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In-situ formation of carbon nanotubes in pyrolytic carbon—silicon nitride composite ceramics

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Abstract

Carbon nanotube reinforced pyrolytic carbon/silicon nitride (CNT-PyC/Si $_3$ N $_4$) composite ceramics were fabricated through in-situ growth of CNTs in PyC-Si $_3$ N $_4$ ceramics by precursor infiltration and pyrolysis. CNTs were in-situ formed by the addition of nano-sized Ni into phenolic resin and Si $_3$ N $_4$ powder blend, and the content of CNTs increased with the increase of Ni content. Due to the formation of CNTs in the interparticle pores of CNTs/PyC-Si $_3$ N $_4$ ceramic, the PyC wrapped Si $_3$ N $_4$ particles were bridged by CNTs, which led to the increase of electrical conductivity. Different from the previously reported PyC-Si $_3$ N $_4$ ceramics fabricated by chemical vapor infiltration (CVI), the PyC-Si $_3$ N $_4$ ceramics exhibited a shielding mechanism dominated by absorption. Compared to PyC-Si $_3$ N $_4$ ceramics prepared with same procedure, the shielding effectiveness of CNTs-PyC/Si $_3$ N $_4$ increased significantly with the formation of CNTs. With the increase of CNT content, the shielding effectiveness of CNTs/PyC-Si $_3$ N $_4$ ceramics increased from 25.5 to 43.6 dB, in which the absorption shielding effectiveness increased from 15 to 30 dB over the frequency range of 8.2–12.4 GHz.

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1. Introduction

Recently, lots of researches have been carried out to investigate the electromagnetic (EM) shielding for the purpose of protecting environment and sensitive devices from electromagnetic interference (EMI) [1–6]. A traditional way to eliminate EMI is to use metal as a shielding material [7,8]. However, the shielding mechanism of metal materials is mainly reflected due to the mobile charge carriers and high electrical conductivity (σ). The reflected EM wave from shielding material could also interfere with the devices. As a comparison, ceramic is more suitable to be used as shielding material than metal in harsh environment, which is attributed

to the unique properties of ceramics such as low density, good oxidation resistance, relatively high hardness, thermal-chemical corrosion resistance, good machinability, high creep resistance, and high thermal shock resistance [9-13]. Compared with ceramics, carbon possesses comparatively high electrical conductivity, low density, improved EM absorption property, and good environment stability [14], so carbon and ceramic hybrid materials are promisingly used as shielding material in harsh environment instead of ceramic. In our previous work, the EM shielding properties of pyrolytic carbon reinforced silicon nitride (PyC-Si₃N₄) composite ceramics fabricated by chemical vapor infiltration (CVI)[15] and precursor infiltration pyrolysis (PIP)[16] methods have been investigated. It was found that the high electrical conductivity of PyC-Si₃N₄ ceramic fabricated by the CVI method always led to a relatively high reflection shielding effectiveness (SE_R) compared with absorption shielding effectiveness (SE_A) .

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Table 1

PyC content, density, porosity, sample thickness, electrical conductivity and EMI SE of PyC/Si₃N₄ composite ceramic fabricated by CVI and PIP methods.

Fabrication process	PyC content (vol%)	SE_T (dB)	SE_A (dB)	SE_R (dB)	Sample thickness (mm)	Porosity (%)	Density (g/cm ³)	Electrical conductivity (S/m)
CVI	12.1	26.3	5.3	21.0	0.7	31.7	1.99	2.6×10^4 4.2
PIP	4.0	13.0	8.0	5.0	2.0	10.2	2.70	

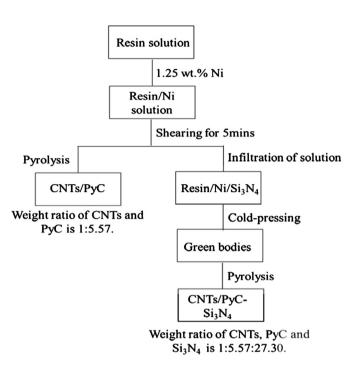


Fig. 1. Schematic illustration of experimental procedure.

The PyC–Si $_3$ N $_4$ ceramics fabricated by the PIP method possessed a relatively high SE_A compared to SE_R owing to the lower electrical conductivity. However, the overall shielding property of the material was relatively low (Table 1). Usually, a total shielding effectiveness (SE_T) of 30 dB, corresponding to 99.9% attenuation of the EMI radiation, is considered as an adequate level of shielding for many applications [17]. Carbon nanotubes (CNTs) as an excellent EM wave absorber (CNTs) have been widely used in polymer-based materials for EMI shielding [18–20]. However, the EMI SE of CNT reinforced Si $_3$ N $_4$ ceramics has not been reported due to the difficulties in dispersing CNTs, which are apt to agglomerate, and in avoiding the damage on CNTs at high fabrication temperatures [21].

