

# Mechanical properties and bioactivity of $\beta$ - $\text{Ca}_2\text{SiO}_4$ ceramics synthesized by spark plasma sintering

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## Abstract

Bioactive beta-dicalcium silicate ceramics ( $\beta$ - $\text{Ca}_2\text{SiO}_4$ ) were fabricated by spark plasma sintering (SPS). The relative density of as-prepared  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics reached 98.1% when sintered at 1150 °C, leading to great improvement in bending strength (293 MPa), almost 10 times higher than that of the specimen prepared by conventional pressureless sintering (PLS). High fracture toughness ( $3.0 \text{ MPa m}^{1/2}$ ) and Vickers hardness (5.8 GPa) of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics were also achieved by SPS at 1150 °C. The simulated body fluid (SBF) results showed that  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics had a good in vitro bioactivity to induce hydroxyapatite (HAp) formation on their surface, which suggests that  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics are promising candidates for load-bearing bone implant materials.

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**Keywords:** A. Beta-dicalcium silicate ceramics; B. Mechanical properties; C. Bioactivity; D. Spark plasma sintering

## 1. Introduction

Dicalcium silicate ( $\text{Ca}_2\text{SiO}_4$ ) is an important material in the calcium–silica system, which is frequently identified as an important constituent in Portland cement [1,2], refractory materials [3] and corrosion-resistance coating materials [4,5]. And it has also been well studied because of its polymorphism [6]. Recently,  $\text{Ca}_2\text{SiO}_4$  ceramics have been investigated as a new type of bioceramic for hard tissue regeneration [7,8]. Some studies [7–10] have demonstrated that  $\text{Ca}_2\text{SiO}_4$  powders, ceramics and coatings are bioactive and can quickly induce the formation of a bone-like apatite layer on their surface after soaking in a simulated body fluid (SBF). Moreover, previous study revealed that  $\text{Ca}_2\text{SiO}_4$  ceramics were biocompatible and could support the mesenchymal stem cells adhesion and

spreading [7]. However, poor sinterability and the residual pores in  $\text{Ca}_2\text{SiO}_4$  ceramics deteriorate the mechanical properties. Gou et al. prepared  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics with a relative density of only 88.8% by pressureless sintering (PLS) and the bending strength was lower than 30 MPa, which was much lower than that of the cortical bone (50–150 MPa) [7,11]. The low density resulted in the unsatisfied mechanical properties, which severely limit the application of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics as load-bearing implant materials. In fact, because of the poor sinterability of silicate materials, it is still difficult to obtain fully dense  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics using conventional sintering techniques, such as PLS and hot-pressing (HP). Therefore, it is necessary to develop an advanced sintering technique to enhance the density and the mechanical properties of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics.

Spark plasma sintering (SPS) is a well-known technique for rapid densification of various ceramics at moderate temperatures. During the SPS process, a high electric-pulsed current is applied to provide high heating rate and the activation of powder particles is considered to be achieved at short time

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[12,13]. Due to its high heating rate, high pressure, high energy activity and short sintering time, grain coarsening can be inhibited and dense ceramics with higher performance can be obtained using SPS technique at lower sintering temperatures in comparison with conventional sintering techniques (PLS, HP, etc.) [14]. Previous works showed that some bioceramics sintered by SPS, such as hydroxyapatite (HAp) and alumina ( $\text{Al}_2\text{O}_3$ ), have smaller grain size and higher mechanical properties than those obtained by conventional sintering techniques [15–18].

In the present work, dense  $\beta\text{-Ca}_2\text{SiO}_4$  ceramics were fabricated by the SPS technique and their mechanical properties and in vitro bioactivity were systematically investigated.

## 2. Materials and methods

$\beta\text{-Ca}_2\text{SiO}_4$  powders were synthesized through a modified two-step coprecipitation method using  $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$  and  $\text{Na}_2\text{SiO}_3 \cdot 9\text{H}_2\text{O}$  as precursors. The synthesis process was similar to that of  $\text{Ca}_3\text{SiO}_5$  powders [19] and not shown here for brevity. Afterwards, the  $\beta\text{-Ca}_2\text{SiO}_4$  powders were sintered at 1000–1150 °C for 5 min in vacuum (<10 Pa) under a pressure of 70 MPa by spark plasma sintering (Dr. Sinter 2040, Sumitomo Coal Mining Co., Ltd., Japan).

