

# Microstructure and mechanical properties of $\text{Al}_2\text{O}_3$ – $\text{MgB}_2$ composites

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Received 1 September 2003; received in revised form 24 February 2004; accepted 24 March 2004

Available online 26 June 2004

## Abstract

The microstructure and mechanical properties of  $\text{Al}_2\text{O}_3$ –5wt.%  $\text{MgB}_2$  composites were studied by scanning electron microscopy (SEM) and Vickers hardness measurements. The experiments show that MgO whiskers can grow at temperatures as low as 950 °C. When sintered at 1450 °C, due to the strong vaporization of Mg, MgO and  $\text{MgAl}_2\text{O}_4$  appear around  $\text{Al}_2\text{O}_3$  grains. The microstructure of the  $\text{Al}_2\text{O}_3$ –5wt.%  $\text{MgB}_2$  differs remarkably from  $\text{Al}_2\text{O}_3$  sintered at the same temperature. The fracture toughness of the  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite is 4.0  $\text{MPa m}^{1/2}$  which is slightly higher than for pure  $\text{Al}_2\text{O}_3$  ceramics.

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**Keywords:** B. Microstructure; D. Alumina;  $\text{MgB}_2$

## 1. Introduction

Alumina is a widely used ceramic due to its refractoriness, high hardness, good wear resistance and high chemical stability, however, the brittleness limits its applications. It has been shown that the introduction of a second phase can reduce  $\text{Al}_2\text{O}_3$  grain size and enhance fracture toughness ( $K_{IC}$ ) significantly [1–4]. MgO is a traditional additive to  $\text{Al}_2\text{O}_3$  since it can reduce the sintering temperature and grain size. In early studies on  $\text{Al}_2\text{O}_3$ –MgO composites, MgO was added directly to  $\text{Al}_2\text{O}_3$ . However, the enhancement of the  $K_{IC}$  is not obvious. Recently, it has been reported that nanometer-sized MgO whiskers can grow during the oxidation of  $\text{MgB}_2$  at 900 °C [5,6]. Since the MgO whisker has high melting point, high strength and good plasticity, adding  $\text{MgB}_2$  may be a desirable way to grow MgO whiskers in  $\text{Al}_2\text{O}_3$  and enhance its toughness. In this work, we investigate an  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite and discuss the influence of adding  $\text{MgB}_2$  on the microstructure and mechanical properties.

## 2. Experimental

$\text{MgB}_2$  was synthesized by vacuum encapsulation. A stoichiometric mixture of commercial Mg (purity > 99%, 100–200 mesh) and B powder (purity > 96%, average particle size  $\sim 2 \mu\text{m}$ ) was ground in an agate mortar, then pressed into pellets and put into a quartz tube which was vacuum encapsulated. The sample was heated rapidly to 850 °C and held at this temperature for 2 h. The obtained  $\text{MgB}_2$  sample was checked by X-ray diffraction (XRD) and scanning electron microscopy (SEM).  $\text{MgB}_2$  powder was heated in a thermal-analyzer to 900 °C and kept at this temperature for 3 h, then examined by SEM.

$\text{MgB}_2$  powder was added into  $\text{Al}_2\text{O}_3$  powder (purity > 99%, average particle size 1.4  $\mu\text{m}$ ) at a weight ratio 5:95, and then mixed thoroughly and pressed into pellets under 10 mPa. The pellets were put into the MgO crucible and sintered at a heating rate of 5–10 °C  $\text{min}^{-1}$  in an electric furnace and kept at the final temperature (850, 950 and 1450 °C, respectively) for 1 h. Pellets of pure  $\text{Al}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$ –5% MgO were also sintered at the same conditions in order to comparing their microstructures with  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite.

The microstructure was studied with a SEM equipped with X-ray energy dispersive analysis (EDS). The surface

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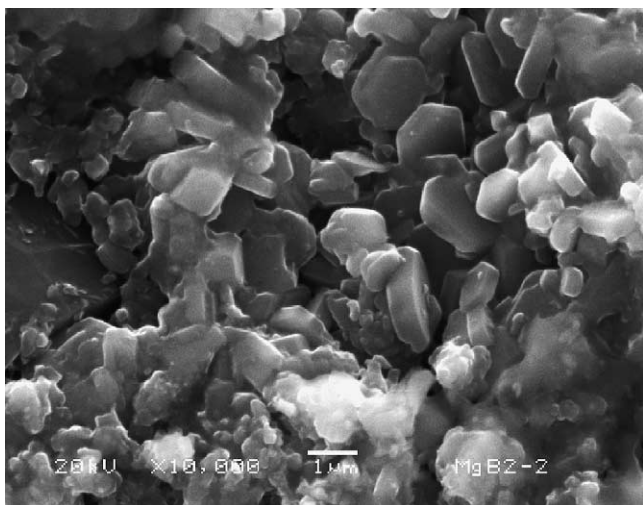