In the present work, $PyC-Si_3N_4$ composite ceramics reinforced by CNTs (CNTs/PyC-Si₃N₄) were fabricated through in-situ growth of CNTs by pyrolysis of phenolic resin containing Ni catalyst with the PIP method. The aim of this work is to fabricate a novel Si_3N_4 based shielding composite ceramic which possesses higher SE_A and low SE_R . In this work, the effects of Ni loadings on the content of CNTs, on the microstructure of $PyC-Si_3N_4$, on the electrical conductivity and EMI SE of the as-prepared materials are investigated, respectively.

2. Experimental procedure

2.1. Preparation of CNTs-PyC materials

Fig. 1 shows the schematic illustration of experimental procedure. Phenolic resin (PF 2313, purity > 96.5% Xi'an resin factory, Xi'an, China), ethanol and hexamethylenetetramine $(C_6H_{12}N_4)$ which acts as a curing agent, were mixed by a weight ratio of 10:10:1, and nano-sized Ni particles (mean particle size 50 nm, purity > 99.9%) were prepared by a weight ratio of 0, 0.25, 0.50, 0.75 and 1.25 wt% of phenolic resin, respectively. When the phenolic resin was uniformly dissolved in ethanol, the Ni powders were added into phenolic resin solution, and then the different Ni contained phenolic resin solution samples were sheared with an emulsifier at a speed of 7000 r/min for 5 min. After dried for 48 h at 80 °C, the phenolic resin specimens with different catalyst were pyrolysed at 1000 °C for 2 h. The heating rate was 5 °C/min. In this experiment, the formation of CNTs could lead to the increase in carbon yield of phenolic resin. To vary the carbon yield of phenolic resin with different Ni catalyst, the carbon vield is defined as follows:

Carbon yield
$$\% = \frac{W_{CP}}{W_{PR}} \times 100$$
 (1)

where W_{PR} and W_{CP} are the weight of phenolic resin and carbon phase (PyC or CNTs/PyC) derived from pyrolysis of phenolic resin, respectively.

2.2. Preparation of CNTs/PyC-Si₃N₄ ceramics

Phenolic resin solution with 0–1.25 wt% Ni loadings was infiltrated into Si_3N_4 (mean particle size of 1.2 µm, α - $Si_3N_4 > 95\%$), and the weight ratio of phenolic resin and Si_3N_4 was 3:7. When dried for 48 h at 80 °C, the obtained Si_3N_4 and phenolic resin blend was cold-pressed into green bodies and pyrolyzed in Ar at 1000 °C for 2 h. The heating rate was also 5 °C/min. After pyrolysis, the as-received porous CNTs/PyC–Si₃N₄ ceramics were machined into specimens, which were designated as samples A, B, C, D and E, corresponding to 0, 0.25, 0.5, 0.75 and 1.25 wt% Ni content of phenolic resin in the green bodies, with dimensions of 22.86 mm (length) × 10.16 mm (width) × 2 mm (thickness).

2.3. Compositional and microstructural characterization

X-ray diffraction (XRD) was employed for phase analysis (X'Pert Pro, Philips, Netherlands). INVIN Raman spectroscopy (RMS; Renishaw, UK) was used to characterize the

graphitization degree of CNTs/PyC. The microstructure of the samples was observed by scanning electron microscopy (SEM; S-4700, Hitachi, Tokyo, Japan). Transmission electron microscope (TEM; G-20, FEI-Tecnai, Hillsboro, USA) was employed to characterize the microstructure of CNTs.

2.4. Electrical and EM shielding property characterization

Electrical conductivity was measured by the two-wire method using a current source (Keithley 6220 DC, Ohio, USA). Scattering parameters (S-parameters, S_{11} and S_{21}) in 8.2–12.4 GHz were measured by a vector network analyzer (VNA; MS4644A, Anritsu, Kana-gawa, Japan) using the waveguide method. In this work, total shielding properties were assessed by SE_T . SE_R and SE_A were calculated according to the measured reflected (R) and transmitted (T) coefficients:

$$SE_R = -10 \times \log_{10}(1-R)$$
 (2)

$$SE_A = -10 \times \log_{10}(T/(1-R))$$
 (3)

$$SE_T = SE_A + SE_R \tag{4}$$

where R and T are calculated according to

$$R = |S_{11}|^2, \ T = |S_{21}|^2 \tag{5}$$

3. Results and discussion

3.1. Effect of Ni loadings on the content of CNTs in CNTs/PyC

The addition of Ni catalyst could lead to an increase in carbon yield. Fig. 2 displays the TGA and DSC curves of phenolic resin containing 0 and 1.25 wt% Ni catalyst. At the temperatures higher than 130 $^{\circ}$ C, the weight of the system began to decrease with H₂O molecular evaporating out [22]. When the temperature reached 200 $^{\circ}$ C, CO₂ and CO were released. According to TGA results, the weight loss mainly

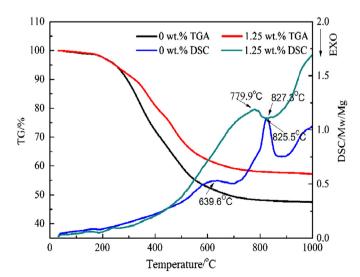


Fig. 2. TGA and DSC curves of phenolic resin containing 0 and 1.25 wt% Ni catalyst.

