# **Effect of Loading Speed on Fracture** Behaviour of ZrO<sub>2</sub>(Al<sub>2</sub>O<sub>3</sub>) Matrix Composites Reinforced with SiC Whiskers

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Abstract: The fracture toughnesses, fracture behaviour and toughening mechanisms of 20 vol% SiCw-ZrO<sub>2</sub> (2 mol% Y<sub>2</sub>O<sub>3</sub>), 20 vol% SiCw-ZrO<sub>2</sub> (6 mol% Y<sub>2</sub>O<sub>3</sub>), 20% SiCw-Al<sub>2</sub>O<sub>3</sub> and 20 vol% SiCw-20 vol% ZrO<sub>2</sub> (2 mol% Y<sub>2</sub>O<sub>3</sub>)-Al<sub>2</sub>O<sub>3</sub> composites (SiCw means SiC whisker) were investigated by three-point bending tests, XRD and scanning electron microscopy techniques. The results show that the fracture toughnesses of the composite materials increase with increasing loading speed because of the increase in the amount of dynamic t→m ZrO<sub>2</sub> transformation and whisker pullout effect. Whisker/matrix characteristis have a significant influence on the effect of loading speed on the fracture behaviour. © 1998 Elsevier Science Limited and Techna S.r.l.

#### 1 INTRODUCTION

The incorporation of  $\beta$ -SiC whiskers into  $ZrO_2(Y_2O_3)$ ,  $Al_2O_3$ ,  $ZrO_2(Y_2O_3) + Al_2O_3$ other ceramic matrices has been shown to produce significant increases in mechanical strength and fracture toughness. 1-4 The increase in strength can be understood in terms of the reinforcing effect of the whiskers and is dependent on the in-situ strength of each phase. The increase in toughness is attributed to several energy-absorbing processes, particulary crack deflection and crack bridging by the whiskers, whisker pullout, and the stressinduced martensitic transformation of tetragonal zirconia grains. 1-6 The operation of various toughening mechanisms depends, to a large extent, on the nature of the whisker/matrix interface. 1,3,4,7,8

Ceramic matrix composites are increasingly being utilized in structural applications where

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severe environments are encountered. Their low specific gravity, high hardness, thermal stability, and resistance to corrosion make them important materials in technological application. However, ceramic materials are sensitive to dynamic loading.9-11 So far, studies in this field are very limited.

The research reported in this article deals specifically with the effect of loading speed on the fracture behaviour of 20 vol% SiCw-ZrO<sub>2</sub>  $(2 \text{ mol}\% \text{ Y}_2\text{O}_3)$ ,  $20 \text{ vol}\% \text{ SiCw-ZrO}_2$   $(6 \text{ mol}\% \text{ Pol}\% \text{ SiCw-ZrO}_2)$ Y<sub>2</sub>O<sub>3</sub>), 20 vol% SiCw-Al<sub>2</sub>O<sub>3</sub> and 20 vol% SiCw-20 vol% ZrO<sub>2</sub> (2 mol% Y<sub>2</sub>O<sub>3</sub>)-Al<sub>2</sub>O<sub>3</sub> composites.

#### 2 EXPERIMENTAL

The materials used in this study were ZrO<sub>2</sub>  $(2 \text{ mol}\% \text{ Y}_2\text{O}_3), \text{ ZrO}_2 (6 \text{ mol}\% \text{ Y}_2\text{O}_3), \alpha\text{-Al}_2\text{O}_3$ and 20 vol% ZrO<sub>2</sub> (2 mol% Y<sub>2</sub>O<sub>3</sub>)-Al<sub>2</sub>O<sub>3</sub> composites reinforced with 20 vol% SiC whiskers. The  $\beta$ -SiC whiskers were supplied by Tokai Carbon, F. Ye et al.

