

Microwave dielectric properties of BiNbO₄ ceramics with CuO–V₂O₅ addition

Hong Ryul Lee^a, Ki Hyun Yoon^{a,d,*}, Eung Soo Kim^b, Ji Won Choi^c, Richard Boucher^d

^a School of Advanced materials Engineering, Yonsei University, Seoul 120-749, Republic of Korea

^b Department of Materials Engineering, Kyonggi University, Suwon 442-769, Republic of Korea

^c Thin Film Materials Research Ctr., Korea Institute of Science and Technology, Seoul, 139-650, Republic of Korea

^d Institute of Materials Science, Technical University of Dresden, 01062 Dresden, Germany

Available online 4 May 2011

Abstract

BiNbO₄ ceramics were developed by using CuO–V₂O₅ as a liquid phase sintering agent. The resultant dielectric properties were analyzed in terms of the densification and the amount of CuO–V₂O₅ sintering agent. The addition of 0.8 wt.% CuO–V₂O₅ as its sintering agent was observed to perform most satisfactory. At 850 °C, uniform and enhanced microstructure was observed for the BiNbO₄ specimen with 0.8 wt.% CuO–V₂O₅ addition. Furthermore, the effect of CuO–V₂O₅ addition on the microwave dielectric properties of BiNbO₄ was also investigated. As the sintering temperature increased to 900 °C, the dielectric constant increased but nearly constant and the quality factor (*QF*) showed a maximum at 850 °C and then decreased for all compositions of the 900 °C sintered specimens. With an increase in CuO–V₂O₅ content, the temperature coefficient of frequency (*TCF*) increased in accordance with the dielectric mixing rule and microstructural behavior.

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Keywords: A. Sintering; C. Dielectric properties; Chemical synthesis; Microstructure

1. Introduction

With the rapid progress in commercial wireless communication, the miniaturization of mobile communication terminals and components has become increasingly important. The application of multilayer microwave devices will contribute to the realization of this aim [1]. So far effort has been concentrated on the fabrication of a dielectric material within the multilayered integrated circuit. During the fabrication of multilayer microwave devices, low-firing microwave dielectric materials with high *QF* values are necessary for its co-firing process with low-loss, low-melting point conductors such as silver and copper. The most popular method of achieving this goal involves, both using low temperature sintering agents and mixing compositions with different dielectric properties [2,3]. By combining two or more

components, a near-zero *TCF* and high *QF* values can be obtained.

Numerous dielectric compounds including Nb₂O₅ and their solid solutions have been investigated in the microwave frequency range [4–6]. The niobate based materials are candidates for microwave dielectrics due to their low cost and high quality factor [6]. Among a large number of niobate based compositions, BiNbO₄ was selected for this study. BiNbO₄ exhibits a dielectric constant of ~40, a *QF* ~10,000 GHz, and a *TCF* ~+15 ppm/°C [7]. BiNbO₄ ceramics can be sintered at low temperature and still have good microwave dielectric properties. Their sintering temperature can be controlled by a small addition of CuO–V₂O₅ as a sintering agent [8]. However, a systematic investigation of compositional details, the dielectric properties of BiNbO₄ ceramics and sintering agents are necessary for designing dielectric compositions. Moreover, a modification of the *TCF* is necessary because of the large negative value of the coefficient. Because of the high *QF* and negative *TCF* value of BiNbO₄, an appropriate mixture of BiNbO₄ and CuO–V₂O₅ could be expected to provide both a high *QF* value and temperature stable resonant frequency. In this study, the influence of CuO–

* Corresponding author at: School of Advanced materials Engineering, Yonsei University, Seoul 120-749, Republic of Korea.
Tel.: +82 31 812 0778; fax: +82 31 812 0778.

E-mail address: khyyoon@yonsei.ac.kr (K.H. Yoon).

V_2O_5 as a sintering agent on the microwave dielectric properties of $BiNbO_4$ was investigated as a function of sintering temperature and composition.

