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Effects of SrTiO₃ additives on the structure and microwave dielectric properties of Ba_{4.2}Sm_{9.2}Ti₁₈O₅₄ ceramics

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Abstract

The effects of SrTiO₃ additives on the microstructure and the dielectric properties of $Ba_{4.2}Sm_{9.2}Ti_{18}O_{54}$ (BST) materials have been investigated. The microstructure of BST doped with SrTiO₃ was analyzed using X-ray diffraction (XRD), scanning electron microscopy (SEM) and electron probe microanalyzer (EPMA). The XRD, SEM and EPMA results showed that small amounts of SrTiO₃ (less than 4 wt.%) could be accommodated in BST while a secondary metatitanate phase appeared in the samples with 8 wt.% SrTiO₃ added, the addition of SrTiO₃ increased the lower solubility limit (x values) of $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$. The relative permittivities and the TC_f values showed an approximately linear increase with increasing additions of SrTiO₃. It was observed that near zero TC_f values could be achieved with the addition of SrTiO₃ to BST ceramics. With 4 wt.% SrTiO₃ addition and sintered at 1360 °C for 2 h, BST ceramics exhibited excellent dielectric properties: $\varepsilon_r = 81.2$, $Q_f = 8470$ GHz and $TC_f = -1.5$ ppm/°C.

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1. Introduction

For over 30 years, dielectric ceramics based on BaO-Ln₂O₃-TiO₂ (where Ln are lanthanide elements) have been focused on because of their excellent microwave properties. A combination of a high-dielectric constant, low-dielectric loss and high-temperature stability of the permittivity makes them very important for the applications in microwave communication devices. The earliest work on these systems is credited to Bolton [1] and Kolar et al. [2]. The crystal structure of these ceramics belongs to the tungsten bronze structural family and consists of a three-dimensional framework of corner-sharing perovskite-like TiO₆ octahedra. Linked at the corners in a complex way they yield three types of openings: large pentagonal sites (A₂-sites), tetragonal sites (A₁-sites) and small triangular sites. The conventional formula Ba_{6-3x}Ln_{8+2x}Ti₁₈O₅₄ has been accepted for this system and the basic structural formula is [A₁]₁₀[A₂]₄Ti₁₈O₅₄ [3–5]. According to Ohsato [6] the lanthanide cations occupy

the tetragonal channels, Ba²⁺ cations fill the pentagonal channels and the remaining Ba ions share the tetragonal channels with the lanthanides. The triangular channels are empty. The lower solubility limit (x) of $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ is 0.3 [7]. High permittivity of 78 and high $Q_f = 9720 \text{ GHz}$ have been reported when x = 0.6 and Ln = Sm [8]. However, this system has a high-negative TC_f of about $-10 \text{ ppm}/^{\circ}C$, thus a lot of work has been done to tune TCf to near zero including partial substitution of Nd3+/La3+ with Sm3+ in the rhombic channels [9,10]. Substitution of Sr²⁺ with Ba²⁺ has also been found to be very helpful in stabilizing the low-TC_f behavior [11–13], but the Q_f values decreased if a near zero TC_f value is needed. In the present study, SrTiO₃ ceramics have been used as additives in an effort to tune the TCf of Ba_{4.2}Sm_{9.2}Ti₁₈O₅₄ (BST) ceramics to near zero. Unlike BST ceramics with a tungsten bronze structure, SrTiO₃ ceramics feature perovskite structure. Wise et al. [14] reported that the SrTiO₃ ceramics have permittivities of about 290 and highpositive TC_f values of about 1647 ppm/°C. Therefore, it is possible using SrTiO₃ as additives to improve the TC_f values of BST. In the present work, the effects of SrTiO₃ additives on the structural and microwave dielectric properties of BST have been investigated.

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2. Experimental procedures

Samples were prepared by the conventional solid-state reaction method. Reagent grade BaCO3, Sm2O3, TiO2 and SrTiO₃ with the purity of over 99.5 wt.% were used as raw materials. The starting materials were mixed according to the stoichiometries of Ba_{4.2}Sm_{9.2}Ti₁₈O₅₄ using deionised water and zirconia milling media. The mixtures were calcined at 1250 °C for 2 h. To form the mixed compositions, controlled amounts of SrTiO₃ were added to the calcined BST. The mixed powders were then remilled for 3 h and dried. Then the dried powders with PVA binders were pressed into disks 15 mm in diameter and 7-10 mm in thickness under a pressure of 100 MPa. Samples were sintered at 1340–1380 °C for 2 h in an air atmosphere. The bulk densities of the samples were measured by Archimedes' method. X-ray diffraction (XRD) experiments were performed on bulk samples using a Philips X'Pert PRO diffractometer operating at 40 kV, 40 mA with a fixed divergence slit of 0.9570°. A continuous scan was carried out using monochromatic Cu Kα radiation filtered through a Ni foil with 2θ angles in the range of $10-70^{\circ}$ and a step size of 0.02°. The microstructure of the as-sintered surface was studied using field emission scanning electron microscope (FE-SEM) model FEI Sirion 200. The selected samples were ground on 1200 grade SiC paper, polished on diamond paste to 0.5 µm and thermally etched at 1260 °C for 10 min. The composition analyses of the thermally etched samples were performed by electron probe microanalyzer (EPMA) model JEOL JXA-8800R. The dielectric properties were measured using dielectric post-resonator technique developed by Hakki and Coleman [15]. The temperature coefficient of resonant frequency (TC_f) was also measured by the same method in the temperature range of 25–75 °C.

