

# Microwave dielectric properties of $(1 - x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$ ceramics

Jiamao Li<sup>a,b</sup>, Tai Qiu<sup>b,\*</sup>

<sup>a</sup> School of Materials Science and Engineering, Anhui University of Technology, Maanshan 243002, PR China

<sup>b</sup> College of Materials Science and Engineering, Nanjing University of Technology, Nanjing 210009, PR China

Received 30 December 2011; received in revised form 6 February 2012; accepted 7 February 2012

Available online 14 February 2012

## Abstract

Microstructures and microwave dielectric properties of  $(1 - x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ( $0.1 \leq x \leq 0.7$ ) ceramics have been investigated. A two-phase system was formed in the given compositional range. The grain morphology exhibited two different types of grain: large circular grain and small square grain. With the increasing  $x$  value, the grain morphology of the small square grain became irregular. The microwave dielectric properties were strongly related to the composition. As the  $x$  value increased from 0.1 to 0.7, the dielectric constant ( $\epsilon_r$ ) decreased from 87 to 48.3, the quality factor ( $Q \times f$ ) value from 14390 to 8360 GHz, and the temperature coefficient of resonant frequency ( $\tau_f$ ) value from +130.6 to −24.8 ppm/°C, respectively. For practical application, an  $\epsilon_r$  of 74.3, a  $Q \times f$  value of 12690 GHz and a  $\tau_f$  value of +8.8 ppm/°C were obtained for  $0.7\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - 0.3\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics sintered at 1450 °C for 4 h.

© 2012 Elsevier Ltd and Techna Group S.r.l. All rights reserved.

**Keywords:**  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$ ;  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$ ; Microwave dielectric properties; Microstructure

## 1. Introduction

With the rapid development of the wireless communication, the demand for microwave components with combined dielectric properties has been increased. For practical application, three key properties of high quality factor ( $Q \times f$ ), high dielectric constant ( $\epsilon_r$ ) and near-zero temperature coefficient of resonant frequency ( $\tau_f$ ) are required to the microwave dielectric ceramics. High dielectric constant ceramics make it possible to noticeably miniaturize passive microwave components. In the past 30 years, many efforts have been made to develop microwave ceramics with a high dielectric constant. C. Huang et al. [1] reported that the partial substitution of  $\text{Ca}^{2+}$  ions by  $\text{La}^{3+}$  ions in  $\text{CaTiO}_3$  led to the formation of single phase  $\text{Ca}_{1-x}\text{La}_{2x/3}\text{TiO}_3$  solid solution. Meanwhile, a decrease in  $\epsilon_r$ ,  $\tau_f$  and an increase in  $Q \times f$  value with the increasing  $x$  value were observed. When  $x = 0.4$ ,  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  ceramics showed a high  $\epsilon_r$  of 109 and a maximum  $Q \times f$  value of 17,600 GHz. However, complete suppression of the large positive  $\tau_f$  ( $\tau_f = +213$  ppm/°C) to zero was not achieved.

Therefore, it should be an important issue to further adjust the  $\tau_f$  value of  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  to zero. Practically, two or more compounds having positive and negative  $\tau_f$  values are used to form a solid solution or mixed phases to adjust  $\tau_f$  to zero. Several ceramic systems such as  $(1 - x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x(\text{Li}_{0.5}\text{Nd}_{0.5})\text{TiO}_3$  ( $\epsilon_r = 105$ ,  $Q \times f = 7000$  GHz,  $\tau_f = +4.5$  ppm/°C at  $x = 0.4$ ),  $(1 - x)(\text{Mg}_{0.95}\text{Co}_{0.05})\text{TiO}_3 - x\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  ( $\epsilon_r = 21.9$ ,  $Q \times f = 131,000$  GHz,  $\tau_f = -15.5$  ppm/°C at  $x = 0.1$ ) and  $(1 - x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Nd}(\text{Mg}_{0.5}\text{Ti}_{0.5})\text{O}_3$  ( $\epsilon_r = 49$ ,  $Q \times f = 13,000$  GHz,  $\tau_f = +1$  ppm/°C at  $x = 0.4$ ) with near-zero  $\tau_f$  values have been developed in recent years [1–3].