2. Experimental procedures

Mixed oxide powders of $BiNbO_4$ with $CuO-V_2O_5$ as a sintering agent were prepared from Bi_2O_3 , Nb_2O_5 , CuO and V_2O_5 with purity higher than 99.5% by a conventional mixed-oxide method. First, $BiNbO_4$ was synthesized through the calcination of $Bi_2O_3-Nb_2O_5$ at $750^\circ C$ for 3 h. CuO and V_2O_5 were also calcined in order to synthesize $CuO-V_2O_5$ as the sintering agent at $500^\circ C$ for 5 h. The final compositions were batched and then wet mixed with ZrO_2 balls for 24 h in ethanol. After drying, the reagent was calcined at $800^\circ C$ for 3 h. The calcined powders were milled again with ZrO_2 balls for 24 h in ethanol and then sieved using an 80-mesh screen. Prepared powders were dried in an oven ($100^\circ C$) for 24 h and pressed into disks, where a pressing pressure of 1450 kg/cm^2 was used for all specimens in the cold isostatic pressing process. Specimens were then sintered at $830\text{--}920^\circ C$ for 3 h at a heating rate of $200^\circ C/\text{min}$. Crystalline phases of the sintered specimens were identified by X-ray powder diffraction (Rigaku D/Max-3 C, Japan) using $Cu\ K\alpha$ radiation ($\lambda = 1.5418\text{ \AA}$) with $40\text{ kV}/30\text{ mA}$, a sampling width of 0.02° , and scan speed of $4^\circ/\text{min}$ in the 2θ range of $10\text{--}80^\circ$. Microstructures of the specimens were studied by scanning electron microscopy (SEM, Hitachi S-4200, Japan). Microwave dielectric properties of the specimens were measured by the post resonant method using the TE_{011} mode [9].

3. Results and discussion

Fig. 1 shows the DTA curve of $BiNbO_4$ powders for a heating rate of $5^\circ C/\text{min}$.

Fig. 2 shows the XRD patterns of $BiNbO_4$ calcined at $850^\circ C$ and $1150^\circ C$ for 3 h, showing orthorhombic and triclinic crystal

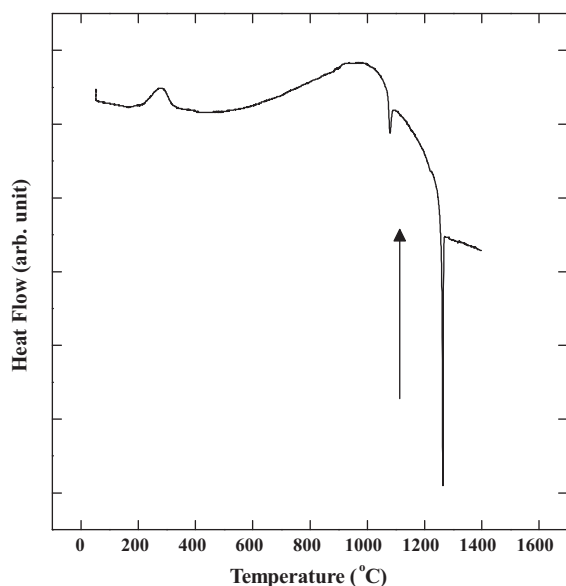


Fig. 1. DTA curves of $BiNbO_4$ powders. (heating rate: $5^\circ C/\text{min}$).