3. Results and discussion

The variation of bulk densities as a function of the addition of $SrTiO_3$ and sintered at temperatures between 1340 and 1380 °C for 2 h are shown in Fig. 1. The densities of the sintered ceramics were significantly affected by the addition amounts of $SrTiO_3$ and sintering temperatures. Addition of

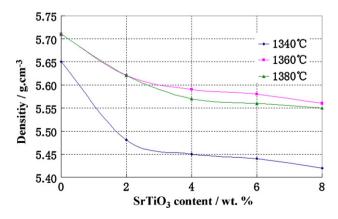
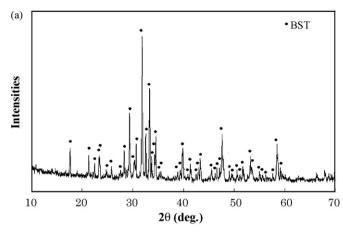


Fig. 1. The variation of bulk densities with amounts of $SrTiO_3$ added into BST sintered at different temperature for 2 h.



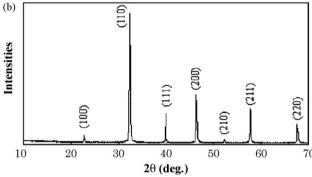


Fig. 2. XRD patterns of BST calcined at 1250 $^{\circ}$ C for 2 h and SrTiO₃ powder: (a) BST and (b) SrTiO₃.

SrTiO₃ to BST ceramics causes a marked reduction in density. With the increasing addition amounts of SrTiO₃, the densities of the ceramics sintered at 1360 °C decreased from 5.71 g/cm³ for pure BST to 5.56 g/cm³ for the samples with the addition of

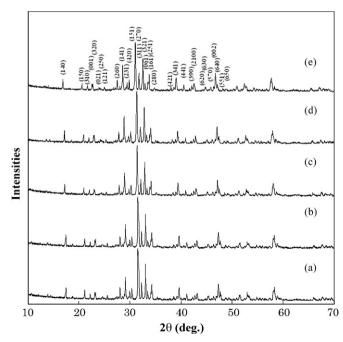


Fig. 3. XRD patterns of sintered BST ceramics with various addition amounts of SrTiO₃ and sintered at $1360\,^{\circ}$ C for 2 h where (a) 0 wt.%; (b) 2 wt.%; (c) 4 wt.%; (d) 6 wt.% and (e) 8 wt.%.

8 wt.% SrTiO₃. The ceramics sintered at 1360 $^{\circ}$ C have the highest densities.

Fig. 2 shows the X-ray diffraction patterns of (a) BST powder calcined at 1250 °C for 2 h and (b) SrTiO₃ powder. All the peaks in Fig. 2(a) can be assigned to that of the orthorhombic tungsten bronze type compounds, designated as $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ solid solutions [7]. In Fig. 2(b), all the peaks can be recognized as the SrTiO₃ single phase with perovskite structure (JCPDS 39-0487).

Fig. 3 shows the XRD patterns of BST ceramics with SrTiO₃ additives and sintered at 1360 °C. All the XRD patterns of Fig. 3(a)–(e) can be assigned to that of the orthorhombic tungsten bronze type compounds, designated as $Ba_{6-3x}Sm_{8+2x}$ - $Ti_{18}O_{54}$ solid solutions. With the increasing addition contents of perovskite-type SrTiO₃ on BST-based tungsten bronze structure, extra peaks were not observed even at the highest

concentration of 8 wt.% SrTiO₃. It was considered that the possible reflections from a secondary phase might overlap with the tungsten bronze structure reflections. No significant changes in the XRD patterns were observed as reported by Silva et al. [16] and Zhu et al. [17] where small amounts (less than 10 wt.%) of similar perovskite-type Li₂O–Nd₂O₃–4TiO₂ and NdAlO₃ were added to BNT structure, respectively.