In order to achieve a near-zero  $\tau_f$  value,  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics ( $\epsilon_r \sim 24.7$ ,  $Q \times f \sim 33,200$  GHz,  $\tau_f \sim -34.3$  ppm/°C) [4] were chosen as a  $\tau_f$  compensator and added to  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  ceramics to form a new ceramic system  $(1 - x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  in this paper. Based on phase composition and the microstructure of the present ceramics, the resultant microwave dielectric properties were studied.

## 2. Experimental procedures

The starting materials were high-purity grade ( $\geq 99.9\%$ ) powders of  $\text{CaCO}_3$ ,  $\text{La}_2\text{O}_3$ ,  $\text{TiO}_2$ ,  $\text{Sm}_2\text{O}_3$  and  $\text{Nb}_2\text{O}_5$ . The

\* Corresponding author. Tel.: +86 25 83587262; fax: +86 25 83587268.

E-mail addresses: [lijiamao@ahut.edu.cn](mailto:lijiamao@ahut.edu.cn) (J. Li), [qiutai51@yahoo.cn](mailto:qiutai51@yahoo.cn) (T. Qiu).

powders were individually prepared according to the desired stoichiometry  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  and  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$ , and ground in ethanol for 24 h in a ball mill with zirconia balls.  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  and  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  powders were calcined at 1100 °C for 3 h and 1200 °C for 4 h, respectively. The calcined powders were weighed according to the composition of  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  and remilled 24 h. After dried, these powders with 7 wt.% PVA solution as a binder were pressed into pellets with dimensions of 12 mm diameter and 6 mm thickness under a pressure of 300 MPa. These pellets were finally sintered at 1400–1550 °C for 4 h in air.

The bulk densities of the sintered pellets were measured by the Archimedes method. The crystalline phases of the ceramics were identified by using an X-ray diffractometer (XRD) using Cu K $\alpha$  radiation (40 kV and 20 mA, XRD, D8 Advance, Bruker, Germany). The microstructural observations and analysis of the sintered surfaces were performed by using scanning electron microscopy (SEM, JEOL JSM 6490, Japan) coupled with energy dispersive spectroscopy (EDS). The dielectric constant ( $\epsilon_r$ ) and unloaded  $Q$  values at microwave frequencies were measured using the Hakki–Coleman dielectric resonator method, as modified and improved by Courtney [5,6]. The  $\tau_f$  was measured in a temperature range from 25 to 80 °C. The  $\tau_f$  value was calculated by the following equation:

$$\tau_f = \frac{f_{80} - f_{25}}{f_{25} \cdot 55} \times 10^6 (\text{ppm}/^\circ\text{C}) \quad (1)$$

where  $f_{25}$  and  $f_{80}$  are the  $\text{TE}_{018}$  resonant frequencies at 25 and 80 °C, respectively.

### 3. Results and discussion

The XRD patterns of  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  (hereafter referred to as  $(1-x)\text{CLT} - x\text{CSN}$ ) ceramics with different  $x$  values are shown in Fig. 1. No second phase is detected and the pattern exhibits a two-phase system that includes CLT phase and CSN phase through the entire compositional range. With the increase of the  $x$  value in the system, the relative intensities of CLT reflection lines decrease gradually, implying that the content of CSN phase in the  $(1-x)\text{CLT} - x\text{CSN}$  ceramics increases. When the  $x$  value increases to 0.5, the main crystal phase changes from CLT to CSN phase. Table 1 lists the lattice parameters of the CLT phase. The values of  $a$  axis,  $b$  axis,  $c$  axis and unit cell volume almost do not change with the increase of CSN content as seen from Table 1. This result is similar to the  $(\text{K}_{0.5x}\text{Bi}_{1-0.5x})(\text{Mo}_x\text{V}_{1-x})\text{O}_4$  ceramics reported by D. Zhou