happened in the temperature range of 300-600 °C. In this stage, gaseous products such as H₂, CH₄, CO₂ and other hydrocarbon gases evaporated out of phenolic resin [22]. With the temperature increasing, the weight loss of phenolic resin increased gradually. At temperatures above 900 °C, the carbonization process has apparently gone to completion. After pyrolysis, phenolic resin exhibited a carbon yield of 47.46 wt%, which increased to 56.00 wt% for phenolic resin containing 1.25 wt% Ni. During the pyrolysis, when the gaseous hydrocarbon evaporating out of phenolic resin passed over Ni catalyst, decomposition of hydrocarbon was achieved on the catalyst surface, and then CNTs were in-situ formed (Fig. 3). Fig. 3(a) and (b) shows the SEM images of PyC and CNTs/ PyC derived from pyrolysis of pure phenolic resin and phenolic resin containing 1.25 wt% Ni catalyst. In Fig. 3(b), with the addition of Ni catalyst, plenty of CNTs was in-situ formed. Fig. 3(c) shows the TEM image of a single CNT. The CNTs exhibited apparent burls, indicating a growth mechanism of carbon nanoparticles—nanowires—nanotubes. Similar growth mechanism was reported in the literatures [23,24], in which the CNTs were prepared by floating and detonationassisted CVD methods. Fig. 3(d) shows HRTEM micrograph of a multi-walled microstructure of CNTs. Table 2 lists the carbon yield of phenolic resin containing 0-1.25 wt% Ni catalyst after pyrolysis at 1000 °C. In Table 2, W_R is the gross residual weight of phenolic resin containing different contents of Ni catalyst and W_{CP} as carbon phase, in which the weight of Ni is subtracted from W_R . When the Ni content varied from 0 to 1.25 wt%, the carbon yield increased from 47.46 to 56.00 wt%, in which content of CNTs increased from 0 to 8.54 wt%.

In Fig. 2, the DSC curve of pure phenolic resin shows two endothermic peaks in the vicinity of 639.6 °C and 828.5 °C. These two peaks are associated with the thermal decomposition of hydrocarbon evaporating out of phenolic resin [25]. Compared with the DSC curve of pure phenolic resin, the weak endothermic peak at 639.6 °C disappeared in that of phenolic resin containing 1.25 wt% Ni, the endothermic peak at 828.5 °C turned smaller in intensity and the corresponding temperature shifted to 778.9 °C, and an exothermic peak appeared at 827.3 °C, which was not observed for the pure resin. With the addition of Ni, the apparent activation energy of decomposition reaction can be obviously reduced while the hydrocarbon decomposition takes place on the catalyst surface [26]. Therefore, the first weak peak at 639.6 °C disappeared and the second peak turned correspondingly weaker due to the addition of Ni catalyst. For synthesizing CNTs, typically, nanometer-size metal particles are required to enable hydrocarbon decomposition at a lower temperature than the spontaneous decomposition temperature of the hydrocarbon [27], so the endothermic peak at 828.5 °C decreased to 778.9 °C with the addition of catalyst. The growth of MWCNT is a graphitization process of amorphous carbon. The graphitization behavior of amorphous carbon mainly consists of two steps: (i) the growth of small graphitic crystallites and (ii) reorientation and merging of the crystallites to form a threedimensional graphitic order [28]. During this process, the excess free energy of the amorphous state relative to the stable

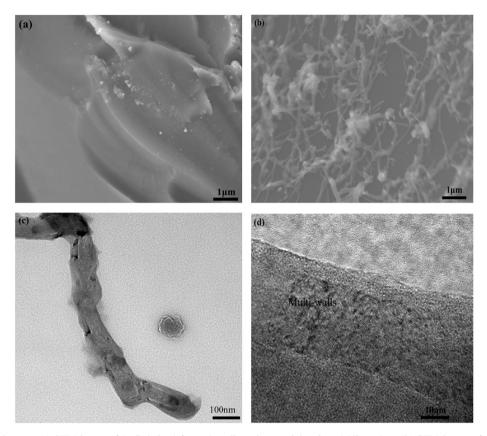


Fig. 3. SEM and TEM images, (a) SEM image of PyC derived from phenolic resin containing 0 wt% Ni catalyst, (b) SEM image of CNTs/PyC derived from phenolic resin containing 1.25 wt% Ni catalyst, (c) TEM image of a single CNT, (d) HRTEM image of CNT.

Table 2 Carbon yield of phenolic resin samples containing 0–1.25 wt% Ni catalyst.

Ni content (wt%) in phenolic resin	0	0.25	0.50	0.75	1.25
W_R (wt%)	47.46	48.28	52.00	56.49	57.25
W_{CP} (wt%)	47.46	48.03	51.50	55.74	56.00

crystalline phase is instantaneously released [29,30], leading to the appearance of the exothermic peak for phenolic resin containing 1.25 wt% Ni catalyst.