Typical scanning electron microscopy (SEM) micrographs of the as-sintered surfaces of BST ceramics with $SrTiO_3$ additives and sintered at different temperatures are shown in Fig. 4. The ceramics show typical columnar grain morphology usually observed in $Ba_{6-3x}Ln_{8+2x}Ti_{18}O_{54}$ (Ln = Nd and Sm) ceramics [16,17]. The SEM results confirm the occurrence of phases identified in the XRD patterns. It is noticeable that the size of the columnar grain increases with increasing $SrTiO_3$ content as well as sintering temperatures.

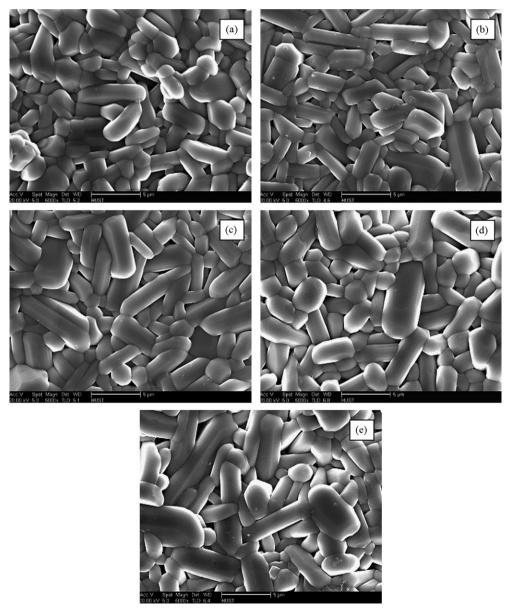


Fig. 4. FE-SEM micrographs of BST-based ceramics with various addition amounts of $SrTiO_3$ and sintered for 2 h where (a) 4 wt.%, 1340 °C; (b) 0 wt.%, 1360 °C; (c) 4 wt.%, 1360 °C; (d) 8 wt.%, 1360 °C and (e) 4 wt.%, 1380 °C.

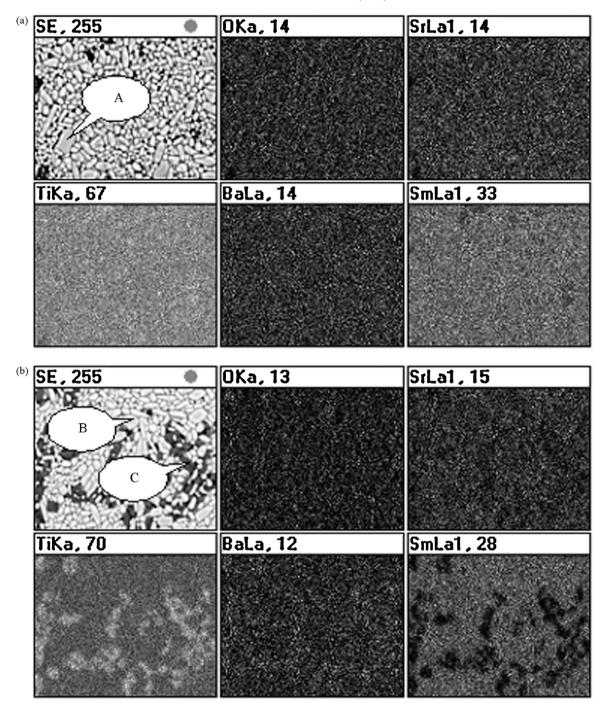


Fig. 5. EPMA surface scan patterns of BST doped with $SrTiO_3$ sintered at 1360 °C for 2 h where (a) 4 wt.% and (b) 8 wt.%.

No obvious second phases could be found with increasing addition contents of $SrTiO_3$. Furthermore, with increasing sintering temperature, significant grain growth was observed with accompanying reduction in porosity; therefore, samples sintered at 1360 °C displayed improved densification and the highest densities. For samples sintered at 1380 °C the microstructure exhibited abnormal growth of the grains resulting in density decrease.

Fig. 5 and Table 1 show the EPMA patterns of the polished samples. As a bright dot means high intensity of the element, we recognized each phase on the basis of the dot darkness.

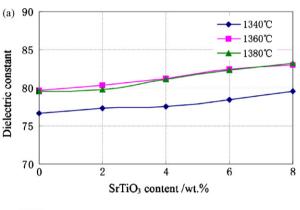
Fig. 5(a) shows a homogeneous phase and means that BST formed a solid solution with $SrTiO_3$, the Sr^{2+} occupied the A1 sites in tungsten bronze structure. Fig. 5(b) shows a mixed phases structure, where the bright matrix phase is BST: $SrTiO_3$ solid solution and the black secondary phase is bariumstrontium–samarium metatitanate. It is probable that, as the concentration of $SrTiO_3$ increases, the lower solubility limit (x) of $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ is reached and a secondary metatitanate phase starts to form, as the phase diagram predicts. In this paper, the solid solution limit of $SrTiO_3$ in BST is thought to be about 4 wt.% and the resultant phase would correspond to