The samples for microstructure and property characterization were cut from the as-sintered samples by a diamond wheel, polished using SiC abrasive paper and a 0.5  $\mu\text{m}$  diamond suspension, respectively. The bulk density was measured by the Archimedes method. Phase identification of the as-prepared powders and ceramics was conducted via an X-ray diffractometer (XRD; D/max 2200PC, Rigaku, Japan) using monochromatic Cu K $\alpha$  radiation. The fracture surfaces of the samples were observed by scanning electron microscopy (SEM; Model JSM-6700F, JEOL, Japan).

The bending strength and Young's modulus of  $\beta\text{-Ca}_2\text{SiO}_4$  ceramics (2 mm  $\times$  3 mm  $\times$  18 mm) were measured using a three-point bending method in a universal testing machine (Model 1195, Instron, Canton, MA). The span length and crosshead speed were 12 mm and 0.5 mm/min, respectively. The Vickers hardness was measured with a micro-hardness tester (Tukon 2100B, Wolpert-Wilson Instrument, Aachen, Deutschland) under a load of 19.6 N and a dwell time of 15 s. The fracture toughness was determined by an indentation method described by Evans and Charles [20]. The measured values for strength, hardness and toughness were the average of 5 separate measurements.

The  $\beta\text{-Ca}_2\text{SiO}_4$  ceramic discs ( $\Phi$  10 mm  $\times$  2 mm) sintered at 1150 °C were placed in polystyrene bottles containing simulated body fluid (SBF) solution (pH 7.40). The bottles with the samples and SBF were maintained at 37 °C for 1, 3, 7 and 14 days, respectively, at a surface area-to-volume ratio of 0.1  $\text{cm}^2/\text{mL}$  without refreshing the soaking medium. The SBF was prepared as previously described by Kokubo and had similar ion concentrations to those in human blood plasma [21]. After soaking for various periods, the discs were removed from the SBF solution, rinsed with deionized water, and then dried at 60 °C. The formation of bonelike HAp on the ceramic

surface was characterized by XRD, SEM and Fourier transform infrared spectroscopy (FTIR; Nicolet Co., USA) using KBr technology. The concentrations of Ca, Si and P in SBF after soaking were determined by inductively coupled plasma atomic emission spectroscopy (ICP-AES; Varian Co., USA) and pH value of the soaking solution was measured using an electrolyte-type pH meter (PHS-2C; Jingke Leici Co., China).

## 3. Results and discussion

### 3.1. Synthesis and microstructure characterization

Fig. 1 shows the XRD patterns of the as-prepared powders and bulk ceramics sintered in the range of 1000–1150 °C. All the reflections belong to  $\beta\text{-Ca}_2\text{SiO}_4$ , indicating that no phase evolution occurred in the SPS process.

Fig. 2 presents the SEM micrographs of fracture surfaces of  $\beta\text{-Ca}_2\text{SiO}_4$  samples sintered at different temperatures. It reveals the microstructure evolution of  $\beta\text{-Ca}_2\text{SiO}_4$  ceramics. When the sintering temperature was 1000 °C, the average grain size was 1–2  $\mu\text{m}$  (Fig. 2(a)) and the density was 95.7% (Fig. 3). As the sintering temperature increased, pores diminished gradually, which was accompanied with the rapid increase of average grain size and density. The relative density reached 97.7% at 1050 °C. In addition, the fracture surfaces of  $\beta\text{-Ca}_2\text{SiO}_4$  ceramics exhibited homogeneous microstructures composed of equiaxed grains and the average grain size increased from 1 to 2  $\mu\text{m}$  at 1000 °C (Fig. 2(a)) to 2–3  $\mu\text{m}$  at 1050 °C (Fig. 2(b)). As the sintering temperature reached 1100 °C, the relative density increased slightly (98.0%) while the microstructure consisted of fine equiaxed grains and large lamellar grains (Fig. 2(c)–(e)). A higher magnification image shows that the dissociation occurred along the specific crystal face even in the fine grain (Fig. 2(h)). When sintered at 1150 °C, all the fine grains grew and transformed into lamellar grains (Fig. 2(f) and (g)), while the relative density almost kept at the same level (98.1%).