Fig. 1. Microstructure of  $\text{MgB}_2$  made by vacuum encapsulation.

of the pellets was burnished by SiC sand paper, and then polished by diamond cream to get smoothness. Vickers diamond hardness indentation at a load of 9.8 N and loading time of 10 s was used to test the mechanical properties, and fracture toughness was calculated by using the average length of radial cracks and the Liang's equation [7].

### 3. Results and discussion

Fig. 1 shows the microstructure of the synthesized  $\text{MgB}_2$ . It can be seen that many grains show hexagonal shape due to the hexagonal crystal structure of  $\text{MgB}_2$ . XRD pattern shows that the sample prepared by vacuum encapsulation has a pure phase of  $\text{MgB}_2$  with a thin impurity of  $\text{MgO}$  that may be caused by the thin residual oxygen left in the quartz tube. After heating at  $900^\circ\text{C}$  for 3 h in air,  $\text{MgO}$  whiskers with diameters about 10–100 nm appear on the grain surface in the oxidation process of  $\text{MgB}_2$ , as Fig. 2 shows. The

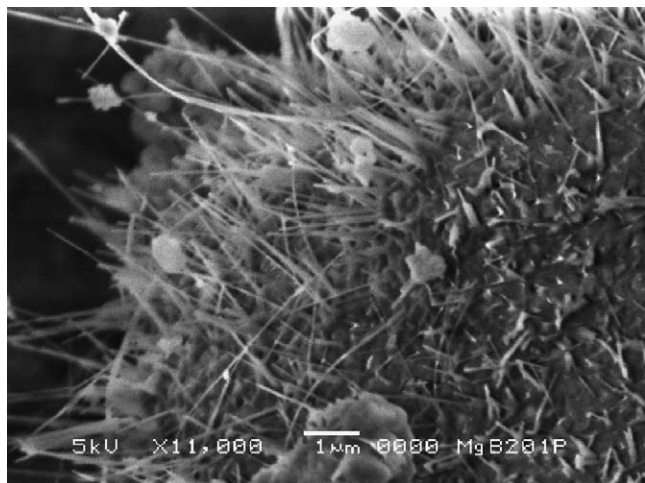


Fig. 2.  $\text{MgO}$  whiskers growing from oxidation of pure  $\text{MgB}_2$ .



Fig. 3. Micrograph of the  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composites sintered at  $850^\circ\text{C}$ .

growth of the whisker is caused by the reaction of oxygen with the vapor of  $\text{Mg}$  [8]. When  $\text{MgB}_2$  is heated in air or in oxygen,  $\text{MgO}$  can be formed by two ways. In the first way, oxygen diffuses into the grain of  $\text{MgB}_2$  and reacts with  $\text{Mg}$  to form  $\text{MgO}$ . In the second way,  $\text{Mg}$  evaporates first and then reacts with oxygen on the grain surface to form  $\text{MgO}$ . The already formed  $\text{MgO}$  on the grain surface will serve as a seed crystal (as can be seen from Fig. 2, there are many small prominences on the grain surface) and then  $\text{MgO}$  will grow continuously on the seed to form long thin  $\text{MgO}$  whiskers.

When  $\text{MgB}_2$  is added into  $\text{Al}_2\text{O}_3$  and sintered at 850, 950 and  $1450^\circ\text{C}$ , its microstructure is remarkably different from that of the pure  $\text{MgB}_2$  after oxidation. Fig. 3 shows the micrograph of  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  sintered at  $850^\circ\text{C}$ . Comparing with Fig. 2, we can see that the diameter of the whisker becomes thicker and almost does not vary when the whisker grows longer. It can also be seen that all whiskers in  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  sintered at  $850^\circ\text{C}$  have approximately the same diameter of about 200 nm. On the other hand, whiskers grown from pure  $\text{MgB}_2$  are relatively thin. In addition, from Fig. 2, we can find that some whiskers become thinner gradually when they grow longer. The other obvious difference is that the whiskers grown in  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite have bamboo shape and the number of whiskers in  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite is less than for the pure  $\text{MgB}_2$ .