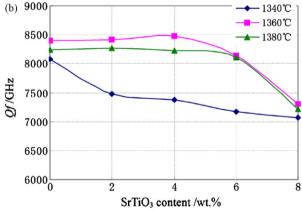
Table 1
The comparison of EPMA results among grain A, B and C in Fig. 5

	Ti K (at.%)	Sr L (at.%)	Ba L (at.%)	Sin L (at.%)	O (at.%)
Grain A	20.78	0.68	5.32	10.26	62.96
Grain B	21.33	1.71	4.43	9.50	63.04
Grain C	27.67	0.35	6.85	1.05	64.09

 $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ with x = 0.4, the addition of $SrTiO_3$ increased the lower solubility limit (x) of $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$.

Fig. 6 shows the microwave dielectric properties of BST ceramics with increasing additions of SrTiO₃ sintered at different temperatures for 2 h. Additions of SrTiO₃ increased





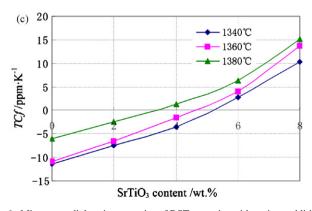


Fig. 6. Microwave dielectric properties of BST ceramics with various addition amounts of $SrTiO_3$ and sintered at different temperature for 2 h: (a) dielectric constant, (b) $Q_{\rm f}$ values, and (c) $TC_{\rm f}$ values.

the dielectric constant slightly and this observed change is attributed to the similar decrease of x values in $Ba_{6-3x}Sm_{8+2x-1}$ Ti₁₈O₅₄ solid solutions, it had been reported [6] that the decrease of x values in $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ solid solutions would lead to the increase of dielectric constant and TC_f values. SrTiO₃ improved the permittivities of BST from 79.7 to 83.0 for samples with 8 wt.% additions and sintered at 1360 °C. As a function of sintering temperatures, the ceramics sintered at 1360 °C had the highest densities and therefore exhibited the highest permittivities. Fig. 6(b) shows the variation in Q_f values of BST ceramics with various additions of SrTiO₃. The entire range of compositions investigated exhibit a decrease in the $Q_{\rm f}$ values, the modest additions of 4 wt.% SrTiO₃ had virtually no effect on the Q_f values of BST, but further addition of SrTiO₃ led to a rapid decrease in the $Q_{\rm f}$ values, the existence of the second phase was thought to lead to the decrease. As a result of the poor densification, the samples sintered at 1340 °C exhibited the lowest Q_f values. Nevertheless, additions of $SrTiO_3$ are detrimental to the Q_f values of BST-based ceramics. Fig. 6(c) shows the change in TC_f values with different addition amounts of SrTiO₃ and sintering temperatures. In a similar way to the variation of permittivities, the TC_f values show an approximately linear increase with increasing content of the additives. SrTiO₃ improved the TC_f of BST from -10.8 to -1.5 ppm/°C when 4 wt.% SrTiO₃ was added. It is apparent that the TC_f values of tungsten bronze structured BST ceramics can be tuned to near zero with additions of perovskite structured SrTiO₃.

4. Conclusions

The additions of SrTiO₃ decreased the densities of BST ceramics. Small additions of perovskite structure SrTiO₃ (less than 4 wt.%) could be accommodated in BST-based tungsten bronze structure, but EPMA results revealed a secondary metatitanate phase in BST-based ceramics with 8 wt.% SrTiO₃ added, the solid solution limit of SrTiO₃ in BST is thought to be about 4 wt.% and the resultant phase would corresponds to $Ba_{6-3x}Sm_{8+2x}Ti_{18}O_{54}$ with x = 0.4, therefore, the addition of SrTiO₃ increased the lower solubility limit (x) of Ba_{6-3x}Sm_{8+2x-} Ti₁₈O₅₄. The relative permittivities and the TC_f values showed an approximately linear increase with increasing additions of $SrTiO_3$, which was attributed to the similar decrease of x values in Ba_{6-3x}Sm_{8+2x}Ti₁₈O₅₄ solid solutions. It was observed that near zero TC_f values could be achieved with the addition of SrTiO₃ additives to BST ceramics. The modest additions of less than 4 wt. % SrTiO₃ had no obviously effect on the Q_f values of BST-based ceramics, but further addition of SrTiO₃ led to a rapid decrease in the $Q_{\rm f}$ values. With 4 wt.% SrTiO₃ addition

and sintered at 1360 °C for 2 h, BST ceramics exhibited excellent dielectric properties: $\varepsilon_r = 81.2$, $Q_f = 8470$ GHz and $TC_f = -1.5$ ppm/°C.

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