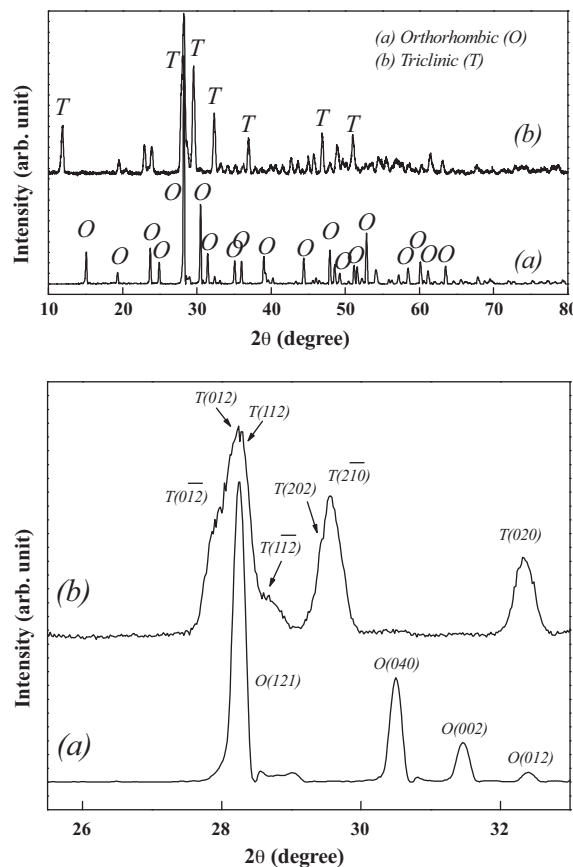


Fig. 2. XRD patterns of $BiNbO_4$ specimens calcined (a) at $850^\circ C$ for 3 h and (b) at $1150^\circ C$ for 3 h, showing crystal structures of orthorhombic and triclinic, respectively.

structures, respectively. In these figures, the phase change from the low temperature orthorhombic phase to the high temperature triclinic phase can be observed as its temperature increases and the phase transition temperature seems to be about $1079^\circ C$. In this work, therefore, the effect of $CuO-V_2O_5$ on the sintering behavior was studied for the composition of $BiNbO_4$ in order to lower the sintering temperature to $\sim 850^\circ C$,

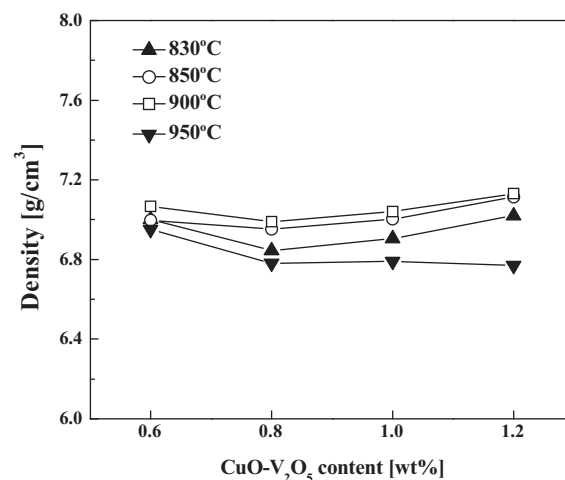


Fig. 3. Bulk density of $BiNbO_4$ specimens as a function of $CuO-V_2O_5$ content sintered at $830\text{--}900^\circ C$ for 3 h.