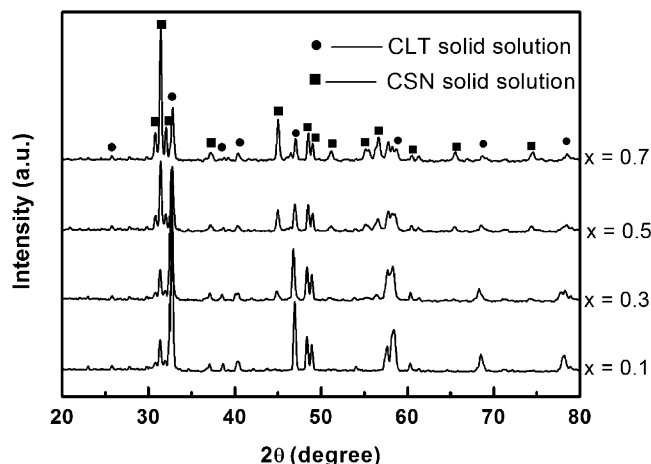


Fig. 1. XRD patterns of  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics with different  $x$  values.

et al. [7]. The reason is that the phase composition and structure of the two end members shall not change with the different ratio between them in a stable composite system.

However, compared with the diffraction peaks of CLT phase reported by C. Huang et al. [1], the diffraction peaks of the CLT phase in the present composite system slightly shift to lower angles with the increasing  $x$  value, indicating that the unit cell volume is enlarged. It is mainly attributed to a larger effective radius of  $(\text{SmNb})^{4+}$  (0.799 Å) than that of  $\text{Ti}^{4+}$  (0.605 Å). This phenomenon means that a limited solid solution might be formed by element substitution between CLT phase and CSN phase.

Fig. 2 shows the variation of bulk density for the  $(1-x)\text{CLT} - x\text{CSN}$  ceramics as a function of sintering temperature. It is obviously seen that the density steadily increases first with the increase of sintering temperature and then saturates for all compositions. The density saturation with sintering temperature implies the densification. However, the densification temperature is different for different compositions.

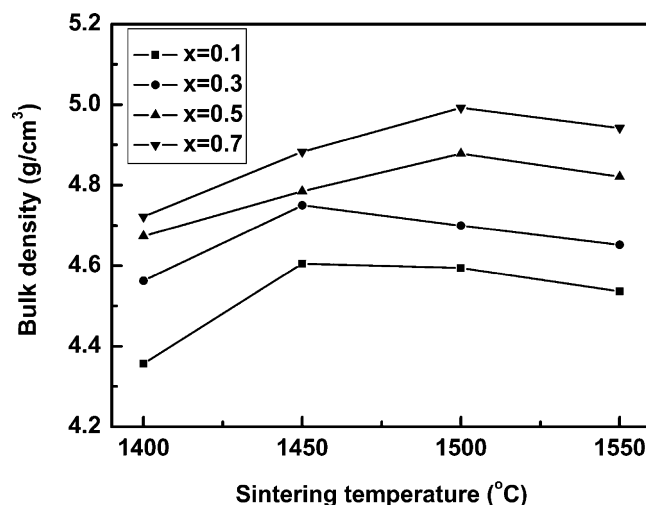


Fig. 2. Variation of bulk density for  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics as a function of sintering temperature.

Table 1  
Lattice parameters of the CLT phase.