Japan, with a diameter of  $0.5 \sim 1 \,\mathrm{mm}$  and a length of  $30 \sim 60$  mm. Ultrafine zirconia powders, stablized by 2 or 6 mol% Y<sub>2</sub>O<sub>3</sub>, had an average particle size of 0.65 mm. Ultrafine Al<sub>2</sub>O<sub>3</sub> powders, with a grain size of about 0.1 mm, were shown, by the XRD technique, to be  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>. The 20 vol% SiCw-ZrO<sub>2</sub>(Y<sub>2</sub>O<sub>3</sub>) composites were hotpressed under a pressure of 25 MPa for 1h at 1600°C. The SiCw-Al<sub>2</sub>O<sub>3</sub> and SiCw-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> composites were hot-pressed under a pressure of 25 MPa for 1 h at 1650°C. As-received and acidleached whiskers were incorported into  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> matrix, respectively, to elucidate the effect of whisker surface treatment on the properties of the composites. The whiskers were leached with 5 vol% HF acid for 10 h and washed five times with distilled water and absolute alcohol to remove the oxide-rich layer present on the surface of the as-received whiskers.

Fracture toughness measurements of the composites were performed on single-edge notched bar (SENB) specimens (2 mm×4 mm×25 mm) with a span of 16 mm, and a half-thickness notch was made using a diamond wafering blade. The test was conducted at cross-head speeds of between 0.002 mm min<sup>-1</sup> and 2 mm min<sup>-1</sup>.

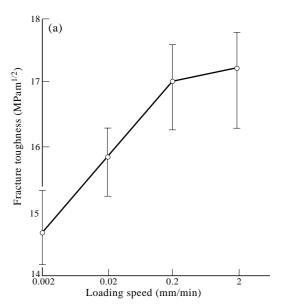
The percentage of t-ZrO<sub>2</sub> in the total ZrO<sub>2</sub> was estimated by XRD on both as-polished and the fractured surfaces. Fracture surfaces of the composites were examined using a Hitachi S-570 scanning electron microscope.

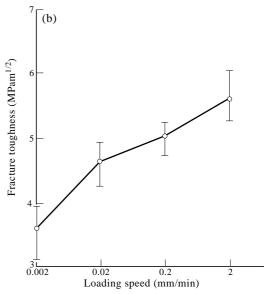
#### 3 RESULTS

The hot-pressing conditions used in this study result in almost theoretically dense composites with a very homogeneous distribution of whiskers. Each of the different materials will be discussed separately.

# 3.1 Effect of loading speed on fracture behaviour of 20 vol% SiCw–ZrO<sub>2</sub>(Y<sub>2</sub>O<sub>3</sub>) composites

The influence of loading speed on the fracture toughness from  $0.002\,\mathrm{mm\,min^{-1}}$  to  $2\,\mathrm{mm\,min^{-1}}$  for SiCw–ZrO<sub>2</sub> composites is shown in Fig. 1, indicating that the fracture toughness increased with increasing loading speed. For ZrO<sub>2</sub> ( $2\,\mathrm{mol\,\%}\ \mathrm{Y_2O_3}$ ) composite, the fracture toughness increases from 14.67 MPam<sup>1/2</sup> at  $0.002\,\mathrm{mm\,min^{-1}}$  to  $17.00\,\mathrm{MPam^{1/2}}$  at  $0.2\,\mathrm{mm\,min^{-1}}$ . However, in the higher loading speed range of  $0.2-2\,\mathrm{mm\,min^{-1}}$ , the fracture toughness of the composite is not sensitive to the loading speed. In contrast, the fracture toughness of ZrO<sub>2</sub> ( $6\,\mathrm{mol\,\%}\ \mathrm{Y_2O_3}$ ) composite always increases with increasing loading speed from 0.002 to  $2\,\mathrm{mm\,min^{-1}}$ .





**Fig. 1.** Effect of loading speed on fracture toughness of ZrO<sub>2</sub>(Y<sub>2</sub>O<sub>3</sub>) + 20vol% SiCw composites: (a) ZrO<sub>2</sub>(2Y) + SiCw composites; (b) ZrO<sub>2</sub>(6Y) + SiCw composites.

