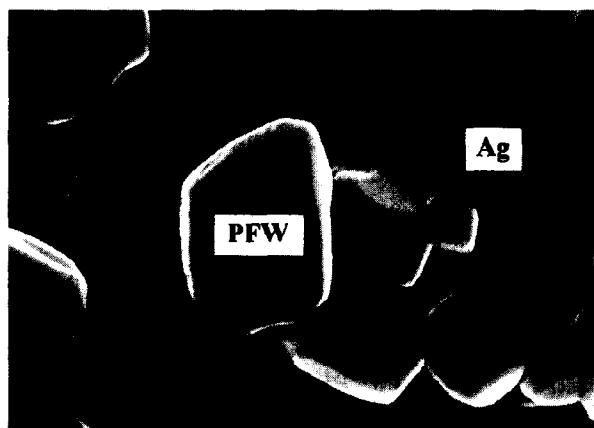
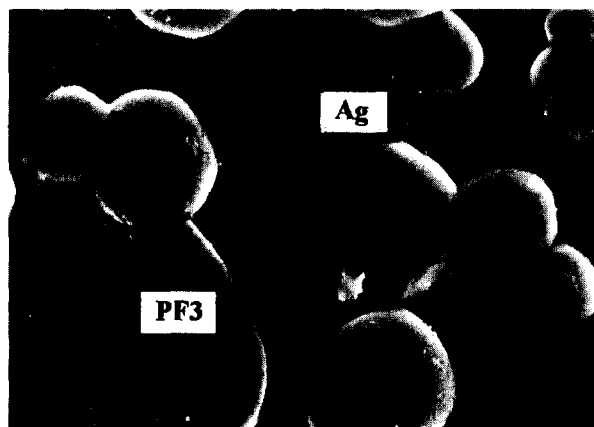


Fig. 3. X-ray diffraction patterns for the specimens of silver/palladium mixed with (a) PFW, (b) PF3, (c) PF7 and (d) PFN ceramics after heating at 900 °C for 2 h.

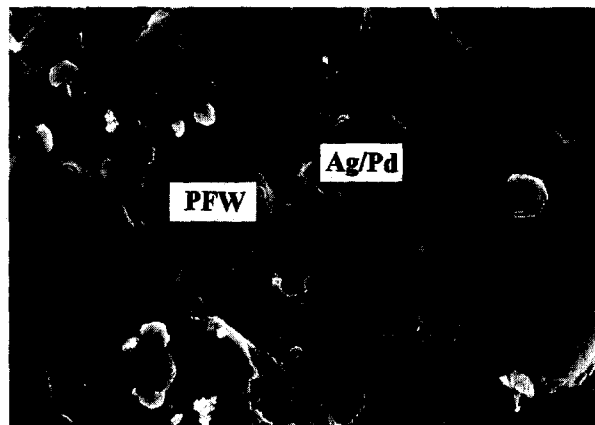


(a)

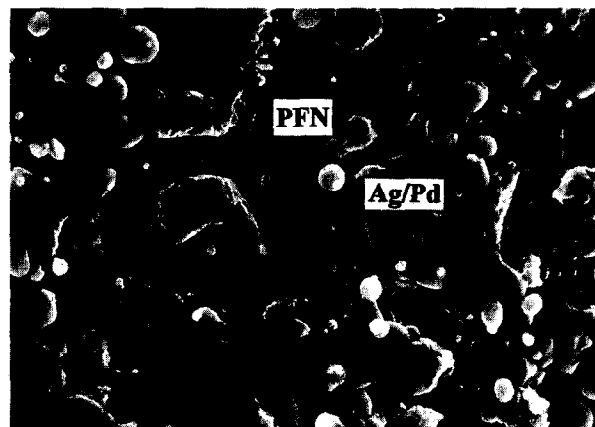


(b)

Fig. 2. Scanning electron micrographs of the specimens of silver mixed with (a) PFW and (b) PF3 ceramics after heating at 900 °C for 2 h.



(a)



(b)

Fig. 4. Scanning electron micrographs of the specimens of silver/palladium mixed with (a) PFW and (b) PFN ceramics after heating at 900 °C for 2 h.