$x$	$a$ (Å)	$b$ (Å)	$c$ (Å)	$V_m$ (Å <sup>3</sup> )
0.1	5.53713	5.43587	7.75206	233.33
0.3	5.53785	5.43558	7.75212	233.35
0.5	5.53898	5.43332	7.75210	233.30
0.7	5.53926	5.43446	7.75208	233.36

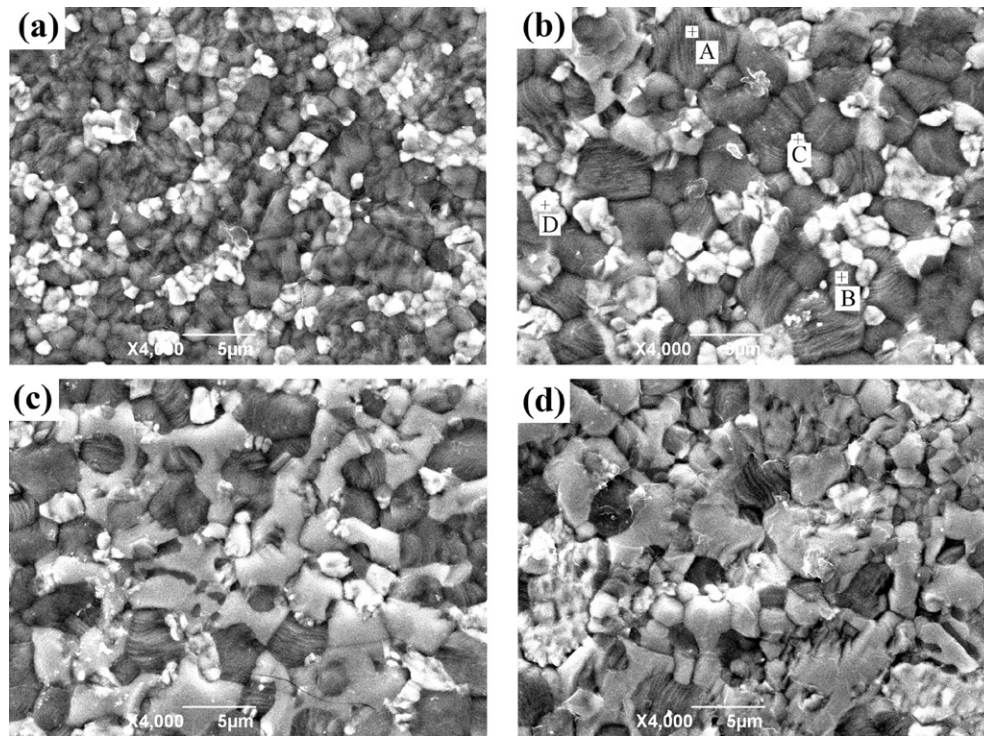


Fig. 3. SEM micrographs of  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3-x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics sintered at  $1500\text{ }^\circ\text{C}$  for 4 h: (a)  $x = 0.1$ ; (b)  $x = 0.3$ ; (c)  $x = 0.5$ ; (d)  $x = 0.7$ .

For compositions of  $x = 0.1$  and  $0.3$ , the maximum bulk density appears at about  $1450\text{ }^\circ\text{C}$ . In contrast, the bulk density maximum occurs at about  $1500\text{ }^\circ\text{C}$  for compositions with  $x = 0.5$  and  $0.7$ . These results indicate that the addition of CSN significantly retards the sintering of the system owing to its higher sintering temperature ( $\sim 1550\text{ }^\circ\text{C}$ ) than that of CLT ( $\sim 1400\text{ }^\circ\text{C}$ ) [1,4]. In addition, the bulk density increases with the increasing  $x$  value for a given sintering temperature due to the larger density ( $5.20\text{ g/cm}^3$ ) of CSN ceramics than that ( $4.60\text{ g/cm}^3$ ) of CLT ceramics [1,4].

The SEM micrographs of the  $(1-x)\text{CLT}-x\text{CSN}$  ceramics sintered at  $1500\text{ }^\circ\text{C}$  for 4 h are illustrated in Fig. 3. It can be found that the dense ceramics are obtained and few pores are observed for all compositions. There are two kinds of grains in the present ceramic system, the circular ones with bigger grain size of  $3\text{--}5\text{ }\mu\text{m}$  and the square ones with smaller grain size of  $0.5\text{--}4\text{ }\mu\text{m}$ . In order to identify the compositional difference between the two types of grains, the element analysis was performed by means of EDS. According to the EDS analysis showed in Table 2, the square grains such as C and D have much more Nb, Sm and La element contents than the circular grains