The results of XRD analysis of the fracture surfaces of  $ZrO_2$  (2 mol%  $Y_2O_3$ ) composite are shown in Table 1. It can be seen that the dynamic  $t\rightarrow m$   $ZrO_2$  transformation exists at both the low and high loading speed, and the amount of  $t\rightarrow m$  transformation increases with loading speed. The increase in dynamic  $t\rightarrow m$  transformation undoubtedly makes a greater contribution to the fracture toughness of the composite. This is consistent with the measured results of fracture toughness. For  $ZrO_2(6Y)$  composite, there is no dynamic  $t\rightarrow m$   $ZrO_2$  transformation within the whole loading speed range in our study, as shown in Table 2, indicating no effect of transformation toughening.

SEM fractographs of the ZrO<sub>2</sub>(2Y) composite are shown in Fig. 2, indicating that the number and length of whisker pullout increase with increasing loading speed, in particular at the lower loading

Materials		Loading speed ( $\nu$ ) (mm min <sup>-1</sup> )						
	0.002	0.02	0.2	2				
ZrO <sub>2</sub> (2Y)+20 vol% SiCw	14.67±0.50	15.80±0.55	17.00±0.70	17.20±0.85				
$ZrO_2(6Y) + 20 \text{ vol}\% \text{ SiCw}$	3.60±0.35	4.66±0.30	5.01±0.25	5.60±0.30				

Table 1. Fracture toughnesses ( $K_{IC}$ , MPam<sup>1/2</sup>) of ZrO<sub>2</sub>(Y<sub>2</sub>O<sub>3</sub>)+20 vol% SiCw composites at different loading speeds during SENB tests

speeds [Fig. 2(a) and (b)]. At a higher loading speed, this effect is not apparent [Fig. 2(c) and (d)]. For ZrO<sub>2</sub>(6Y) composite (Fig. 3), at a loading speed of 0.002 mm min<sup>-1</sup>, the number of whisker pullouts is very small, and the fracture surface is rather smooth [Fig. 3(a)]. With increasing loading speed, the effect of whisker pullout increases at both low and high loading speeds in our studies, which are also consistent with the results of fracture toughness.

The large difference in fracture toughness of ZrO<sub>2</sub> (Y<sub>2</sub>O<sub>3</sub>)–SiCw composites due to the Y<sub>2</sub>O<sub>3</sub> content have been explained very clearly in the previous article.<sup>1</sup>

# 3.2 Effect of loading speed on the fracture behaviour of 20 vol% SiCw–Al<sub>2</sub>O<sub>3</sub> composites

The fracture toughnesses of  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> matrix composites reinforced with as-received or acid-leached

 $20 \, \text{vol}\%$  SiCw under different loading speed are summarized in Table 3. It can be seen that the fracture toughnesses of both composites increase with increasing loading speed from  $0.002 \, \text{mm min}^{-1}$  to  $2 \, \text{mm min}^{-1}$ , and the dependence of the composite using as-received SiC whiskers on loading speed is stronger. With increasing loading speed, the difference in fracture toughness between the two types of  $Al_2O_3$  composites disappears, as shown in Fig. 4.

The fracture surfaces of two composites are shown in Figs 5 and 6. For the composite with asreceived SiC whiskers, at a lower loading speed (such as 0.002 mm min<sup>-1</sup>), the fracture surface was rather smooth, and few pulled-out whiskers were observed [Fig. 5(a)]. However, the effect of whisker pullout obviously increased with increasing loading speed [Fig. 5(b)–(d)], resulting in a large increase in fracture toughness when the loading speed was increased from 0.002 mm min<sup>-1</sup> to 2 mm min<sup>-1</sup>. In