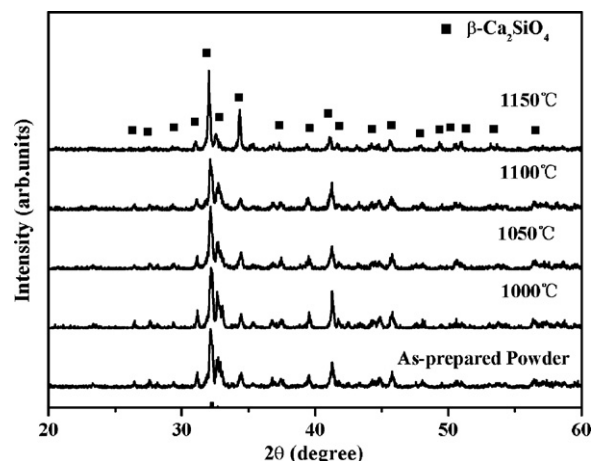


Fig. 1. XRD patterns of  $\beta\text{-Ca}_2\text{SiO}_4$  powders and ceramics sintered at 1000–1150 °C.

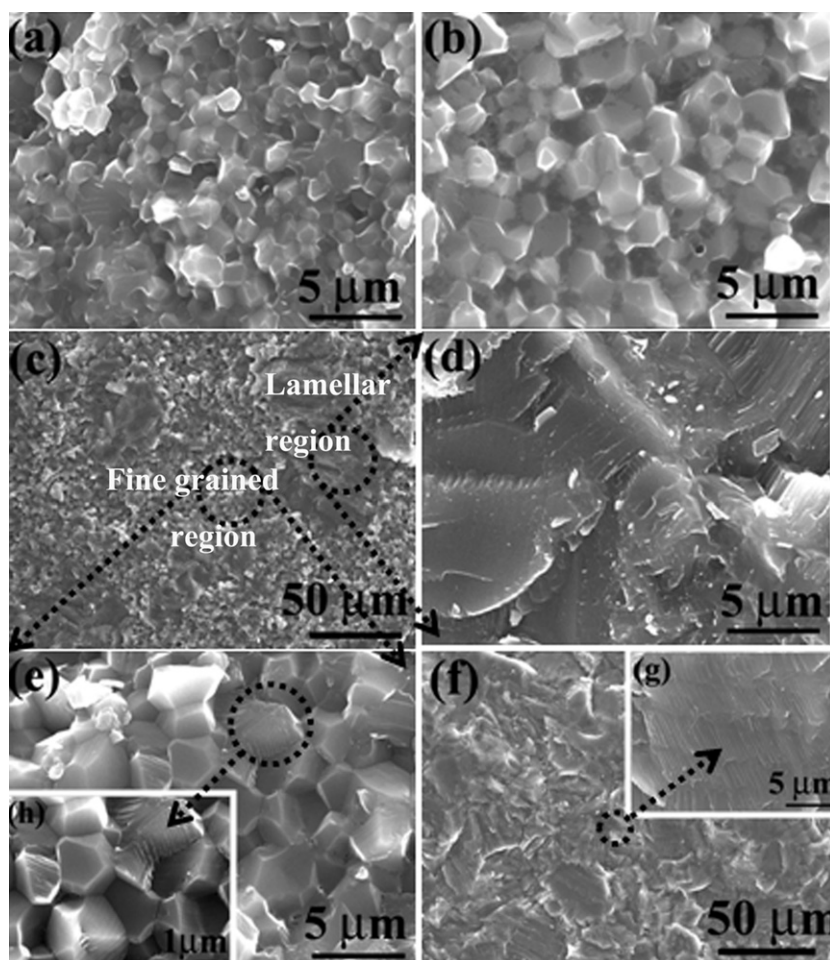


Fig. 2. SEM photographs of the fracture surface of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered at different temperatures: (a) 1000 °C, (b) 1050 °C, (c, d, e, h) 1100 °C and (f, g) 1150 °C.