Fig. 4 shows the XRD pattern of PyC and CNTs/PyC samples derived from pyrolysis of phenolic resin containing 0–1.25 wt% Ni. An obvious peak of C(002) plane from CNTs at 2θ of 26.5° [20] appeared with the addition of Ni catalyst. With the increase in content of Ni catalyst, the intensity of the carbon peak increased gradually. Obviously, the formation of CNTs could lead to an improvement in the graphitization degree of the CNTs/PyC, and the graphitization degree increased with the increase of CNT content. It is known that higher intensity of C(002) peak is indicative of a more improved graphitic degree [31]. Therefore, with the increase of Ni content, the content of CNTs formed in CNTs/PyC increased gradually.

The Raman spectra of PyC derived from phenolic resin and CNTs/PyC samples derived from phenolic resin containing 0.25–1.25wt% Ni exhibited D-peak at around 1356 cm⁻¹ associated with defects and disorder degree, and G-band at

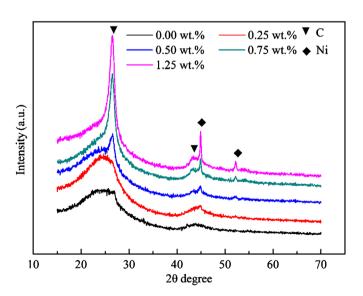


Fig. 4. XRD pattern of PyC and CNTs/PyC derived from pyrolysis of phenolic resin containing 0, 0.25, 0.5, 0.75 and 1.25 wt% Ni catalyst.

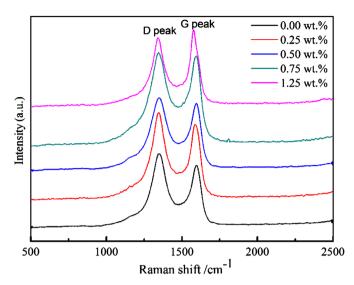


Fig. 5. Raman spectrum of PyC and CNTs/PyC derived from pyrolysis of phenolic resin containing 0, 0.25, 0.5, 0.75 and 1.25 wt% Ni catalyst.

around 1582 cm⁻¹ corresponding to the signal from graphite (Fig. 5). The graphitization degree of PyC and CNTs/PyC samples can be determined by the $I_D:I_G$ ratio. The lower the D:G ratio is, the higher graphitization degree of the samples. The PyC sample had a D:G ratio of 1.156, while the CNTs/PyC samples derived from phenolic resin containing 0.25–1.25wt% Ni attained D:G ratios of 1.136, 1.070, 1.031 and 0.912, respectively. The Raman spectra indicate that the content of CNTs increased with the increase of Ni content in the phenolic resin, which is consistent with the XRD patterns.

3.2. Formation of CNTs in Si₃N₄ ceramics

When the effect of Ni loadings on the content of CNTs was obtained, CNTs were in situ formed by infiltration and pyrolysis of phenolic resin containing Ni catalyst in Si₃N₄. After pyrolysis at 1000 °C, CNTs/PyC-Si₃N₄ composite ceramics were obtained. Fig. 6(a)-(e) shows the SEM images of CNTs/PyC-Si₃N₄ ceramic derived from pyrolysis of green bodies containing 0-1.25 wt% Ni in phenolic resin. PyC was uniformly distributed among Si₃N₄ particles in sample A (Fig. 6(a)). Owing to the addition of Ni catalyst in samples B-E (Fig. 6(b)-(e)), CNTs were in-situ formed in the pores of PyC-Si₃N₄ ceramic. With the increase of Ni content, the content of CNTs increased gradually, which is consistent with the variation in CNTs/PyC. Fig. 6(f) exhibits the TEM image of CNT formed in CNTs/PyC-Si₃N₄. The black particles wrapped in CNTs were Ni catalyst with a particle size of 40–60 nm. In the TEM image, obvious burl of CNT appeared between Ni particles, which exhibited the same growth mechanism as the one in CNTs/PyC. Fig. 7 shows the XRD pattern of PyC-Si₃N₄ ceramic (sample A) and CNTs/PyC-Si₃N₄ ceramic (sample E). Compared with sample A, the intensity of weak carbon peak at 2θ of $20-30^{\circ}$ of sample E increased slightly. Since the intensity of Si₃N₄ peak was highly intense, the carbon peak intensity was correspondingly weakened. Additionally, the weight percentage of CNTs in $PyC-Si_3N_4$ was less due to the small weight ratio of phenolic resin to Si_3N_4 in the green bodies. The content of CNTs in CNTs/PyC-Si₃N₄ samples derived from pyrolysis of green bodies with phenolic resin containing 0–1.25 wt% Ni catalyst is listed in Table 3.