such as A and B, but they do not contain Ti element. Associating with the XRD analysis in Fig. 1, it can be concluded that the circular and the square grains were the CLT and the CSN grains, respectively. Both of the pure  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  and  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  composition belong to the perovskite structure. The La and Sm have similar ionic radius and maybe some of the Sm can substitute for the La in  $\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3$  to form a limited solid solution. Similarly, the La can also substitute for the Sm in  $\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  to form another solid solution to achieve a more stable system. Combining these EDS results (shown in Table 2) with the XRD and SEM analysis of the  $(1-x)\text{CLT}-x\text{CSN}$  ceramics, the real composition might not be  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3-x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$ , might be  $(1-x)\text{Ca}_{0.6}(\text{La},\text{Sm})_{0.267}\text{TiO}_{3-x}\text{Ca}((\text{Sm},\text{La})_{0.5}\text{Nb}_{0.5})\text{O}_3$ . Furthermore, the grain size of the CSN grain increases and the grain morphology becomes irregular with the increasing  $x$  value. This phenomenon indicates that the CLT solid solution can inhibit the grain growth of the CSN solid solution, which may affect the dielectric properties.

Fig. 4 shows the dielectric constant ( $\epsilon_r$ ) and  $Q \times f$  value of the  $(1-x)\text{CLT}-x\text{CSN}$  ceramics as a function of  $x$  value. It is clearly seen that the  $\epsilon_r$  value decreases almost linearly with the increasing  $x$  value, which is attributed to the fact that CLT ( $\epsilon_r = 109$ ) has a much higher dielectric constant than CSN ( $\epsilon_r = 24.7$ ) does. As the  $x$  value increases from  $0.1$  to  $0.7$ , the  $\epsilon_r$  value decreases from  $87$  to  $48.3$ . However, an anomalous behavior is found that the  $Q \times f$  value of the  $(1-x)\text{CLT}-x\text{CSN}$  ceramics is outside the range exhibited by the end members CLT with a  $Q \times f$  value  $17600\text{ GHz}$  of and CSN with a  $Q \times f$  value of  $33200\text{ GHz}$ . With  $x$  increasing from

Table 2  
EDS data of  $0.7\text{CLT}-0.3\text{CSN}$  ceramics for spots A–D.

Spot	Atom (%)					
	Ca–K	Ti–K	Nb–L	Sm–L	La–L	O–K
A	12.70	19.18	1.47	1.67	2.41	62.57
B	12.21	21.31	1.07	0.94	2.41	62.06
C	13.11	0	10.04	6.56	4.97	65.32
D	13.94	0	9.63	7.14	3.59	65.7

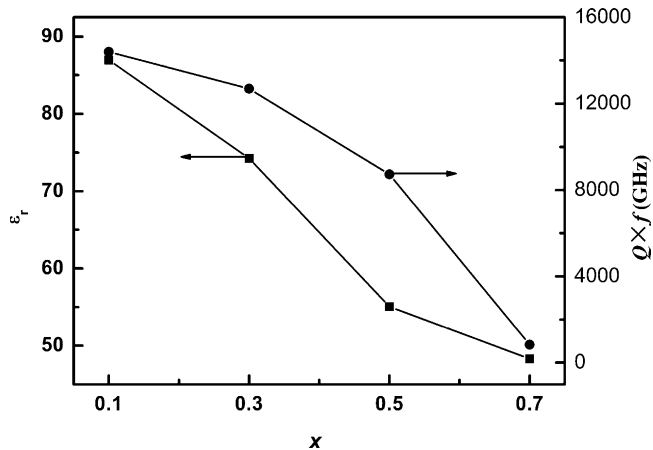


Fig. 4. Dielectric constant and  $Q \times f$  value of the  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ceramics as a function of  $x$  value.