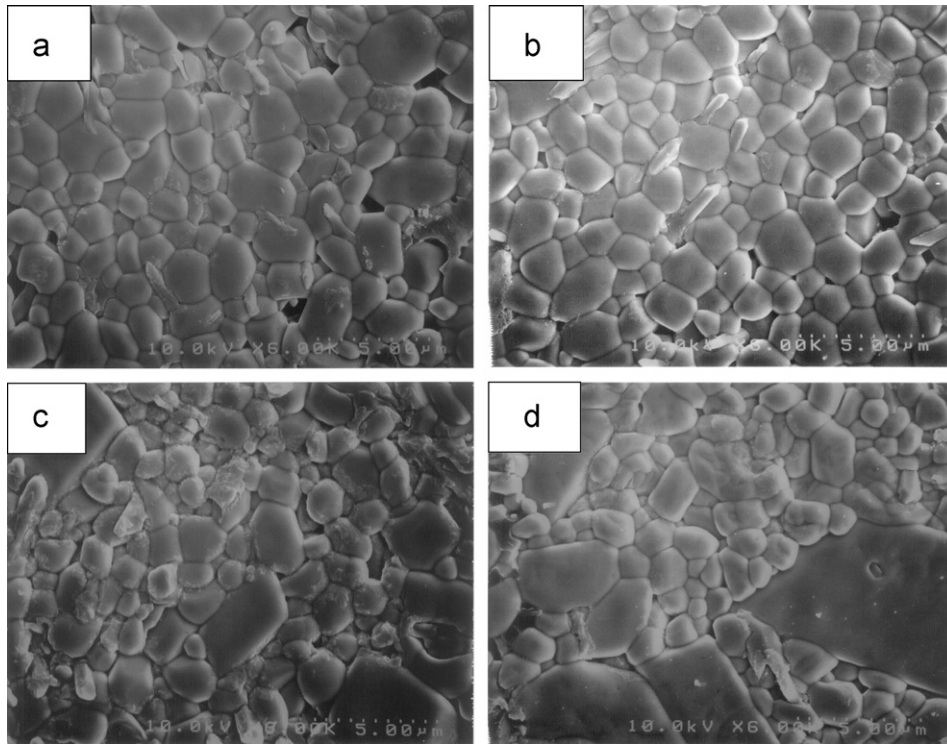


Fig. 4. SEM micrographs of BiNbO₄ specimens as a function of CuO–V₂O₅ content; (a) 0.6 wt.%, (b) 0.8 wt.%, (c) 1.0 wt.%, (d) 1.2 wt.% sintered at 850 °C for 3 h.

for a possible co-firing process with internal conductors below the melting temperature of the metals such as Ag and Cu. The bulk densities of the BiNbO₄ specimens as a function of CuO–V₂O₅ content and sintering temperature are given in Fig. 3. Except for the 950 °C sintered specimens, the densities of the

specimens remain initially almost unchanged and then increase a little with increasing CuO–V₂O₅ content due to the low melting point of CuO–V₂O₅ (m.p. = 650 °C) [10]. Fig. 3 also shows the densities as a function of sintering temperature. With an increase of sintering temperature, the low temperature

