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# Short communication

# Effect of Ta<sub>2</sub>O<sub>5</sub> in (Ca, Si, Ta)-doped TiO<sub>2</sub> ceramic varistors

Shaohua Luo a,b,\*, Zilong Tang a, Jianying Li c, Zhongtai Zhang a

<sup>a</sup> State Key Laboratory of New Ceramics and Fine Processing, Department of Materials Science and Engineering, Tsinghua University, Beijing 100084, China

<sup>b</sup> Department of Materials Science and Engineering, Northeastern University at Qinhuangdao Branch, Qinhuangdao, 066004, China <sup>c</sup> Multi-Disciplinary Materials Research Center, Xi'an Jiaotong University, Xi'an 710049, China

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#### **Abstract**

TiO<sub>2</sub> varistors doped with 0.2 mol% Ca, 0.4 mol% Si and different concentrations of Ta were obtained by ceramic sintering processing at 1350 °C. The effect of Ta on the microstructures, nonlinear electrical behavior and dielectric properties of the (Ca, Si, Ta)-doped TiO<sub>2</sub> ceramics were investigated. The ceramics have nonlinear coefficients of  $\alpha = 3.0$ –5.0 and ultrahigh relative dielectric constants which is up to  $10^4$ . Experimental evidence shows that small quantities of Ta<sub>2</sub>O<sub>5</sub> improve the nonlinear properties of the samples significantly. It was found that an optimal doping composition of 0.8 mol% Ta<sub>2</sub>O<sub>5</sub> leads to a low breakdown voltage of 14.7 V/mm, a high nonlinear constant of 4.8 and an ultrahigh electrical permittivity of  $5.0 \times 10^4$  and tg  $\delta = 0.66$  (measured at 1 kHz), which is consistent with the highest and narrowest grain boundary barriers of the ceramics. In view of these electrical characteristics, the TiO<sub>2</sub>–0.8 mol% Ta<sub>2</sub>O<sub>5</sub> ceramic is a viable candidate for capacitor–varistor functional devices. The characteristics of the ceramics can be explained by the effect and the maximum of the substitution of Ta<sup>5+</sup> for Ti<sup>4+</sup>. © 2007 Elsevier Ltd and Techna Group S.r.l. All rights reserved.

Keywords: TiO2 varistor; Tantalum oxide; Microstructure; Electrical property

# 1. Introduction

Varistors are known for their application as surge protection devices in power system and also in electronic circuits. Up to now, ZnO-based varistors have been extensively studied. The recent trend in electrical appliance design requires varistors that contain more functions and have a relatively low breakdown voltage, which facilitate the denser integrated circuits. Moreover, the low permittivity of ZnO varistor weakens its ability to absorb the sparks, and therefore restricts its application in the low voltage circuit. The  $TiO_2$ -based varistor has attracted much interest in recent years. Yan and Rhodes [1] first reported that (Nb, Ba)-doped  $TiO_2$  ceramics had useful varistor properties with  $\alpha$  of about 4. Then  $TiO_2$  ceramics with different dopants added were developed such as: (Pb, Nb)- $TiO_2$  [2], (Ba, Bi, Nb)- $TiO_2$  [3], (Cr, Nb)- $TiO_2$  [4], (Y, Nb)- $TiO_2$  [5] and (Ca, Si, Ce,

Nb)-TiO<sub>2</sub> [6,7]. As above, the 5+ valences Nb is commonly used as the dopant to decrease the lattice resistivity of  $\text{TiO}_2$  in most papers. Divalence or trivalence cations with large ionic radii, e.g., alkaline metal segregate at the  $\text{TiO}_2$  grain boundaries. The addition of Bi or Pb results in the formation of low-melting component, which redound to create the efficient boundary barrier layer.

Although  ${\rm Ta}^{5+}$  with a valence 5+ and similar ionic radii as  ${\rm Ti}^{4+}$ , which can donate conduction electrons and have a reasonable solubility in the Ti sublattice that of Nb<sup>5+</sup>, the system of Ta-doped TiO<sub>2</sub> had been few studied. The Ta<sub>2</sub>O<sub>5</sub> is also applied in other varistor system such as SnO<sub>2</sub>-based varistors [8]. Only mone-doped Ta-TiO<sub>2</sub> [9], binary doped Ta-TiO<sub>2</sub>: M (M = Ba [10], Ca [11,12]) ceramics had been studied. The detailed study of system of ternary-doped Ta-TiO<sub>2</sub> has not been reported yet. Meantime, volatility of low-melting component from Bi<sub>2</sub>O<sub>3</sub> and PbO during high-temperature sintering causes problems in reproducing high-quality electronic ceramics. So the SiO<sub>2</sub>, a stable compound can be used to form low-melting component. In this paper, the nonlinear electrical behavior and dielectric properties of (Ca, Si, Ta)-doped TiO<sub>2</sub> ceramics were studied. In particular, the effects of

<sup>\*</sup> Corresponding author at: State Key Laboratory of New Ceramics and Fine Processing, Department of Materials Science and Engineering, Tsinghua University, Beijing 100084, China. Tel.: +86 1062772623; fax: +86 1062783046. E-mail address: luosh03@mails.tsinghua.edu.cn (S. Luo).