### 3.2. Mechanical properties

Fig. 3 shows the influence of sintering temperature on the relative density and Vickers hardness of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics. The Vickers hardness increased with the increase of sintering

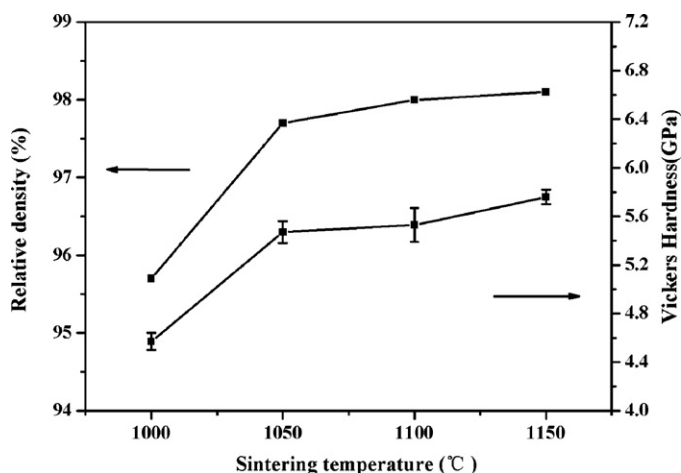


Fig. 3. The relative density and Vickers hardness of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered at 1000–1150 °C.

temperature, which was similar to the tendency of relative density. When sintered at 1000 °C, the Vickers hardness was only 4.6 GPa. At the sintering temperature of 1050 °C, the Vickers hardness increased about 14.6% (5.5 GPa). After that, the Vickers hardness of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics improved slightly with the increase of the sintering temperatures. When sintered at 1150 °C, the Vickers hardness increased slightly to 5.8 GPa. The hardness reflects the local elastic and plastic deformation resistance of materials. The increase in density is in favor of hardness.

The bending strength and fracture toughness of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics as a function of sintering temperature are presented in Fig. 4. Both bending strength and fracture toughness increased with the sintering temperatures increasing, and the change of bending strength was more obvious. When sintered at 1000 °C, the bending strength and fracture toughness of the specimen were only 185 MPa and 2.5  $\text{MPa m}^{1/2}$ , respectively. At the sintering temperature of 1150 °C, the bending strength reached the maximum value of 293 MPa, corresponding to the maximum value of Young's modulus (99 GPa). Similarly, the fracture toughness also increased with the increase of the sintering temperatures and reached the maximum value of 3.0  $\text{MPa m}^{1/2}$  when the sintering temperature was 1150 °C. The

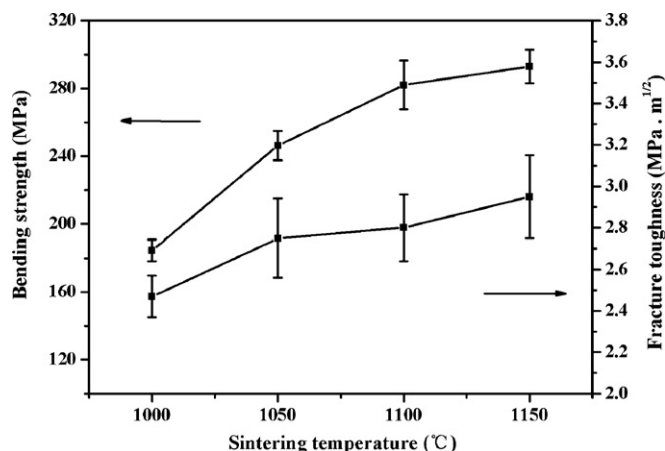


Fig. 4. Bending strength and fracture toughness vs. sintering temperature.