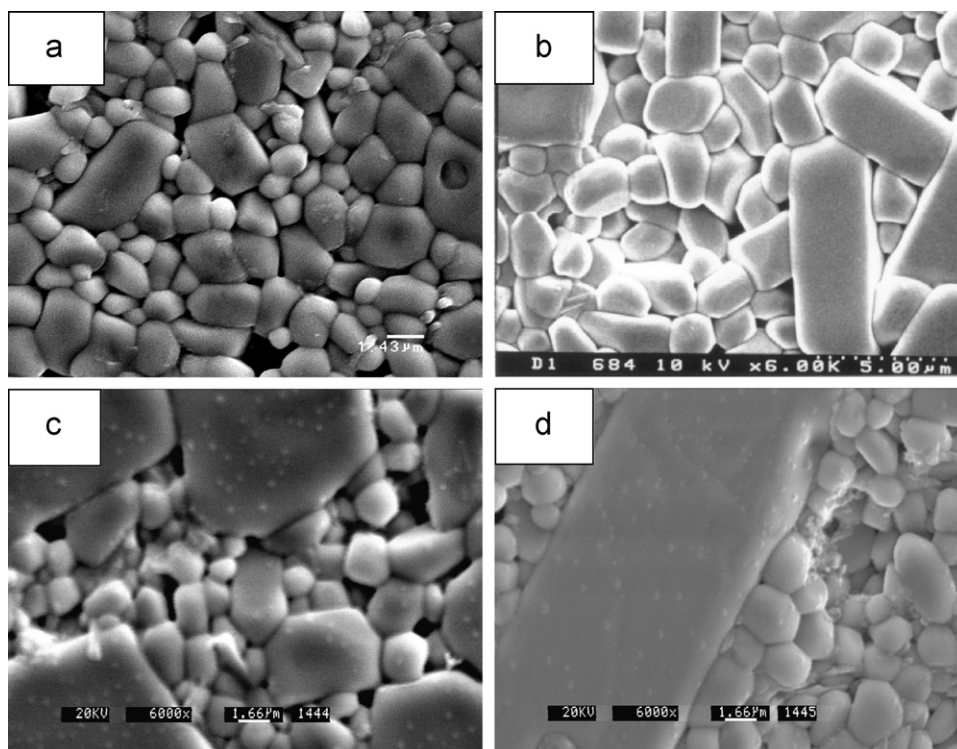


Fig. 5. SEM micrographs of BiNbO₄ specimens as a function of CuO–V₂O₅ content; (a) 0.6 wt.%, (b) 0.8 wt.%, (c) 1.0 wt.% and (d) 1.2 wt.% sintered at 900 °C for 3 h.

sintering behavior appears effectively with the addition of $\text{CuO-V}_2\text{O}_5$ and reaches a maximum value at 900°C . This figure shows that the densification with $\text{CuO-V}_2\text{O}_5$ at 900°C is higher than that at 950°C , which suggests that a temperature higher than 900°C is unnecessary. This result reveals that a significant reduction in the sintering temperature of BiNbO_4 is possible with $\text{CuO-V}_2\text{O}_5$ addition as a sintering agent while maintaining high density.

Figs. 4 and 5 show the SEM micrographs of BiNbO_4 ceramics with different amounts of $\text{CuO-V}_2\text{O}_5$ addition, and sintered for 3 h at 850°C and 900°C , respectively. When sintered at 850°C , a small and regular grain size ($1\text{--}3\ \mu\text{m}$) was easily observed for the 0.6 and 0.8 wt.% $\text{CuO-V}_2\text{O}_5$ -added specimens. However, in Fig. 4(c) and (d), abnormal grain growth could be detected, and this behavior seems to be the result of the liquid phase sintering due to the melting of $\text{CuO-V}_2\text{O}_5$. In Fig. 5, the abnormal grain growth due to liquid phase sintering is observed even in the specimen of 0.8 wt.% $\text{CuO-V}_2\text{O}_5$. Moreover it occurs more strongly than in Fig. 4 because of the higher sintering temperature. It seems that Cu and V form liquid phases during the sintering stage. For liquid phase sintering, the liquid phase is resident or disappears in the final stages. This suggests that the secondary phase could appear at the grain boundary or inside the grain, and that the phases would be rich in Cu and V. However, the secondary phases were not identified by XRD since detection of a minor phase by XRD was extremely difficult and its composition was very complex [11], and, therefore, further research is required. This fact is in accord with a previous report which suggested the formation of a residual phase containing Cu as the liquid phase of Cu-doped BiNbO_4 ceramics [12].

Fig. 6 shows the microwave dielectric properties of BiNbO_4 ceramics with $\text{CuO-V}_2\text{O}_5$ addition sintered at 850°C and 900°C for 3 h. The dielectric constants are nearly constant, and the QF values decrease with an increasing addition of $\text{CuO-V}_2\text{O}_5$. After reaching a maximum at the composition of 0.8 wt.% $\text{CuO-V}_2\text{O}_5$, the QF decreases when sintered at 850°C . The QF values are generally known to be affected by the morphology of the specimens such as grain size and uniformity. Therefore, the decrease in its QF is thought to be due to the non-uniform microstructure caused by the abnormal grain growth resulting from liquid phase densification seen in Figs. 4 and 5. The TCF increased gradually with increasing $\text{CuO-V}_2\text{O}_5$ content. The TCF is known to be related to the composition and the second phase of the ceramic samples. No significant difference was observed in the TCF value between the specimens prepared at different sintering temperatures. However, the TCF value become more positive with increasing $\text{CuO-V}_2\text{O}_5$ content due to the effect of V_2O_5 and the subsequent formation of its liquid phase in sintering stage. This is in agreement with the reports of the previous studies on BiNbO_4 and MgNb_2O_6 ceramics [13,14]. Therefore, it is believed from this result that the TCF value of BiNbO_4 ceramics can be adjusted to near-zero by carefully controlling the content of $\text{CuO-V}_2\text{O}_5$.