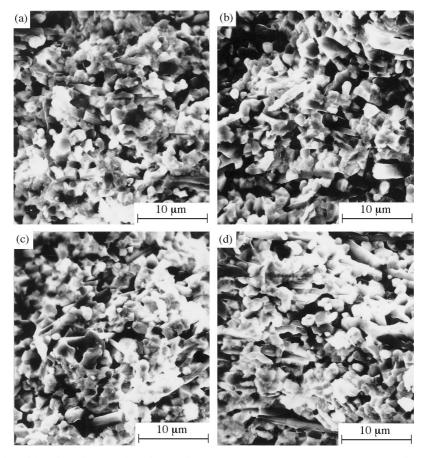


Fig. 2. SEM fractographs of bending fractured surfaces of  $ZrO_2(2Y) + 20vol\%$  SiCw composite under different loading speeds: (a)  $0.002 \, \text{mm min}^{-1}$ ; (b)  $0.02 \, \text{mm min}^{-1}$ ; (c)  $0.2 \, \text{mm min}^{-1}$ ; (d)  $2 \, \text{mm min}^{-1}$ .

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Table 2. Amount of $t \rightarrow m$ transformation of $ZrO_2$ in $ZrO_2(Y_2O_3)+20$ vol% SiCw composites during fracture	of
SENB tests under different loading speeds	

Materials	ZrO <sub>2</sub> (2Y)+20 vol% SiCw				ZrO <sub>2</sub> (6Y)+20 vol% SiCw			
	Loading speed ( $\nu$ ) (mm min <sup>-1</sup> )			Loading speed ( $\nu$ ) (mm min <sup>-1</sup> )				
	0.002	0.02	0.2	2	0.002	0.02	0.2	2
Amount of m-ZrO <sub>2</sub> at the polished surface Amount of m-ZrO <sub>2</sub> at the fracture surface Amount of ZrO <sub>2</sub> t $\rightarrow$ m transformation	26.4 60.5 34.1	26.4 61.9 35.5	26.4 63.5 37.1	26.4 69 42.6	0 0 0	0 0 0	0 0 0	0 0 0

contrast, the composite produced with acid-leached whiskers exhibited substantial crack/microstructure interactions at a loading speed of 0.002 mm min<sup>-1</sup>, with some evidence of whisker pullout [Fig. 6(a)]. Although the effect of whisker pullout also increased with loading speed, this increase was less than that of the composite reinforced with as-received whiskers [Fig. 6(b)–(d)]. This may explain the results of mechanical properties as shown in Fig. 4.

# 3.3 Effect of loading speed on the fracture behaviour of 20 vol% SiCw-20 vol% $ZrO_2$ (2 mol% $Y_2O_3$ )- $AI_2O_3$ composite

The fracture toughnesses of SiCw–ZrO<sub>2</sub>–Al<sub>2</sub>O<sub>3</sub> composites under different loading speed are shown in

Table 4 and Fig. 7. The effect of loading speed on the fracture toughness of the composite is very sensitive at the lower loading speeds (0.002 and 0.02 mm min<sup>-1</sup>), resulting in an increase in fracture toughness from 7.39 MPam<sup>1/2</sup> (0.002 mm min<sup>-1</sup>) to 9.05 MPam<sup>1/2</sup> (0.02 mm min<sup>-1</sup>). Conversely, at the higher loading speed region (0.02 ~ 2 mm min<sup>-1</sup>), the magnitude of toughness enhancement observed is smaller than that at the lower loading speed region, only a 0.45 MPam<sup>1/2</sup> increase in fracture toughness when the loading speed increased from 0.02 mm min<sup>-1</sup> to 2 mm min<sup>-1</sup>.

The XRD results of polished and fractured surfaces of  $SiCw-ZrO_2-Al_2O_3$  composites are shown in Table 5, indicating the existence of dynamic  $t\rightarrow m\ ZrO_2(2Y)$  transformation, which increased

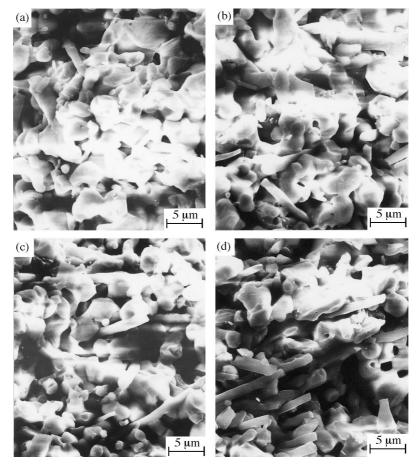


Fig. 3. SEM fractographs of bending fractured surfaces of  $ZrO_2(6Y) + 20vol\%$  SiCw composite under different loading speeds: (a)  $0.002 \text{ mm min}^{-1}$ ; (b)  $0.02 \text{ mm min}^{-1}$ ; (c)  $0.2 \text{ mm min}^{-1}$ ; (d)  $2 \text{ mm min}^{-1}$ .