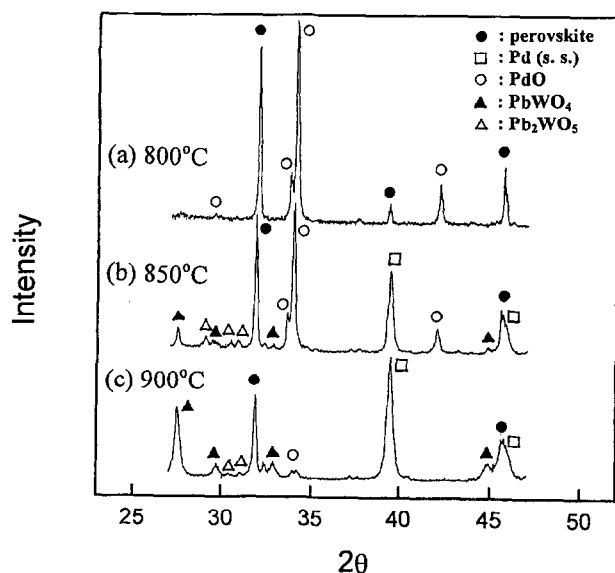


Fig. 5. X-ray diffraction patterns for the mixtures of PFW and palladium heated at (a) 800°C, (b) 850°C and (c) 900°C.

of a porous microstructure, indicating that a partial reaction occurred between PFN and the metal.

3.3 Interaction between PFN/PFW ceramics and palladium

The reactivity of palladium with the PFN/PFW ceramics was found to be considerably higher than those of silver and silver/palladium with the ceramics. The XRD patterns for the mixture of PFW and palladium vs heating temperatures are shown in Fig. 5. At 800°C all palladium was oxidized to become PdO without any variation of PFW. After 850°C-heating, PFW became unstable and was decomposed to generate lead tungstates PbWO₄ and Pb₂WO₅. In addition, the diffraction peaks of palladium shifted to the low angle side, implying the formation of a solid solution. At 900°C, the intensity of Pb(Fe_{2/3}W_{1/3})O₃ was further lowered with an increase in amount of PbWO₄, and most of the PdO was reduced.

The reactions of PF3, PF7 and PFN with palladium were similar to each other, but different from that of PFW with palladium. Figure 6 shows the XRD patterns for the heated mixture of PFN and palladium. After 800°C-heating, PFN kept the same crystal structure associated with the formation of PdO. As the temperature was raised to 850°C, PFN became severely decomposed, and a large amount of a compound exhibiting a pyrochlore structure was formed with a trace of Fe₂O₃. Part of the PdO was reduced to form a palladium-based solid solution. After heating up to 900°C, most of the PFN was decomposed. It is noted that in PFN-containing specimens, the

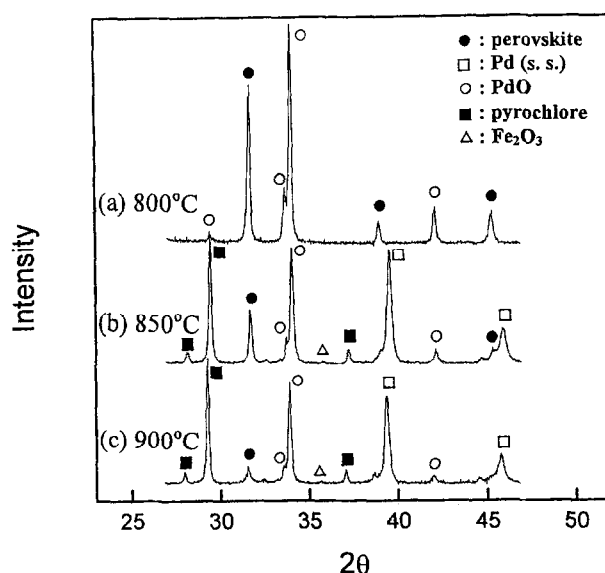


Fig. 6. X-ray diffraction patterns for the mixtures of PFN and palladium heated at (a) 800°C, (b) 850°C and (c) 900°C.

perovskite phases were decomposed to form pyrochlore phases instead of forming PbWO₄ and Pb₂WO₅, which were the products after the decomposition of PFW. The formation of the pyrochlore phase was also observed to occur during the reaction between palladium and Pb(Mg_{1/3}Nb_{2/3})O₃.³

The microstructures of the mixtures of perovskite compounds and palladium did not show significant changes until 850°C, the temperature at which the decomposition reactions occurred. After decomposition, a large amount of plate-like grains were formed in the mixtures of PFW and palladium [see Fig. 7(a)]. The EDS analysis confirmed these grains to be PbWO₄. The finding was in agreement with the results of XRD. The microstructures of decomposed PF3, PF7 and PFN were similar. The granular perovskite grains were decomposed to form small pyrochlore grains, and the microstructures became porous [see Fig. 7(b)]. The EDS analysis indicated that the matrix of palladium with all perovskite compounds contained lead species, implying that a palladium-lead alloy was formed during the reactions. The palladium-lead alloy was also found in the reaction of Pb(Mg_{1/3}Nb_{2/3})O₃ with palladium.³ The extraction of lead species from PFN/PFW ceramics to form the palladium-lead alloy will cause the perovskite structure to become unstable, thereby inducing the occurrence of decomposition.