3.3. Effect of Ni content on electrical conductivity

Fig. 8 shows the electrical conductivity of PyC–Si₃N₄ and CNTs/PyC–Si₃N₄ samples A, B, C, D and E as a function of Ni content increasing from 0 to 1.25 wt% in phenolic resin. The electrical conductivity of the samples increased with the increase in CNT concentration, which varied from 16.6 to 32.1 S/m. Due to the formation of CNTs in the material, the PyC wrapped Si₃N₄ particles were bridged by CNTs. The values of electrical conductivity of Si₃N₄, PyC and CNTs are 10⁻¹³, 10 and 10⁴ S/m, respectively [32–34]. The electrical conductivity of CNTs is superior to that of PyC. In CNTs/PyC–Si₃N₄ ceramic, the bridging of PyC wrapped Si₃N₄ particles by CNTs provided the paths for the electrical current, leading to the considerable decrease of the resistance. Therefore, the increase in conductivity can be ascribed to the formation of CNTs.

3.4. Effect of Ni content on EMI SE

Shielding mechanisms of conductive shielding material include reflection, absorption and multiple reflections [35–37]. Multiple reflections are the internal reflections between the internal surfaces of the shielding material. When the shielding material is thicker than the skin depth, the multiple reflections are typically ignored. The skin depth is the distance at which the strength of electric field drops to (1/e) of the incident strength. Mathematically, this can be calculated using [36,37]

$$\delta = (\sqrt{\pi f \mu \sigma})^{-1} \tag{6}$$

where δ is the skin depth, f is the frequency, μ is the magnetic permeability ($\mu = \mu_o \mu_r$), μ_o is equal to $4\pi \times 10^{-7}$ Hm $^{-1}$, μ_r is the relative magnetic permeability and σ is the electrical conductivity of the shield. In the calculations, the relative magnetic permeability was assumed to be 1. Fig. 9 illustrates the influence of the composite conductivity on the skin depth of CNTs/PyC–Si₃N₄ composite ceramics. The results show a significant decrease in skin depth with the increase in conductivity. When the electrical conductivity increased from 16.6 to 32.1 S/m, the skin depth decreased from 1.38 to 1.00 mm, which means that the sample with thickness of 2 mm in this work is independent of the influence of multiple reflections. Therefore, the attenuation of EM radiation will be mainly attributed to the shielding by reflection and absorption.

A great deal of interacting mobile charge carriers resulting from higher concentration of CNTs could lead to a higher EMI SE, which has been demonstrated [38,39]. Fig. 10 depicts the EMI SE of CNTs/PyC–Si₃N₄ ceramic samples as a function of frequency in X-band. Compared with SE_T values of sample A, SE_T values of samples B, C, D and E increased significantly

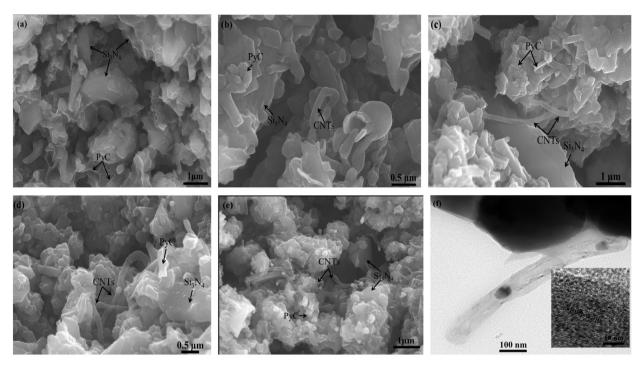


Fig. 6. SEM and TEM images, SEM images of ceramic samples A, B, C, D and E derived from pyrolysis of green bodies with phenolic resin containing 0 wt% (a), 0.25 wt% (b), 0.50 wt% (c), 0.75 wt% (d) and 1.25 wt% (e) Ni catalyst, (f) TEM image of a single CNT, in which inset shows the HRTEM image of CNT.

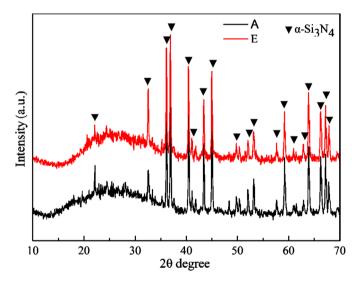


Fig. 7. XRD patterns of PyC–Si $_3N_4$ (sample A) and CNTs/PyC–Si $_3N_4$ (sample E) ceramics.

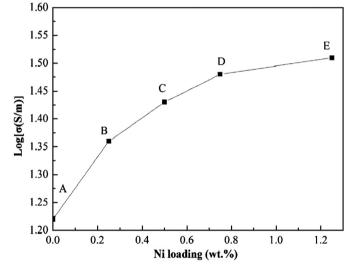


Fig. 8. Electrical conductivity of samples A, B, C, D and E as a function of Ni loading.

Table 3 Si_3N_4 , PyC, CNTs and Ni content, porosity and density of PyC- Si_3N_4 and CNTs/PyC- Si_3N_4 ceramics (samples A-E).