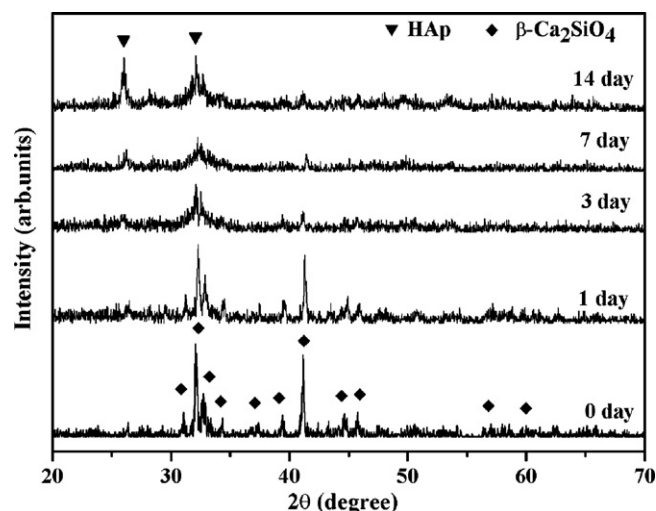


Fig. 5. XRD patterns of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics before and after soaking in SBF.

increase of mechanical properties with temperature was attributed to the pore decrease and density improvement at higher sintering temperatures.

For bio-ceramics, the bending strength and fracture toughness are two crucial mechanical properties. The improvements in strength and fracture toughness are mainly associated with the increase of density, i.e. the decrease of pores. The decrease of fracture toughness is associated with flaws of specimens such as pores and cracks, which decrease the fracture energy dissipation during the fracture process. Since almost fully dense ceramics were achieved using SPS, there is no wonder that an enhancement of fracture toughness in as-prepared  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics was observed. At higher sintering temperature (1150 °C), improved toughness of the ceramics should also be associated with the grain morphology. The fracture surface shows the lamellar cleavage of the plate-like grains is dominant during the fracture process (Fig. 2(f)). As in the cases of  $\text{Si}_3\text{N}_4$  [22] and  $\text{SiC}$  [23], elongated or plate-like grains promote high energy dissipation during fracture and lead to high fracture toughness. Thus, the delamination of grains may be the main reason for their relatively high fracture toughness.

It is generally accepted that the strength of ceramics improves with the increase in the density. The relative density of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered by SPS was higher than 98.0%. In addition, the bending strength reached 293 MPa, which was almost 10 times higher than that of the specimen obtained by PLS. This result demonstrated that SPS offers significant advantages over PLS for the consolidation of  $\beta$ - $\text{Ca}_2\text{SiO}_4$ . The relative density of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics consolidated by PLS was lower than 90% [7]. In addition, high temperature and long dwell time in the PLS process resulted in grain coarsening and flaw structure [24]. On the contrary, SPS is a rapid consolidation technique which includes the effects of electrical discharge, resistance heating and high pressure. All these factors could enhance densification during the SPS process.

It is known that the bioactive ceramics for the application of load-bearing sites implant and replacement are limited due to their unsatisfied mechanical properties. In this work, the bending strength of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered by SPS

(293 MPa) was much higher than that of the cortical bone (50–150 MPa [11]). The fracture toughness of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics (3.0  $\text{MPa m}^{1/2}$ ) was also higher than the low limit of the fracture toughness of human cortical bone (2–12  $\text{MPa m}^{1/2}$  [11]). It is necessary to fabricate  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics with the high fracture toughness by developing composite materials in the future.

### 3.3. In vitro HAP forming ability

Fig. 5 shows the XRD patterns of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics before and after soaking in SBF for various periods. The intensity of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  diffraction peaks decreased slightly and the peaks of HAP was not obvious after soaking for 1 day. In contrast, after a prolonged soaking time of 3 days, most diffraction peaks of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  disappeared and a broad peak at  $2\theta = 31.7^\circ$  corresponding to the (2 1 1) reflection of HAP was evident, indicating that the deposited HAP should be nanocrystalline. With prolonged soaking time from 3 to 14 days, the intensity of HAP peaks increased and the secondary strong peak at  $2\theta = 26^\circ$  corresponding to the (0 0 2) reflection of HAP became more obvious, suggesting that more HAP deposited on the surface of ceramics.