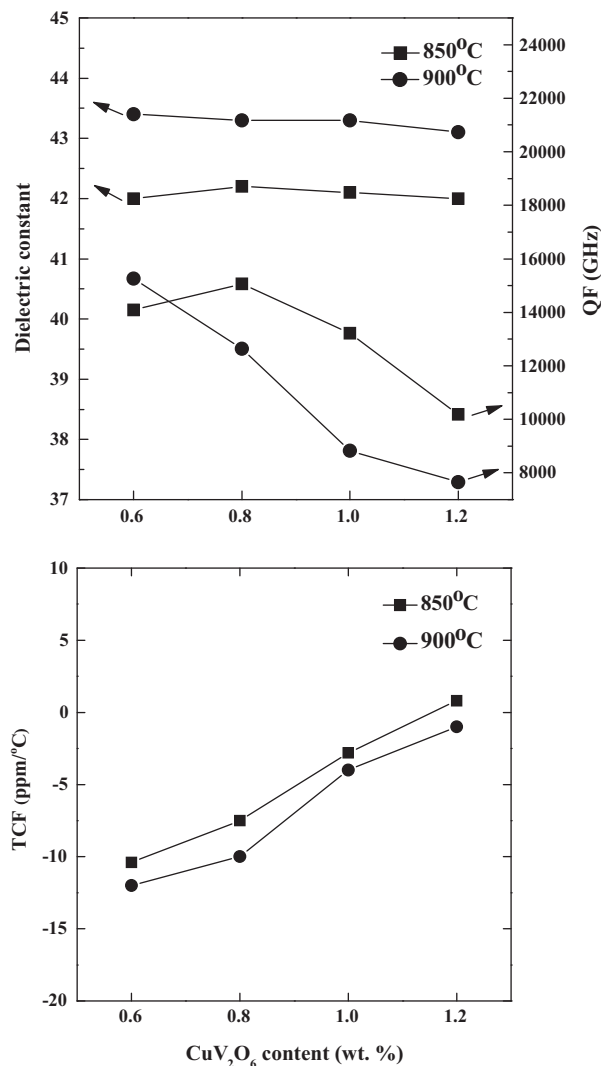


Fig. 6. Dielectric constant, quality factor (QF) and temperature coefficient of resonant frequency (TCF) of BiNbO_4 specimens sintered at 850°C and 900°C for 3 h as a function of $\text{CuO-V}_2\text{O}_5$ content.

4. Conclusion

The addition of $\text{CuO-V}_2\text{O}_5$ as a sintering agent to BiNbO_4 lowered the sintering temperature to $850\text{--}900^\circ\text{C}$. The dielectric constants remain almost constant and the QF values of the specimens with $\text{CuO-V}_2\text{O}_5$ changed with increasing $\text{CuO-V}_2\text{O}_5$ content. This can be attributed to the occurrence of liquid phase densification. The TCF increased gradually with increasing $\text{CuO-V}_2\text{O}_5$ content. Therefore, it is suggested that the TCF of BiNbO_4 -based ceramics can be adjusted to near-zero by carefully controlling the content of $\text{CuO-V}_2\text{O}_5$. Typically, BiNbO_4 with 0.8 wt.% $\text{CuO-V}_2\text{O}_5$ sintered at 850°C , showed the microwave dielectric properties of $\epsilon = 42$, $QF = 15,500\ \text{GHz}$ and $TCF = -4\ \text{ppm}/^\circ\text{C}$.

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