Ta dopant on the nonlinear electrical behavior and dielectric properties of the ceramics were also investigated.

# 2. Experimental

Traditional ceramic process was used to prepare the  $TiO_2$  varistor ceramics. The starting chemicals in the present study were reagent grade  $TiO_2$ ,  $Ta_2O_5$ ,  $SiO_2$  and  $CaCO_3$ . The investigated compositions contained cation ratio of Ti:Si:Ca:Ta = 100:0.4:0.2:x with x = 0.2, 0.4, 0.6, 1.0, 1.6, 2.0. The chemicals were weighted according to the stoichiometric amount of final composite. The powder mixture was wet ball-milled in a polyethylene bottle with  $ZrO_2$  balls for 4 h in deionized water. The milled mixtures were dried, granulated and pressed into disks at 150 MPa, with diameter of 10 mm and thickness of 1.2 mm. The disks were sintered at 1350 °C for 4 h in air, and then cooled down in furnace. For electrical measurements, silver electrodes were prepared on both surfaces of the sintered pellets at 570 °C for 20 min.

The varistor voltage  $V_{0.1 \text{ mA}}$  and  $V_{1 \text{ mA}}$  were measured by using MY-4C meter.  $\alpha$  was calculated by the following formula:

$$\alpha = \frac{\log(I_2/I_1)}{\log(V_2/V_1)} = \frac{1}{\log(V_{1 \text{ mA}}/V_{0.1 \text{ mA}})}$$
(1)

The relative dielectric constant  $\epsilon$  and loss  $\tan \delta$  were measured with an LCR meter (2-3532-50 LCR HITESTER) in the frequency 1 kHz. The microstructures of the sintered pellets and grain size were observed with SEM (JSM-6460LV) technology. The grain sizes were determined by the intercept method.

#### 3. Results and discussion

The X-ray powder diffraction patterns of all samples with different concentrations of Ta are similar (Fig. 1). The analysis of the patterns indicates that no other phase except  $\text{TiO}_2$  rutile phase exists in the samples. Therefore, CaO and  $\text{Ta}_2\text{O}_5$  should form a solid solution in  $\text{TiO}_2$  when the disks were sintered. If

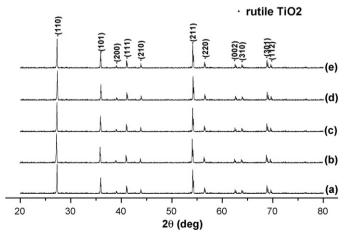


Fig. 1. X-ray powder diffraction patterns of samples doped with different concentrations of Ta: (a) x = 0.2; (b) x = 0.4; (c) x = 0.6; (d) x = 1.0; (e) x = 2.0.

the dopants are dissolved into rutile lattice, the defect equations can be expressed as follows using Kroger–Vink notation:

$$Ta_2O_5 \stackrel{TiO_2}{\longleftrightarrow} 2Ta_{Ti}^{\bullet} + 2e\prime + 4O_O^X + \frac{1}{2}O_2 \uparrow$$
 (2)

$$CaO \stackrel{TiO_2}{\longleftrightarrow} Ca_{Ti} \prime \prime + V_O^{\bullet \bullet} + O_O^X$$
 (3)

Since Ta has an ionic radius similar to that of Ti, it easily dissolves into the  $TiO_2$  lattice. According to Eq. (2), the dissolution of Ta into  $TiO_2$  grains will introduce free electrons and positive charge defects ( $Ta_{Ti}^{\bullet}$ ). Due to the generation of electrons, the free electron concentration in the  $TiO_2$  grains is increased. Thus, the resistivity of  $TiO_2$  grains is decreased. On the other hand, the dissolution of Ca into  $TiO_2$  lattice creates one oxygen vacancy and negatively charged defect ( $Ca_{Ti}''$ ) according to Eq. (3). Comparing  $Ti^{4+}$  (0.61 Å) with  $Ca^{2+}$  (1.01 Å), the  $Ca^{2+}$  with a larger ionic radius and a lower valence prefers to segregate at grain boundaries in order to relieve the great elastic strain energy caused by ionic radius mismatch. So Ca has a very low solubility in the  $TiO_2$  grains. Hence, only a small quantity of Ca added dissolves into  $TiO_2$  grains while most of Ca segregate at grain boundaries.

The typical SEM micrograph of the (Ca, Ta)-doped  $\text{TiO}_2$  varistor is shown in Fig. 2, which is characterized by heterogeneous grains with average grain size ( $d_g$ ) of several microns. Clearly, there is no apparent second phase observed in the SEM micrograph. The average grain size ( $d_g$ ) of each sample, calculated by the intercept method, slowly decreases from 3.77 to 2.08  $\mu$ m with increasing of the doping concentration of Ta from 0.2 to 2.0 mol%.