The SEM micrographs of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics soaked in SBF for different periods are presented in Fig. 6. It is evident that some nano-size crystallites and particles nucleated and deposited on the ceramic surface after soaking for 1 day (Fig. 6(a) and (b)). Some micro-cracks could also be observed on the ceramic surface caused by the shrinkage of the soaked samples in air, suggesting the formation of a thick deposition layer (Fig. 6(a)) [25]. With the increase of soaking time, more HAP agglomerates were formed and deposited on the ceramic surface and the average size of these agglomerates was about 5–8  $\mu\text{m}$  (Fig. 6(c), (e) and (g)). The higher magnification SEM micrographs revealed that the agglomerates were composed of a large number of tiny worm-like crystals with typical morphology of HAP and the size of the crystallites was about 200–300 nm in length and 80 nm in diameter (Fig. 6(d), (f) and



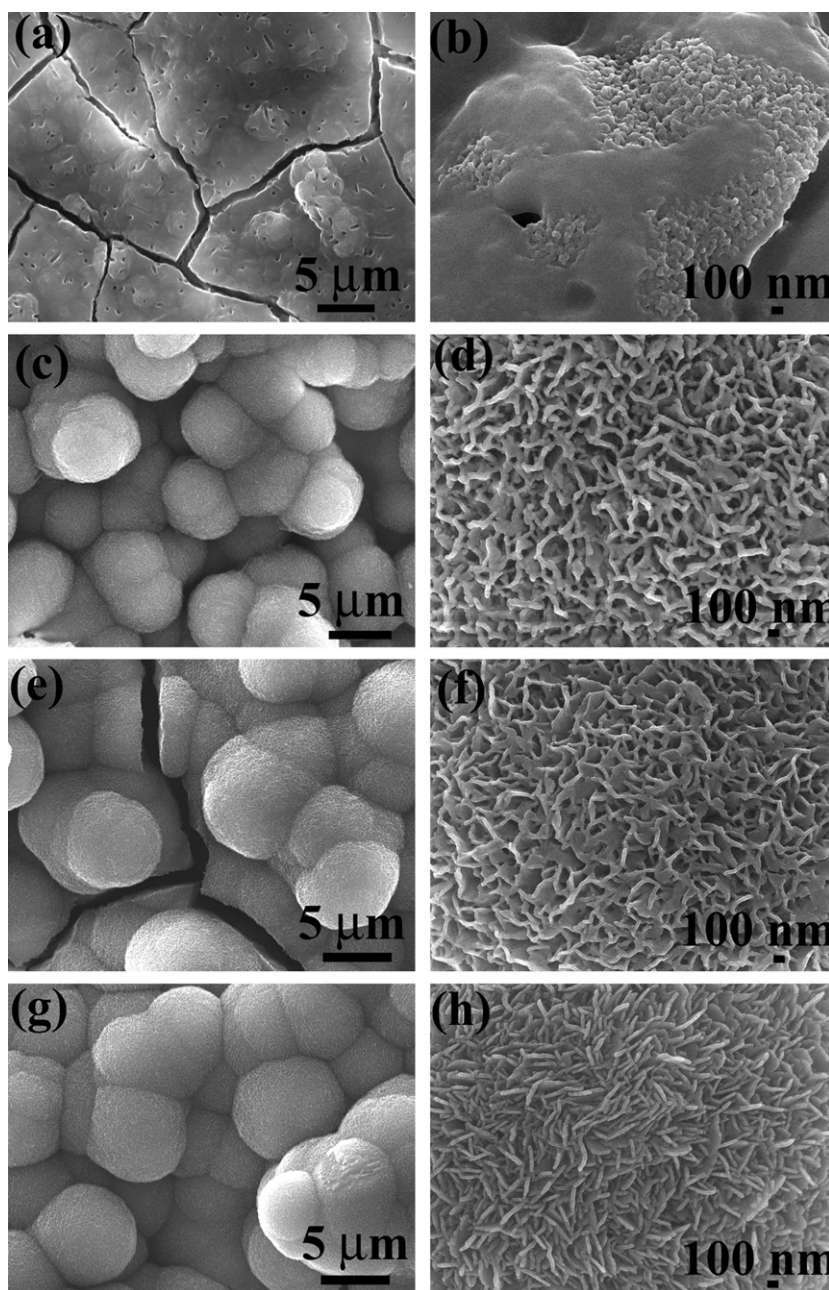


Fig. 6. SEM micrographs of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics soaked in SBF for various times: (a, b) 1 day, (c, d) 3 days, (e, f) 7 days and (g, h) 14 days.

(h)). After soaking for 14 days, more HAP agglomerates grew on the ceramic surface and the HAP layer became more compact (Fig. 6(g) and (h)).

The FTIR spectra of the ceramics before and after soaking in SBF are displayed in Fig. 7. The absorption bands of silicate groups were obvious before soaking. The intense bands at  $510$  and  $980\text{ cm}^{-1}$  were associated with the Si–O–Si vibrational mode of bending, and the band at  $902\text{ cm}^{-1}$  was related to the Si–O symmetric stretch. After soaking for 1 day, the intensity of the silicate absorption bands decreased. Simultaneously, new absorption bands at  $603$  and  $566\text{ cm}^{-1}$  could be detected, which were split from the P–O bending vibration ( $\nu_4$ ) of  $\text{PO}_4^{3-}$  group around  $598\text{ cm}^{-1}$ . The band at  $1035\text{ cm}^{-1}$  could be attributed to the P–O stretching vibration ( $\nu_3$ ) mode. All these bands were