Fig. 4. Effect of loading speed on fracture toughness of  $Al_2O_3 + 20vol\%$  SiCw composites.

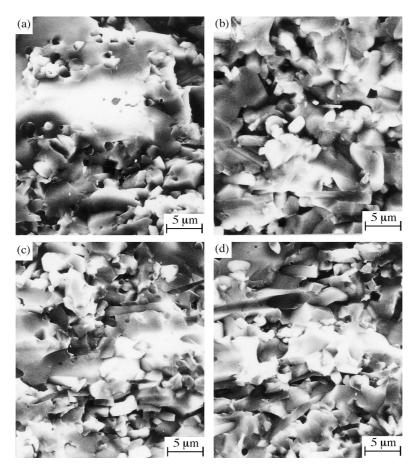


Fig. 5. SEM fractographs of bending fractured  $Al_2O_3 + 20vol\%$  SiCw (as-received) composite under different loading speeds: (a)  $0.002 \text{ mm min}^{-1}$ ; (b)  $0.02 \text{ mm min}^{-1}$ ; (c)  $0.2 \text{ mm min}^{-1}$ ; (d)  $2 \text{ mm min}^{-1}$ .

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zirconia polycrystals (TZP) and zirconia-toughened ceramics (ZTC) materials.<sup>12</sup> Becher<sup>13</sup> concluded that the transformation-toughening contribution to the materials fracture resistance is:

$$\Delta K_{\rm IC}^{\rm T} = A \ B^{1/2} V_{\rm f} \ E_{\rm c} \ e^{\rm T} (K_{\rm IC}^{\rm M} / \sigma_{\rm C}^{\rm T}).$$
 (1)

The terms, A and B are constants related to the stress state,  $V_{\rm f}$  is the fraction of tetragonal phase that transforms,  $E_{\rm C}$  is Young's modulus of the composite,  $e^{\rm T}$  is the transformation strain,  $K_{\rm IC}^{\rm M}$  is the fracture toughness of the matrix and  $\sigma_{\rm C}^{\rm T}$  is the

Table 3. Fracture toughnesses ( $K_{1C}$ , MPam<sup>1/2</sup>) of Al<sub>2</sub>O<sub>3</sub>+20 vol% SiCW composites at different loading speeds

Materials	Loading speed ( $\nu$ ) (mm min <sup>-1</sup> )						
	0.002	0.02	0.2	2			
Al <sub>2</sub> O <sub>3</sub> +received SiCw Al <sub>2</sub> O <sub>3</sub> +acid-leached SiCw	6.02±0.30 8.04±0.55	6.78±0.28 8.68±0.57	8.02±0.45 8.95±0.30	9.00±0.40 9.10±0.45			

Table 4. Fracture toughness ( $K_{IC}$ , MPam<sup>1/2</sup>) of Al<sub>2</sub>O<sub>3</sub>+20 vol% ZrO<sub>2</sub>(2Y)+20 vol% SiCw composites at different loading speeds

Materials	Loading speed (v) (mm min <sup>-1</sup> )				
	0.002	0.02	0.2	2	
Al <sub>2</sub> O <sub>3</sub> +20 vol% ZrO <sub>2</sub> (2Y)+20 vol% SiCw	7.39±0.34	9.05±0.70	9.25±0.55	9.50±0.40	

Table 5. Amount of t→m transformation of ZrO₂ in Al₂O₃+20 vol% ZrO₂(2Y)+20 vol% SiCw composites during fracture of SENB tests under different loading speeds