It is well-known that most of the whiskers can only grow in the vapor phase. Therefore, growth environment, such as temperature, time, atmosphere, and impurity concentration have very important effects on the diameter, the length and the shape of the whiskers. In the above two experiments of growing  $\text{MgO}$  whiskers from  $\text{MgB}_2$ , temperature and heating time are similar, so the difference of the whisker shape is caused by the difference of oxygen atmosphere and impurities. When  $\text{MgB}_2$  is put into  $\text{Al}_2\text{O}_3$  powder and pressed into pellets, it is difficult for the oxygen to enter the sample. This will result in oxygen insufficiency in the sample that depresses the oxidation process of  $\text{MgB}_2$  and affects

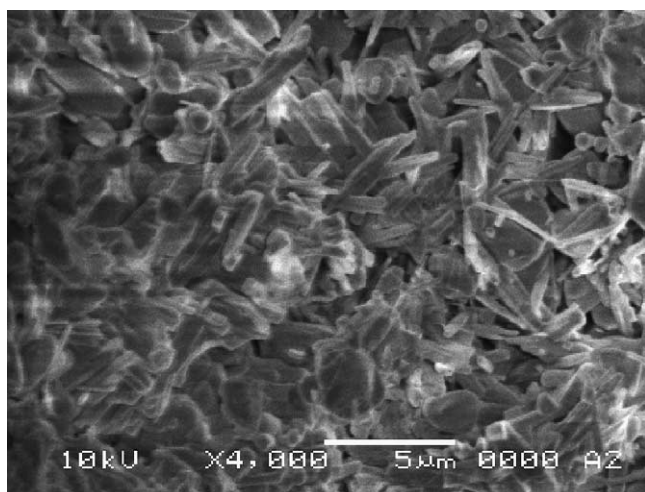


Fig. 4. Micrograph of the  $\text{Al}_2\text{O}_3$ -5%  $\text{MgB}_2$  composites sintered at 950 °C.

the MgO whisker shape. In the case of oxygen deficiency, in MgO crystal seed formed on the grain surface dislocations may be generated, and the bamboo node of the whisker may be the boundary of a twin-crystal. If sintering temperature increases to 950 °C, vaporization and oxidation of Mg in  $\text{MgB}_2$  will become very strong. The bamboo node shape MgO whiskers grow up and become long thin rods with sub-micron size as shown in Fig. 4.

When  $\text{Al}_2\text{O}_3$ - $\text{MgB}_2$  samples are sintered at 1450 °C, their microstructure changes remarkably from samples sintered at 850 and 950 °C. Fig. 5 shows the micrograph of  $\text{Al}_2\text{O}_3$ -5%  $\text{MgB}_2$  heated at 1450 °C, which indicates that most of the grains in the sample grow into columnar shape grain. The oxidation of  $\text{MgB}_2$  plays an important role in the formation of columnar shape grains. At high temperature, Mg elements vaporize almost and Mg vapor can oxidize to form MgO and  $\text{MgAl}_2\text{O}_4$  around  $\text{Al}_2\text{O}_3$  grains. This causes formation of columnar shape grains. Without  $\text{MgB}_2$  additive the columnar shape grain cannot be formed. Fig. 6 shows

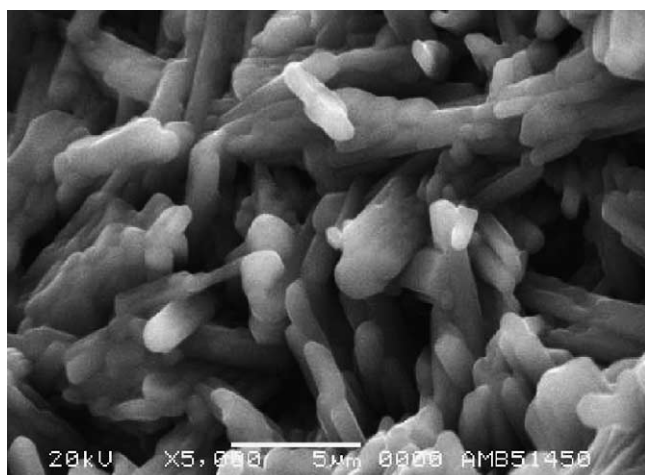


Fig. 5. Micrograph of the  $\text{Al}_2\text{O}_3$ -5%  $\text{MgB}_2$  composites sintered at 1450 °C.