the characteristics of HAP crystals. According to the previous report of infrared correlation charts [26], it can be confirmed that HAP had formed on the ceramic surface. Furthermore, the C–O stretching of  $\text{CO}_3^{2-}$  groups at  $872$ ,  $1415$  and  $1465\text{ cm}^{-1}$  and the band at  $1635\text{ cm}^{-1}$  to the OH absorption could also be recognized in the FTIR spectra after soaking for 1 day [27]. These results further confirmed that a carbonate-containing hydroxyapatite layer could be induced to deposit on the surface of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics in the SBF.

Fig. 8 presents the concentration of Ca, Si and P in SBF as well as the pH value of the immersion solutions as a function of the soaking time. It is obvious that the Ca and Si concentration increased with the soaking time increasing. Simultaneously, the pH value of the immersion solutions increased from 7.40 to

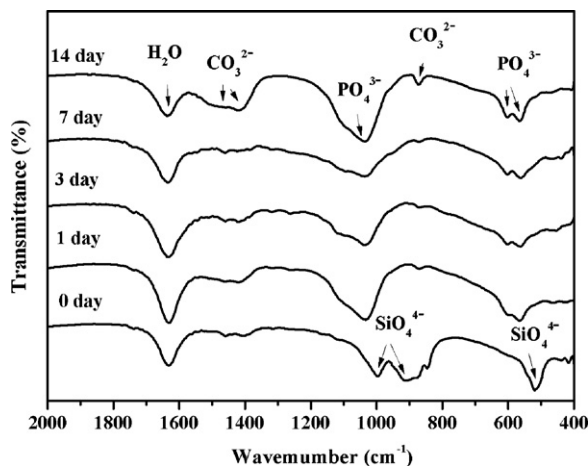


Fig. 7. FTIR spectra of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics soaked in SBF for various periods.

8.16 after soaking for 14 days. In contrast, the P concentration in SBF decreased steeply to a level that was only 25.5% of the starting concentration after soaking for 3 days, and then continuously decreased slowly up to 14 days. The increase in Ca and Si concentrations was attributed to the dissolution of calcium and silicate ions from  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics, and phosphate ions in the immersion solution were consumed with the formation of HAp, which resulted in the decrease of P concentration. Although some calcium ions were consumed to form HAp, more calcium ions were dissolved from the ceramic matrix than those were consumed. Moreover, the pH value of the resultant SBF solution increased due to the ionic exchange between calcium ions in ceramics and  $\text{H}^+$  in SBF [28].