The variation of the percentage of perovskite phases in the specimens vs heating temperatures is illustrated in Fig. 8. At 800°C only perovskite phases were present in the specimens without the occurrence of the pyrochlore phases. The percentage of perovskite phases was considerably decreased with the increase in temperature. At

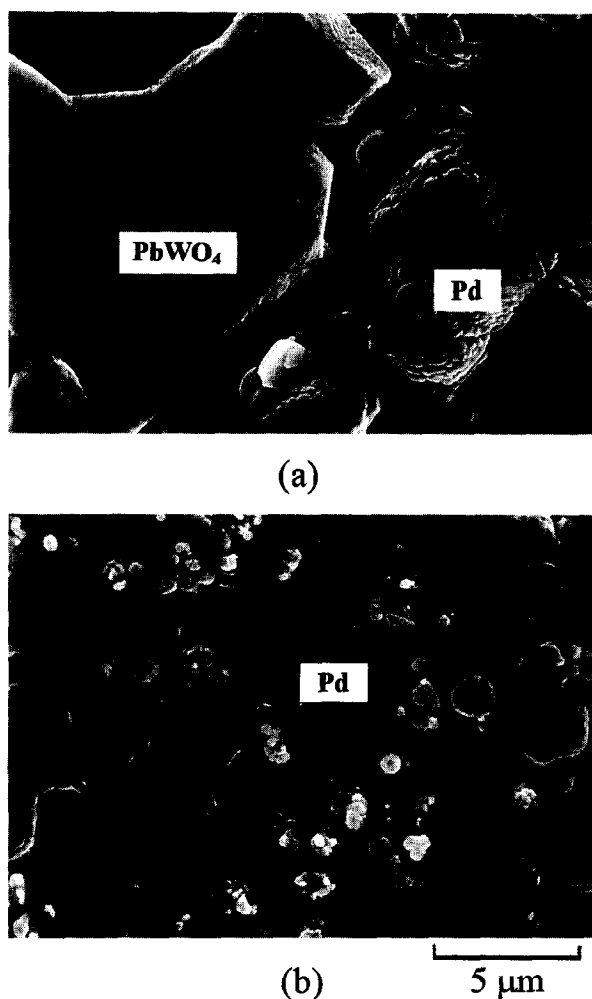


Fig. 7. Scanning electron micrographs of the specimens of palladium mixed with (a) PFW and (b) PF7 ceramics after heating at 900°C for 2 h.

900°C the percentage of perovskite phases dropped to become less than 50% in all specimens. As for PFN, only 10% of the perovskite phase remained. It is noted that the increase of PFN content tends to greatly decrease the remaining amounts of perovskite phases. This phenomenon indicates that the reactivity of palladium with PFN/PFW ceramics significantly depends on the chemical composition of the ceramics. Increasing the PFN content in ceramics will raise the reactivity of ceramics with palladium, and causes more ceramics to decompose.

For studying the oxidation/reduction reactions of palladium in the various perovskite compounds, thermal analysis experiments were performed. The DTA and TGA results of PF7 reacting with palladium are illustrated in Fig. 9. A broad exothermic peak appeared on the DTA plot at above 250°C, associated with a weight gain on the TGA plot. This exothermic reaction indicated the oxidation of palladium to form PdO. As the temperatures got higher, an endothermic reaction vigorously arose from 800°C, with a peak

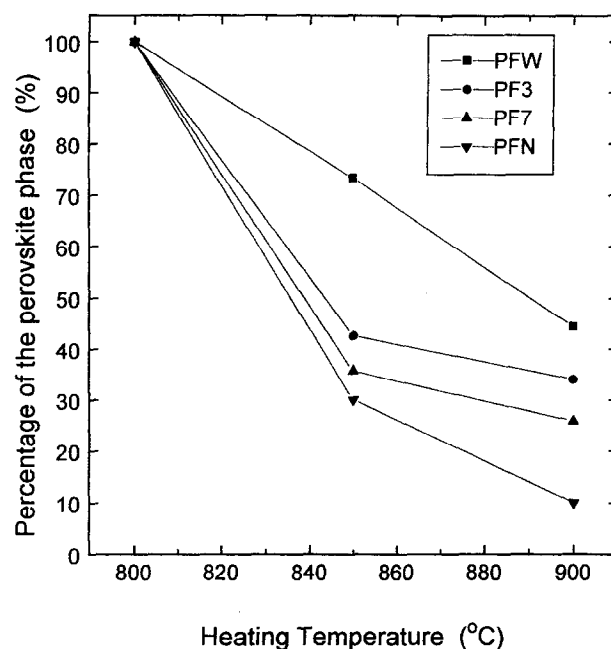


Fig. 8. The relation between the percentage of perovskite phases that remained in ceramics and heating temperatures.