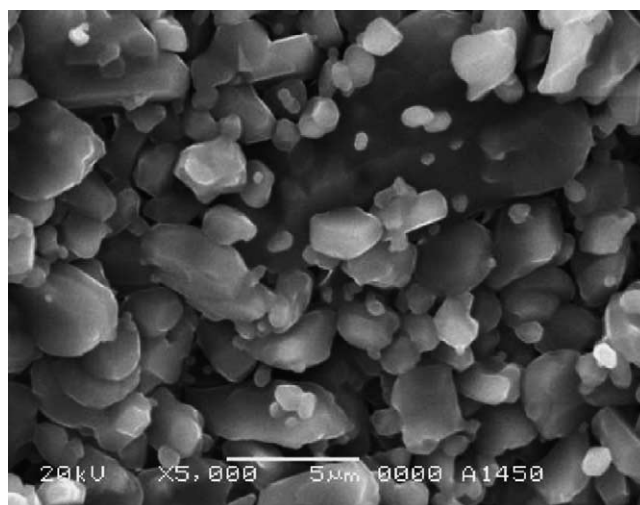


Fig. 6. Micrograph of the alumina without  $\text{MgB}_2$  additive sintered at 1450 °C.

the micrograph of monolithic  $\text{Al}_2\text{O}_3$  ceramic without  $\text{MgB}_2$  additive; it can clearly be seen that there are no columnar shape grains. Therefore, it is the addition of  $\text{MgB}_2$  that helps the formation of columnar shape grains in the  $\text{Al}_2\text{O}_3$ -5%  $\text{MgB}_2$  composites.

It is well-known that the addition of MgO can promote liquid phase sintering of  $\text{Al}_2\text{O}_3$  ceramics, thus resulting in a uniform microstructure and reducing the anisotropy of alumina [9]. However, the effect of adding  $\text{MgB}_2$  into  $\text{Al}_2\text{O}_3$  is not as the same as adding MgO directly. Fig. 7 shows the micrograph of  $\text{Al}_2\text{O}_3$  with 5% MgO additive. The liquid phase sintering effect is obvious, but the columnar shape grains are rare comparing with the samples with  $\text{MgB}_2$  additive. The main difference between  $\text{MgB}_2$  and MgO additive may be explained as follows. When adding MgO directly, only liquid phase sintering effect exists and the vaporization of Mg is difficult due to the high stability of MgO at high

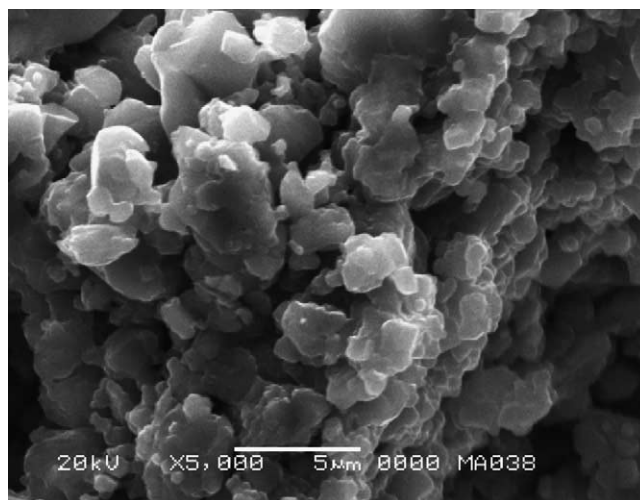


Fig. 7. Micrograph of the alumina with 5% MgO additive sintered at 1450 °C.



Table 1  
Mechanical properties of  $\text{Al}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  ceramics

Specimen	Density ( $\text{g cm}^{-3}$ )	Hardness ( $H_v$ ) GPa	Fracture toughness ( $K_{IC}$ ) $\text{mPa m}^{1/2}$
$\text{Al}_2\text{O}_3$ –5% $\text{MgB}_2$	3.58	2.09	4.0
$\text{Al}_2\text{O}_3$	3.62	2.26	3.3

temperature. While in the case of adding  $\text{MgB}_2$ , Mg can vaporize easily and form a uniform distribution in the specimen. When Mg vapor meets oxygen, MgO and/or  $\text{MgAl}_2\text{O}_4$  will grow on the boundary of  $\text{Al}_2\text{O}_3$  grain and a certain direction may be preferred in the continuous growth, thus columnar shape grains are formed. It was pointed out [10,11] in pure  $\text{Al}_2\text{O}_3$  abnormal growth of grain is not observed. However, with the help of some additive (such as  $\text{Fe}_2\text{O}_3$ ,  $\text{TiO}_2$ , and  $\text{MnO}_2$  [12]) some liquid phase can be formed resulting in abnormal growth of grains, i.e., in some directions the growth rate of grains is faster than other directions. Our experiment shows that  $\text{MgB}_2$  is a much effective additive that helps abnormal growth and formation of columnar shape grains.