As we know, bioactive materials can elicit a specific biological response at the tissue–materials interface, resulting in the formation of HAp layers between the tissues and the materials. The bonelike HAp plays an essential role in forming the chemical bond of bioactive material to the living bone, and the formation of the bonelike HAp in SBF has proven to be useful in predicting the bone bonding ability of material in vitro [29]. Previous studies [11,29–31] have shown that some bio-glasses and glass ceramics, including the  $\text{CaO-SiO}_2$  components, could bond to living bone by means of forming HAp layers, and the  $\text{CaO-SiO}_2$  components contributed mainly to the bioactivity of those materials. It has been proved that  $\text{CaSiO}_3$  ceramics [32,33] and coatings [28,34] consisting of the  $\text{CaO-SiO}_2$  components were bioactive and could induce HAp deposition when soaked in SBF. Liu et al. [28] revealed the mechanism of HAp formation on the  $\text{CaSiO}_3$  surface. Firstly, calcium ions dissolved from the sample surface, leaving a hydrated silica layer, which provided favorable sites for apatite nucleation. On the other hand, the degree of supersaturation of the solution with respect to apatite increased with the dissolution of ions. Hence, the apatite nuclei were rapidly formed on the sample surface, and they spontaneously grew by consuming calcium and phosphate ions from the surrounding fluid. The composition of  $\text{Ca}_2\text{SiO}_4$  is similar to that of  $\text{CaSiO}_3$ . Our results showed that  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered by SPS also possessed excellent bioactivity and could develop a bonelike HAp layer on their surface when soaked in SBF. The

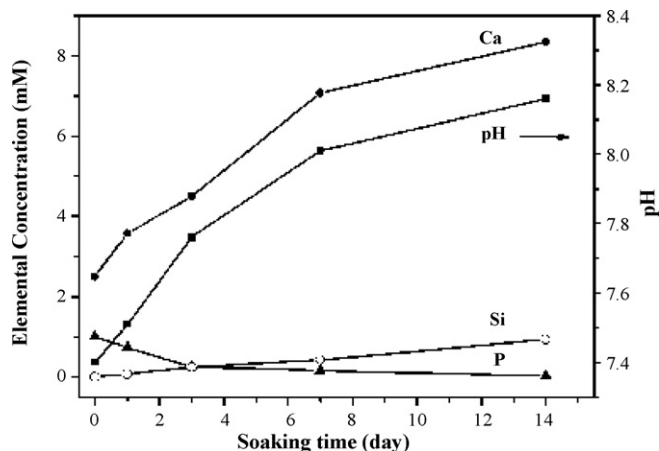


Fig. 8. Time dependence of ion concentrations and pH value in SBF solution when soaking  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics.

ICP-AES analysis results also indicated that the mechanism of bonelike HAp formation on the surfaces of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics might be similar to that of bioactive wollastonite ceramics, which corresponded well to the results of the XRD, FTIR and SEM characterizations above.

#### 4. Conclusions

Dense  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics with the lamellar microstructure were fabricated using SPS at low temperature (1150 °C). The effects of sintering temperature on the microstructures and mechanical properties were evaluated.  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered by SPS have higher density and superior mechanical properties compared with those fabricated by PLS. The high bending strength (293 MPa), Vickers hardness (5.8 GPa), fracture toughness (3.0  $\text{MPa m}^{1/2}$ ) and Young's modulus (99 GPa) were achieved at 1150 °C. The bending strength of  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics produced by SPS was almost 10 times higher than that of the specimen obtained by PLS. The SBF soaking results revealed that  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics sintered by SPS had good bioactivity and could rapidly induce HAp formation after soaking in SBF. The results showed that  $\beta$ - $\text{Ca}_2\text{SiO}_4$  ceramics produced by SPS should be potential candidates as bioactive load-bearing bone repair materials.

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