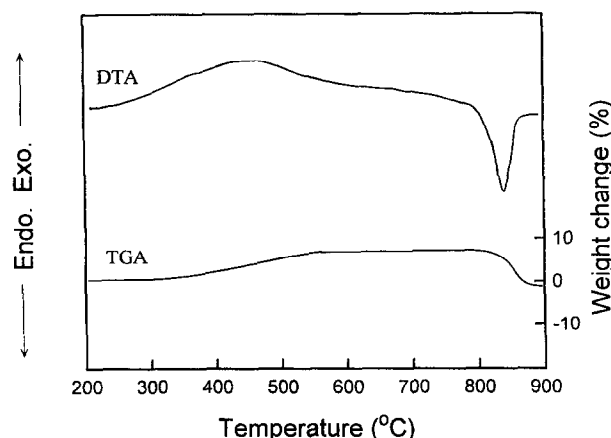


Fig. 9. Differential thermal and thermogravimetric analysis of the mixtures of PF7 and palladium.

temperature at 840°C. From the onset temperature of this endotherm, the weight of the specimen was found to decrease. This endothermic reaction was caused by the dissociation of PdO to become palladium. Figure 10 illustrates the DTA curves of the perovskite compounds mixed with palladium. All specimens showed a broad exotherm from above 250°C, indicating the oxidation of palladium. At elevated temperatures, a sharp endotherm caused by the reduction of PdO occurred in all specimens. The temperatures of the endotherm for PFW, PF3, PF7 and PFN were 820°C, 830°C, 840°C and 860°C, respectively. In PFW another small endothermic peak was found at around 860°C, which was possibly related to the liquid-phase formation caused by the presence of Pb_2WO_5 .^{14,15} The results in Fig. 10 show that increasing the PFN content

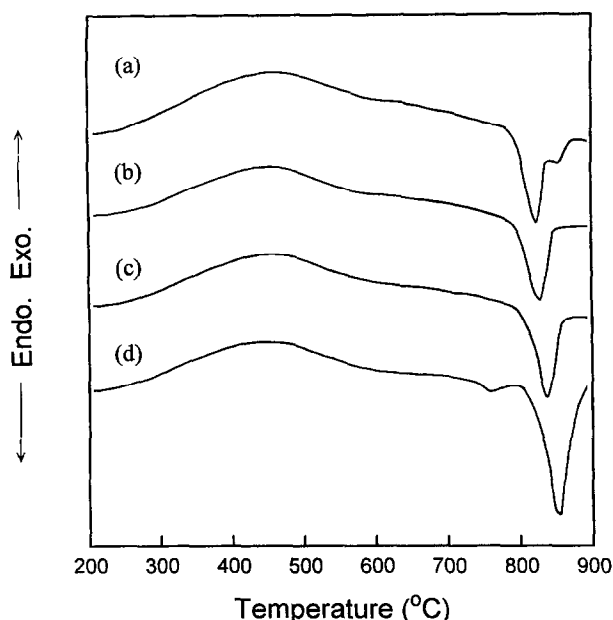


Fig. 10. Differential thermal analysis of the mixtures of perovskite compounds and palladium.

shifted the endotherm to the high-temperature side, implying that the reduction process of PdO was postponed when the content of PFN was increased. The PFN content in PFN/PFW ceramics was found to not only substantially vary the reactivity of palladium with ceramics, but also alter the reduction process of PdO.