0.1 to 0.7, the  $Q \times f$  value decreases from 14390 to 8360 GHz. It is well known that many factors such as densification or porosity, microstructure and secondary phase affect microwave dielectric loss. However, the  $Q \times f$  value is independent of the density for highly densified ceramics [8]. As a result, the  $Q \times f$  value is mainly controlled by the microstructure in the present ceramics. As observed in Fig. 3, an irregular grain morphology appears in the ceramics, producing an increase in lattice imperfection and increasing dielectric loss. Consequently, the decrease in the  $Q \times f$  value might be a result of the grain morphology.

The theoretical and measured  $\tau_f$  values of the  $(1-x)\text{CLT} - x\text{CSN}$  ceramics with various  $x$  values are illustrated in Fig. 5. When the  $x$  value increases from 0.1 to 0.7, the measured  $\tau_f$  value decreases from +130.6 to -24.8 ppm/°C, and the theoretical  $\tau_f$  value decreases from +184 to +31.5 ppm/°C. At  $x=0.3$ , a near-zero  $\tau_f$  value ( $\tau_f = +8.8$  ppm/°C) was achieved for the present system. As is well known, the relationship between temperature coefficient of

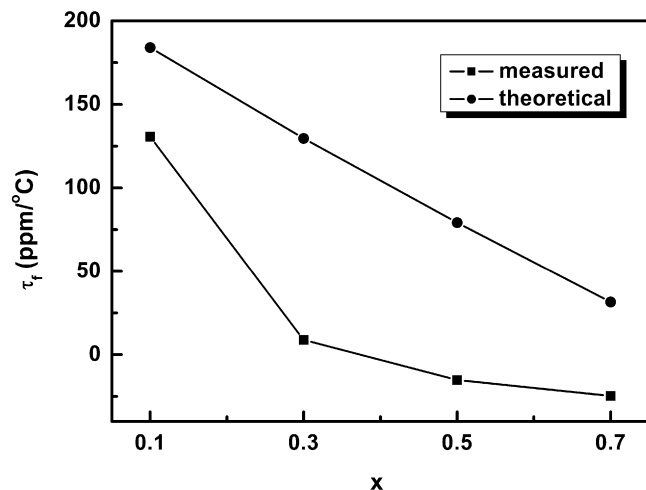


Fig. 5. Theoretical and measured  $\tau_f$  values of the  $(1-x)\text{CLT} - x\text{CSN}$  ceramics with various  $x$  values.

dielectric constant ( $\tau_\epsilon$ ) and  $\tau_f$  is defined as the following equation [9,10]:

$$\tau_\epsilon = \frac{1}{\epsilon_r} \frac{d\epsilon_r}{dT} = \frac{d(\lg \epsilon_r)}{dT} = y_1 \frac{1}{\epsilon_{r1}} \frac{d\epsilon_{r1}}{dT} + y_2 \frac{1}{\epsilon_{r2}} \frac{d\epsilon_{r2}}{dT} = y_1 \tau_{\epsilon r1} + y_2 \tau_{\epsilon r2} \quad (2)$$

where  $y_1$  and  $y_2$  are the volume fractions;  $\tau_{\epsilon r1}$  and  $\tau_{\epsilon r2}$  are the  $\tau_\epsilon$  values of the CLT and CSN ceramics, respectively. Hence, the mixing rule of the  $\tau_f$  value can be described as the following:

$$\tau_f = y_1 \tau_{f1} + y_2 \tau_{f2} \quad (3)$$

The theoretical  $\tau_f$  values of the  $(1-x)\text{CLT} - x\text{CSN}$  ceramics were calculated using Eq. (3). Comparing the measured  $\tau_f$  value with the theoretical  $\tau_f$  value, it is seen that the measured  $\tau_f$  is much more negative, which might result from the formation of solid solution in the  $(1-x)\text{CLT} - x\text{CSN}$  ceramic system. Similar result in the  $\text{Bi}_2\text{MoO}_6\text{-TiO}_2$  composite ceramics was reported by L. Pang et al. [9].