It is believed that the formation of columnar shape grains can increase the fracture toughness. Table 1 compares some mechanical properties of  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  and  $\text{Al}_2\text{O}_3$  composites, and shows that their hardness and density are similar, but the fracture toughness of  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite increases slightly.

The increase of fracture toughness of the  $\text{Al}_2\text{O}_3$ –5%  $\text{MgB}_2$  composite is mainly due to two factors, i.e., (i) liquid phase sintering and (ii) the formation of columnar shape grains. At high temperature,  $\text{MgB}_2$  is oxidized strongly and can form a uniform Mg vapor around  $\text{Al}_2\text{O}_3$  grains, which is a much effective way of liquid phase sintering and is better than adding MgO directly. The formation of columnar shape grains can also enhance fracture toughness because columnar shape grains can form bridge that increases the fracture resistance.

#### 4. Conclusions

By controlling the environmental condition, such as temperature and oxygen atmosphere, MgO whiskers with different shape can be obtained by adding  $\text{MgB}_2$  to  $\text{Al}_2\text{O}_3$ .

When the sample is sintered to  $1450^\circ\text{C}$ , due to the strong vaporization of Mg, MgO and/or  $\text{MgAl}_2\text{O}_4$  will grow around  $\text{Al}_2\text{O}_3$  grains giving rise to columnar shape grains. The fracture toughness of the  $\text{Al}_2\text{O}_3$ – $\text{MgB}_2$  composites is higher than that of pure  $\text{Al}_2\text{O}_3$ . The advantage of the  $\text{MgB}_2$  additive compared to MgO is that the  $\text{MgB}_2$  can form a uniform Mg vapor, help the formation of columnar shape grains and increase the fracture toughness of  $\text{Al}_2\text{O}_3$ – $\text{MgB}_2$  composite.

#### Acknowledgements

This work was supported by a Fund of Natural Science of Henan Province, China.

#### References

- [1] Y. Ji, J.A. Yeomans, Processing and mechanical properties of  $\text{Al}_2\text{O}_3$ –5 vol.% Cr nanocomposites, *J. Eur. Ceram. Soc.* 22 (2002) 1927–1936.
- [2] C.T. Fu, J.M. Wu, A.K. Li, Microstructure and mechanical properties of  $\text{Cr}_2\text{O}_3$  prismatic reinforced  $\text{Al}_2\text{O}_3$  matrix composites, *J. Mater. Sci.* 29 (1994) 2671–2677.
- [3] J.L. Shi, T.S. Yan, Densification and microstructure development of alumina/Y-TZP composite powder (Y-TZP-rich) compacts, *J. Eur. Ceram. Soc.* 15 (1995) 363–369.
- [4] Y. Zeng, D. Jiang, Fabrication and properties of laminated  $\text{Al}_2\text{O}_3/\text{TiC}$  composites, *Ceram. Int.* 27 (2001) 597–602.
- [5] D. Yang, H. Sun, H. Lu, Y. Guo, X. Li, X. Hu, Experimental study on the oxidation of  $\text{MgB}_2$  in air at high temperature, *Supercond. Sci. Technol.* 16 (2003) 576–581.
- [6] D.G. Hinks, J.D. Jorgensen, H. Zheng, S. Short, Synthesis and stoichiometry of  $\text{MgB}_2$ , *Physica C* 382 (2002) 166–176.
- [7] K.M. Liang, G. Orange, G. Fantozzi, Evaluation of indentation fracture toughness of ceramics materials, *J. Mater. Sci.* 25 (1990) 207–214.
- [8] Y. Chen, J. Li, Y. Han, X. Yang, J. Dai, The effect of Mg vapor source on the formation of MgO whiskers and sheets, *J. Cryst. Growth* 245 (2002) 163–170.
- [9] S.T. Bennison, M.P. Harmer, Effect of a magnesia solute on surface diffusion in sapphire and the role of magnesia in the sintering of alumina, *J. Am. Ceram. Soc.* 73 (1990) 833–857.
- [10] H. Song, R.L. Cobel, S. Baik, Origin and growth kinetics of platelike abnormal grains in liquid-phase-sintered alumina, *J. Am. Ceram. Soc.* 73 (1990) 2077–2085.
- [11] I. Bae, S. Baik, Abnormal grain growth of alumina, *J. Am. Ceram. Soc.* 80 (1997) 1149–1156.
- [12] J. Tartai, G.L. Messing, Anisotropic grain growth in  $\alpha\text{-Fe}_2\text{O}_3$ -doped alumina, *J. Eur. Ceram. Soc.* 17 (1997) 719–725.