The  $V_{1 \text{ mA}}$  and  $\alpha$  curves for samples doped with different concentrations of Ta are given in Fig. 3. It can be seen from Fig. 3 that  $V_{1 \text{ mA}}$  decreases sharply with increase of  $Ta_2O_5$ , which is similar to the general reported results. In this process, free electrons can be released from the substitution of  $Ti^{4+}$  with  $Ta^{5+}$  when the Ta addition varies from 0.2 to 1.6 mol%. It is also found that the nonlinear coefficient  $\alpha$  increases from 3.2 to 4.8 at the same time. Thus, the substitution of  $Ti^{4+}$  with  $Ta^{5+}$  cannot only decrease the grain resistance by more free electrons, but

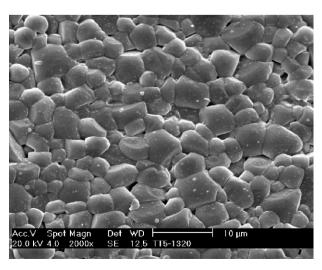


Fig. 2. Typical SEM micrograph of samples.

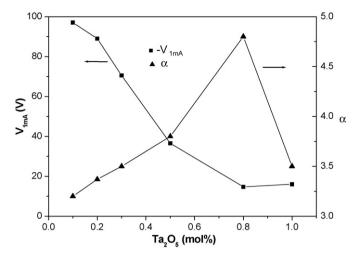


Fig. 3.  $V_{1 \text{ mA}}$  and  $\alpha$  vs. the content of Ta<sub>2</sub>O<sub>5</sub> dopant.

also leads to a high grain boundary barrier and, consequently, high  $\alpha$  value. The sample doped with 0.8 mol%  $Ta_2O_5$  exhibits the highest nonlinear coefficient and the lowest breakdown voltage. However, the substitution of  $Ta^{5+}$  for  $Ti^{4+}$  exists a maximum value. When the dopant  $Ta_2O_5$  exceeds 0.8 mol%, the nonlinear characteristic  $\alpha$  rapidly drops from 4.8 to 3.5. As regards to  $V_{1 \text{ mA}}$ , it rises slightly from 14.7 to 16. The superfluous  $Ta^{5+}$ , which cannot substitute  $Ti^{4+}$  further, will segregate to grain boundary interface. The segregation of  $Ta^{5+}$  blocks the formation and transportation of  $e^-$  and other defects, which will play an effect on the properties of the  $TiO_2$ -based ceramics contrary to the substitution of  $Ta^{5+}$  for  $Ti^{4+}$ . The increasing of Ta addition results in the deterioration of nonlinear property and rising of  $V_{1 \text{ mA}}$ .

Fig. 4 shows the relative dielectric constant ( $\varepsilon_{\gamma}$ ) and tan  $\delta$  with different concentrations of Ta. Obviously, the  $\varepsilon_{\gamma}$  value and tan  $\delta$  exhibit similarly peak-like tendency with increasing of Ta content. It is shown that the 0.8 mol% Ta<sub>2</sub>O<sub>5</sub> specimen possesses two highest values,  $4.99 \times 10^4$  for  $\varepsilon_{\gamma}$  and 0.66 for tan  $\delta$ . Higher effective relative dielectric constant and dissipation factor can be attributed to significant electronic conduction. The low-resistivity surface layer increases the dissipation

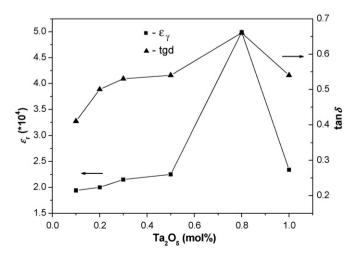


Fig. 4. Effective relative dielectric constant and tan  $\delta$  vs. the content of  $Ta_2O_5$  dopant.

factor of the sample especially in the low-frequency 1 kHz region where electron motion is possible. It is also believed that the increase of the effective relative dielectric constant in the low frequency region usually results from conduction loss. When the concentration of  $Ta_2O_5$  dopant is up to 0.8 mol%, the rising tendency obtains its maximum value.

#### 4. Conclusions

The Ta dopant has significant effects on the nonlinear electrical behavior and dielectric properties of the (Ca, Si, Ta)-doped  $\text{TiO}_2$  varistors. An optimal doping composition of (0.8Ta, 0.4Si, 0.2Ca)-doped  $\text{TiO}_2$  was obtained with a low  $V_{1\text{ mA}}$  of 14.7 V, a high nonlinear constant of 4.8, an ultrahigh electrical permittivity of  $4.99 \times 10^4$  and higher dissipation factor 0.66 (measured at 1 kHz), which can be used as capacitor–varistor ceramics. Deviations from this doping composition, towards either higher or lower  $\text{Ta}_2\text{O}_5$  contents, cause deterioration of the I-V nonlinear characteristics. There is a correlation between the nonlinear electrical and dielectric properties of the (Ca, Si, Ta)-doped  $\text{TiO}_2$  varistors.

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