Loading speed (v) (mm min <sup>-1</sup> )	0.002	0.02	0.2	2
Amount of m-ZrO <sub>2</sub> at the polished surface	68.5	68.5	68.5	68.5
Amount of m-ZrO <sub>2</sub> at the fracture surface	71.2	78.0	79.5	83.4
Amount of ZrO <sub>2</sub> t $\rightarrow$ m transformation	2.7	9.5	11	14.9

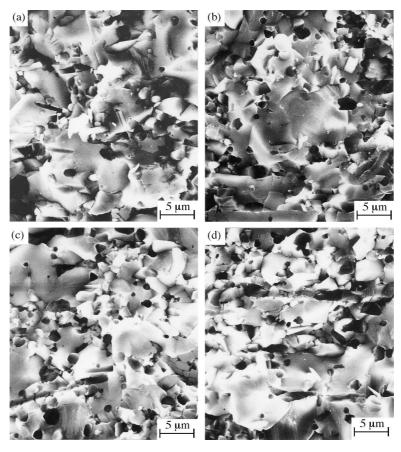


Fig. 6. SEM fractographs of bending fractured  $Al_2O_3 + 20$ vol% SiCw (acid-leached) composite under different loading speeds: (a)  $0.002 \text{ mm min}^{-1}$ ; (b)  $0.02 \text{ mm min}^{-1}$ ; (c)  $0.2 \text{ mm min}^{-1}$ ; (d)  $2 \text{ mm min}^{-1}$ .

Fig. 7. Effect of loading speed on fracture toughness of  $Al_2O_3+20vol\%~ZrO_2(2Y)+20vol\%~SiCw~composite.$ 

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increasing leading speed, the increasing effect of whisker pullout is not obvious, especially at higher loading speeds [Fig. 2(c) and (d)]. In contrast, for ZrO<sub>2</sub>(6Y) composites, the strong interface bonding due to the interface amorphous layer restrains the whisker pullout.<sup>1</sup> This was confirmed by the limited whisker pullout at low loading speed [Fig. 3(a)]. With increasing loading speed, the number of whisker pullouts increased greatly, indicating that whisker pullout is sensitive to loading speed.

For SiCw–Al<sub>2</sub>O<sub>3</sub> composites, the acid-leaching treatment on SiC whiskers decreased the amount of SiO<sub>2</sub> and other impurities on the whiskers surface, <sup>14,15</sup> resulting in a weak interface bonding in the composite. Therefore, for the Al<sub>2</sub>O<sub>3</sub> composite with acid-leached whiskers, even at low loading speeds, the number of whisker pullouts is large [Fig. 5(a)] and is not sensitive to the loading speed [Fig. 5(b)–(d)] which is similar to ZrO<sub>2</sub>(2Y)–SiCw composites. For the composite with as-received whiskers, the strong interface bonding inhibited the whisker pullout. <sup>14</sup> The effect of whisker pullout is sensitive to loading speeds in the range of loading speeds in our study (Fig. 6).

As stated above, the dynamic  $t \rightarrow m ZrO_2$  transformation and effect of whisker pullout increased with increasing loading speed, resulting in the increase in fracture toughness.

# **5 CONCLUSIONS**

1. In the range of loading speed in our study (from 0.002 mm min<sup>-1</sup> to 2 mm min<sup>-1</sup>), the fracture toughnesses of ZrO<sub>2</sub>(2Y), ZrO<sub>2</sub>(6Y), Al<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> + 20 vol% ZrO<sub>2</sub>(2Y) matrix composites reinforced with 20 vol% SiCw increase with increasing loading speed.

- A high loading speed promotes the dynamic t→m ZrO<sub>2</sub>(2Y) transformation during fracturing and hence increases the transformation toughening contribution to the fracture toughnesses of the composites.
- 3. The increase in loading speed promotes the effect of whisker pullout. The characteristic of whisker/matrix interfaces has a strong influence on the effect of whisker pullout on loading speed. The composite with strong interface bonding is more sensitive to loading speed than that with weak interface bonding.

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