Sample	Si ₃ N ₄ content (wt%)	PyC content (wt%)	CNT content (wt%)	Ni content (wt%)	Porosity (vol%)	Density (g/cm ³)
A	83.10	16.90	0	0	42.70	1.67
В	82.50	16.85	0.56	0.09	42.03	1.69
C	81.65	16.74	1.43	0.18	41.16	1.70
D	80.51	16.38	2.86	0.25	40.02	1.72
E	80.30	16.33	2.94	0.43	39.41	1.73

and the values of SE_T increased with the increase of Ni content. To exclude the influence of Ni content on SE_T of PyC-Si₃N₄ ceramics containing different contents of Ni catalyst, the mean values of SE_T and the complex permittivity of 0–1.25 wt% Ni contained paraffin samples were measured (Table 4). The SE_T and the complex permittivity of Ni/paraffin samples were found to be constant with the variation of Ni content, which were attributed to the low content of Ni. Therefore, the increase in SE_T of samples B, C, D and E was ascribed to the contribution of CNTs, which leads to the increase in SE_T from 25.5 dB to 43.6 dB.

Fig. 10(b) shows that SE_A increased with the increasing CNT content. The increase in absorption by increasing CNT concentration is a well-established concept which can be ascribed to higher amount of mobile charge carriers at higher MWCNT concentrations [38–40]. Additionally, the connectivity of CNTs in

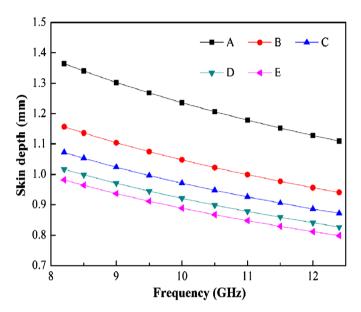


Fig. 9. Skin depth of samples A, B, C, D and E as a function of frequency.

CNTs/PyC-Si₃N₄ could also contribute to the shielding by absorption [41].

For shielding by reflection, the material should have mobile charge carriers (electrons or holes) to interact with incident electromagnetic wave [39]. In Fig. 10(c), the shielding by reflection increased with the increase in CNT content, which can be related to higher amount of mobile charge carriers at greater MWCNT concentrations. As there is a direct relationship between electrical conductivity and shielding by reflection in conductive monolithic materials [35,37], a higher SE_R is expected in high-concentration CNT contained samples.

3.5. Experimental results versus theoretical predications of EMI SE

Theoretically, the EMI SE of shielding materials can be calculated through the following equations [35,36]:

$$SE_T = SE_R + SE_A + SE_{MR} (7)$$

$$SE_R = 39.5 + 10\log\frac{\sigma}{2\pi f \mu} \tag{8}$$

$$SE_A = 8.7 \frac{d}{\delta} = 8.7 d\sqrt{\pi f \mu \sigma} \tag{9}$$

$$SE_{MR} = 20\log|1 - e^{-2d/\delta}|$$
 (10)

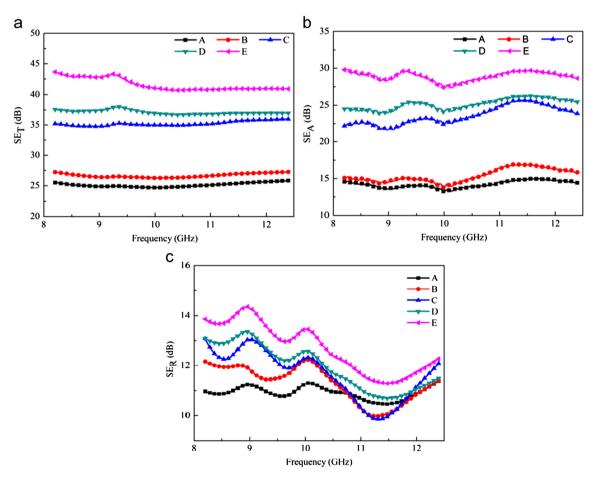


Fig. 10. EMI SE of PyC-Si₃N₄ and CNTs/PyC-Si₃N₄ ceramics, (a) SE_T , (b) SE_A and (c) SE_R of samples A, B, C, D and E as a function of frequency.

Table 4 The mean values of SE_T and complex permittivity of Ni/paraffin specimens containing 0–1.25 wt% Ni contents.

Paraffin content (wt%)	Ni content (wt%)	Real permittivity	Imaginary permittivity	SE_T (dB)
100	0.00	2.2	4.3×10^{-2}	1.0
99.75	0.25	2.2	3.9×10^{-2}	1.0
99.50	0.50	2.2	2.8×10^{-2}	1.0
99.25	0.75	2.2	3.2×10^{-2}	1.0
98.75	1.25	2.2	4.0×10^{-2}	1.0