4 CONCLUSIONS

The interactions of $\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$ (PFN)/ $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$ (PFW) perovskite ceramics with silver/palladium metals were investigated via the analysis of XRD, SEM and DTA. After heating, pure silver did not react with PFN/PFW ceramics, and ceramic grains maintained their original morphology in the matrix of silver. When the mixtures of the ceramics and 70Ag/30Pd were heated at 900°C, the perovskite phases were not significantly changed. However, in the PFN-rich ceramics, the composition of the alloy was varied with a decrease in the palladium content, associated with the formation of PdO. Pure palladium was found to have the highest reactivity with PFN/PFW. The reactions occurred vigorously from 850°C and caused remarkable variation in the microstructures. Palladium induced the decomposition of PFW to form lead tungstates PbWO_4 and Pb_2WO_5 , and resulted in the dissociation of

PFN/PFW ceramics to produce pyrochlore phases and Fe_2O_3 . The reactivity of PFN/PFW ceramic with palladium was virtually dependent on the chemical composition of the ceramics. Increasing the PFN content led to a rise in the reactivity of palladium with ceramics, which caused more ceramics to decompose. In addition, the increase in the PFN content also postponed the reduction process of PdO to palladium.

REFERENCES

1. PEPIN, J. G. & BORLAND, W., Electrode-based causes of delaminations in multilayer ceramic capacitors. *J. Am. Ceram. Soc.*, **72** (1989) 2287–2291.
2. FREIMAN, S. W. & POHANKA, R. C., Review of mechanically related failure of ceramic capacitors and capacitor materials. *J. Am. Ceram. Soc.*, **72** (1989) 2258–2263.
3. WANG, S. F. & HUEBER, W., Interaction of silver/palladium electrodes with lead- and bismuth-based electrodes. *J. Am. Ceram. Soc.*, **76** (1993) 474–480.
4. TAKAMIZAWA, H., UTSUMI, K., YONEZAWA, M. & OHNO, T., Large capacitance multilayer ceramic capacitor. *IEEE Trans. Compon., Hybrids. Manuf. Technol.*, **CHMT-4** (1981) 345–349.
5. YONEZAWA, M., Low-firing multilayer capacitor materials. *Am. Ceram. Soc. Bull.*, **62** (1983) 1375–1383.
6. JANG, S. J., SCHULZE, W. A. & BIGGERS, J. V., Low-firing capacitor dielectrics in the system $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$ – $\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$ – $\text{Pb}_5\text{Ge}_3\text{O}_{11}$. *Am. Ceram. Soc. Bull.*, **62** (1983) 216–218.
7. REILEY, T. C., BADDING, J. V., PAYNE, D. A. & CHANCE, D. A., A low-temperature firing thick film capacitor material based on lead iron niobate/tungstate. *Mater. Res. Bull.*, **19** (1984) 1543–1549.
8. UTSUMI, K. & YONEZAWA, M., Large capacitance multilayer ceramic capacitor with low firing ceramic material. *New Mater. New Process.*, **3** (1985) 142–149.
9. TAKAHARA, H. & KIUCHI, K., Dielectric properties of mixed-sintering ceramics in the system $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$ – $\text{Pb}(\text{Fe}_{1/2}\text{Nb}_{1/2})\text{O}_3$. *Adv. Ceram. Mater.*, **1** (1986) 346–349.
10. FU, S. L. & CHEN, G. F., Low firing thick film dielectrics in the system $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})_x(\text{Fe}_{1/2}\text{Nb}_{1/2})_{0.86-x}\text{Ti}_{0.14}\text{O}_3$ – $\text{Bi}_2\text{O}_3/\text{Li}_2\text{O}$. *Am. Ceram. Soc. Bull.*, **66** (1987) 1397–1400.
11. UTSUMI, K., SHIMADA, Y. & TAKAMIZAWA, H., Monolithic multicomponents ceramic (MMC) substrate. *Mater. Res. Soc. Symp. Proc.*, **72** (1986) 15–26.
12. SHIMADA, Y., UTSUMI, K., YONEZAWA, M. & TAKAMIZAWA, H., Properties of the large-capacitance multilayer ceramic capacitor. *Jpn J. Appl. Phys.*, **20** (1981) 143–146.
13. WANG, S. F. & HUEBER, W., Thermodynamic modelling of equilibrium subsolidus phase relations in the Ag–Pd– O_2 system. *J. Am. Ceram. Soc.*, **74** (1991) 1349–1353.
14. MIZUTANI, N., LU, C. H., SHINOZAKI, K. & KATO, M., Formation of a high-temperature liquid phase during the sintering of $\text{Pb}(\text{Fe}_{2/3}\text{W}_{1/3})\text{O}_3$. *J. Am. Ceram. Soc.*, **73** (1990) 1214–1220.
15. LU, C. H., Compositional effect on the liquid-phase formation in lead iron tungstate ferroelectric ceramics. *J. Am. Ceram. Soc.*, **77** (1994) 2529–2535.