#### 4. Conclusions

The microstructures and microwave dielectric properties of the two-phase system  $(1-x)\text{Ca}_{0.6}\text{La}_{0.267}\text{TiO}_3 - x\text{Ca}(\text{Sm}_{0.5}\text{Nb}_{0.5})\text{O}_3$  ( $0.1 \leq x \leq 0.7$ ) ceramics were investigated. The microwave dielectric properties were strongly related to the composition. The dielectric constant,  $Q \times f$  value and  $\tau_f$  value decreased with an increase of  $x$  value. A dielectric material with an  $\epsilon_r$  of 74.3, a  $Q \times f$  value of 12690 GHz and a  $\tau_f$  value of +8.8 ppm/°C was obtained at  $x=0.3$ , which is a promising candidate for communication components.

#### Acknowledgement

This work was supported by A Project Funded by the Priority Academic Program Development of Jiangsu Higher Education Institutions (PAPD).

#### References

- [1] C. Huang, J. Tsai, Y. Chen, Dielectric properties of  $(1-y)\text{Ca}_{1-x}\text{La}_{2x/3}\text{TiO}_3 - y(\text{Li,Nd})_{1/2}\text{TiO}_3$  ceramic system at microwave frequency, Mater. Res. Bull. 36 (2001) 547–556.
- [2] C. Huang, C. Pan, J. Hsu, J. Wang, Microwave dielectric properties and mixture behavior of  $(\text{Mg}_{0.95}\text{Co}_{0.05})\text{TiO}_3\text{-Ca}_{0.6}\text{La}_{0.8/3}\text{TiO}_3$  ceramic system, J. Alloys Compd. 461 (2008) 521–526.
- [3] Y. Chen, Structure and dielectric characterization of  $x\text{Nd}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3 - (1-x)\text{Ca}_{0.6}\text{La}_{0.8/3}\text{TiO}_3$  in the microwave frequency range, J. Alloys Compd. 509 (2011) 6285–6288.
- [4] L. Khalam, M. Sebastian, Low loss dielectrics in the  $\text{Ca}(\text{B}'_{1/2}\text{Nb}_{1/2})\text{O}_3$  [ $\text{B}' = \text{Lanthanides, Y}$ ] system, J. Am. Ceram. Soc. 90 (2007) 1467–1474.
- [5] B. Hakki, P. Coleman, A dielectric resonator method of measuring inductive capacities in the millimeter range, IEEE Trans. Microwave Theory Tech. MTT-8 (1960) 402–410.
- [6] W. Courtney, Analysis and evaluation of a method of measuring complex permittivity and permeability of microwave materials, IEEE Trans. Microwave Theory Tech. MTT-18 (1970) 476–485.
- [7] D. Zhou, L. Pang, J. Guo, H. Wang, X. Yao, C. Randall, Phase evolution, phase transition, Raman spectra, infrared spectra, and microwave dielectric

- properties of low temperature firing ( $\text{K}_{0.5x}\text{Bi}_{1-0.5x})(\text{Mo}_x\text{V}_{1-x})\text{O}_4$  ceramics with scheelite related structure, *Inorg. Chem.* 50 (2011) 12733–12738.
- [8] W. Kim, T. Hong, E. Kim, K. Yoon, Microwave dielectric properties and far infrared reflectivity spectra of the  $(\text{Zr}_{0.8}\text{Sn}_{0.2})\text{TiO}_4$  ceramics with additives, *Jpn. J. Appl. Phys.* 37 (1998) 5367–5371.
- [9] L. Pang, H. Wang, D. Zhou, X. Yao, A new temperature stable microwave dielectric with low-firing temperature in  $\text{Bi}_2\text{MoO}_6$ – $\text{TiO}_2$  system, *J. Alloys Compd.* 493 (2010) 626–629.
- [10] Y. Wu, X. Zhao, F. Li, Z. Fan, Evaluation of mixing rules for dielectric constants of composite dielectrics by MC-FEM calculation on 3D cubic lattice, *J. Electroceram.* 11 (2003) 227–239.