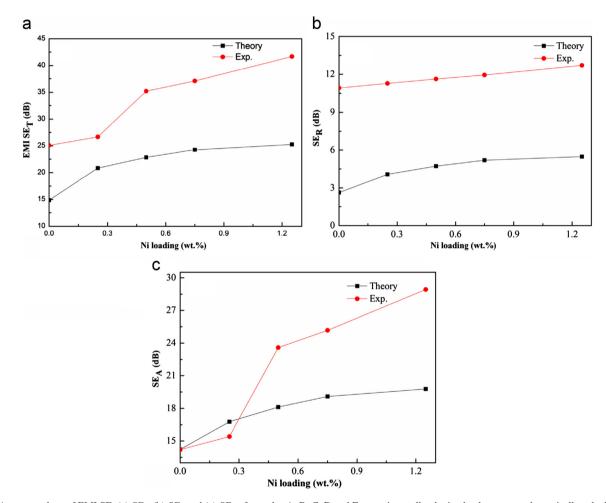


Fig. 11. Average values of EMI SE, (a) SE_T , (b) SE_R and (c) SE_A of samples A, B, C, D and E, experimentally obtained values versus theoretically calculated values as a function of Ni loading.

where SE_{MR} is the shielding by multiple reflections. The calculation of the EMI SE from the above equations is according to the sample thickness, electrical conductivity, magnetic permeability and the EM radiation frequency. When SE_A is higher than 10 dB and the sample thickness is larger than the skin depth, SE_{MR} is always ignored [35,37]. In the present work, the mean value of SE_A is higher than 10 dB, and the sample thickness is greater than skin depth, so the theoretical value of EMI SE was calculated using the following equation:

$$SE_T = SE_R + SE_A \tag{11}$$

The above equation was derived from dense single-phase conductive materials, and there may be difference between the theoretical results and the experimental ones when the shielding materials are porous and composed of different phases [41]. The mean theoretical values and the experimental ones of SE as a function of Ni content are presented in Fig. 11. The experimental value of SE_R is obviously higher than the theoretical one, Fig. 11(b), which can be explained by the larger surface area of porous material than that of dense material [42]. The formation of CNTs in the pores could also increase the surface area. A larger surface area of conductive material could lead to a larger reflection of incident

electromagnetic wave, which leads to a higher SE_R . In Fig. 11(c), the difference between experimental and theoretical values of SE_A increased with the increase of CNT content. This difference may come from the formation of nano-interface between CNTs and PyC which could lead to a strong interfacial polarization relaxation loss, and consequently favors the absorption of microwave [43]. With the increase of CNT content, the interfacial polarization relaxation loss increased gradually and the difference increased at the same time.

4. Conclusion

CNTs were in-situ formed in CNTs/PyC-Si₃N₄ ceramics with the addition of nano-sized Ni particles. The CNT content increased with the increase of Ni loadings. The formation of CNTs in CNTs/PyC leaded to the increase of carbon yield of phenolic resin. Due to the formation of CNTs in the interparticle pores of CNTs/PyC-Si₃N₄ ceramics, the PyC wrapped Si₃N₄ particles were bridged by CNTs. With increasing CNT content, the electrical conductivity of CNTs/PyC-Si₃N₄ ceramic increased gradually. Composite ceramic exhibited a considerable increase in EMI SE with the increase in the content of CNTs in ceramics. Owing to the contribution of CNTs, SE_T of CNTs/PyC-Si₃N₄ ceramics increased from 25.5 dB to 43.6 dB. Regardless of the electrical conductivity, shielding by absorption was always found to be the major contribution to the total EMI SE. The estimated theoretical overall EMI SE was remarkably lower experimental one.

References

- B. Fugetsu, E. Sano, M. Sunada, Y. Sambongi, T. Shibuya, X.S. Wang, T. Hiraki, Electrical conductivity and electromagnetic interference shielding efficiency of carbon nanotube/cellulose composite paper, Carbon 46 (2008) 1256–1258.
- [2] M.S. Cao, W.L. Song, Z.L. Hou, B. Wen, J. Yuan, The effects of temperature and frequency on the dielectric properties, electromagnetic interference shielding and microwave-absorption of short carbon fiber/ silica composites, Carbon 48 (2010) 788–796.
- [3] Y.L. Yang, M.C. Gupta, K.L. Dudley, R.W. Lawrence, Novel carbon nanotube-polystyrene foam composites for electromagnetic interference shielding, Nano Lett. 11 (2005) 2131–2134.
- [4] Y. Huang, N. Li, Y.F. Ma, D. Feng, F.F. Li, X.B. He, X. Lin, H.J. Gao, Y.S. Chen, The influence of single-walled carbon nanotube structure on the electromagnetic interference shielding efficiency of its epoxy composites, Carbon 45 (2007) 1614–1621.
- [5] M.H. Al-Saleh, U. Sundararaj, Electromagnetic interference shielding mechanisms of CNT/Polymer composites, Carbon 47 (2009) 1738–1746.
- [6] S.L. Shi, J. Liang, The effect of multi-wall carbon nanotubes on electromagnetic interference shielding of ceramic composites, Nanotechnology 19 (2008) 255707.
- [7] M. Rosenow, J. Bell, EMI shielding effectiveness of nickel coated carbon fiber as a long fiber thermoplastic concentrate, in: Proceeding of the 43rd Inter-national SAMPE Symposium, 1998 pp. 854–864.
- [8] Z. Osawa, S. Kuwabara, Thermal stability of the shielding effectiveness of composites to electromagnetic interference. Effects of matrix polymers and surface treatment of fillers, Polym. Degrad. Stab. 35 (1992) 33–43.
- [9] H. Park, H.E. Kim, K. Niihara, Microstructural evolution and mechanical properties of Si₃N₄ with Yb₂O₃ as a sintering additive, J. Am. Ceram. Soc. 80 (1997) 750–756.

- [10] A.J. Pyzik, D.R. Beaman, Microstructure and properties of self-reinforced silicon nitride, J. Am. Ceram. Soc. 76 (1993) 2737–2744.
- [11] C. Kawai, A. Yamakawa, Network formation of Si₃N₄ whiskers for the preparation of membrane filters, J. Mater. Sci. Lett. 17 (1998) 873–875.
- [12] P.F. Becher, E.Y. Sun, K.P. Plucknett, K.B. Alexander, C.H. Hsueh, H. T. Lin, Microstructure design of silicon nitride with improved fracture toughness: I. Effects of grain shape and size, J. Am. Ceram. Soc. 81 (1998) 2821–2830.
- [13] F.L. Riley, Silicon nitride and related materials, J. Am. Ceram. Soc. 83 (2000) 245–265.
- [14] J.S. Im, J.G. Kim, Y.S. Lee, Fluorination effects of carbon black additives for electrical proper ties and EMI shielding efficiency by improved dispersion and adhesion, Carbon 47 (2009) 2640–2647.
- [15] X.M. Li, L.T. Zhang, X.W. Yin, Synthesis and electromagnetic shielding property of pyrolytic carbon-silicon nitride ceramics with dense silicon nitride coating, J. Am. Ceram. Soc. 95 (2012) 1038–1041.
- [16] X. Hao, X.W. Yin, L.T. Zhang, L.F. Cheng, Dielectric, electromagnetic interference shielding and absorption properties of Si₃N₄–PyC composite ceramics, J. Mater. Sci. Technol. 29 (2013) 249–254.
- [17] D. Markham, Shielding: quantifying the shielding requirements for portable electronic design and providing new solutions by using a combination of materials and design, Mater. Des. 21 (2000) 45–50.
- [18] Z.F. Liu, G. Bai, Y. Huang, Y.F. Ma, F. Du, F.F. Li, T.Y. Guo, Y.S. Chen, Reflection and absorption contributions to the electromagnetic interference shielding of single-walled carbon nanotube/polyurethane composites, Carbon 45 (2007) 821–827.
- [19] A. Mohammad, A. Thomas, O. Michal, S. Uttandaraman, Comparative study of electromagnetic interference shielding properties of injection molded versus compression molded multi-walled carbon nanotube/polystyrene composites, Carbon 50 (2012) 5126–5134.
- [20] Y. Huang, N. Li, Y.F. Ma, F. Du, F.F. Li, X.B. He, X. Lin, H.J. Gao, Y.S. Chen, The influence of single-walled carbon nanotube structure on the electromagnetic interference shielding efficiency of its epoxy composites, Carbon 45 (2007) 1614–1621.
- [21] C. Balazsi, B. Fenyi, N. Hegman, Z. Kover, F. Weber, Z. Vertesy, Z. Konya, I. Kiricsi, L.P. Biro, P. Arato, Development of CNT/Si₃N₄ composites with improved mechanical and electrical properties, Compos. Part B 37 (2006) 418–424.
- [22] E. Fitzer, W. Schaefer, S. Yamada, The formation of glasslike carbon by pyrolysis of polyfurfuryl alcohol and phenolic resin, Carbon 7 (1969) 643–646.
- [23] Z.P. Zhu, Y. Lu, D.H. Qiao, S. Bai, T.P. Hu, L. Li, J.F. Zheng, Self-catalytic behavior of carbon nanotubes, J. Am. Chem. Soc. 127 (2005) 15698–15699.
- [24] G.X. Du, S.A. Feng, J.H. Zhao, C. Song, S. Bai, Z.P. Zhu, Particle-wire-tube mechanism for carbon nanotube evolution, J. Am. Chem. Soc. 128 (2006) 15405–15414.
- [25] U.S. Choi, B.G. Ahn, O.K. Kwon, Y.J. Chun, Tribological behavior of some antiwear additives in vegetable oils, Tribol. Int. 30 (1997) 677–683
- [26] Y. Matsumura, M. Okumura, Y. Usami, K. Kagawa, H. Yamashita, M. Anpo, M. Haruta, Low-temperature decomposition of methanol to carbon monoxide and hydrogen with low activation energy over Pd/ZrO₂ catalyst, Catal. Lett. 44 (1997) 189–191.
- [27] M. Kumar, Carbon nanotube synthesis and growth mechanism, Nanotechnol, Nanomater, (2011).
- [28] L.J. Ci, B.Q. Wei, C.L. Xu, L. Ji, D.H. Wu, S.S. Xie, W.Y. Zhou, Y.B. Li, Z.Q. Liu, D.S. Tan, Crystallization behavior of the amorphous carbon nanotubes prepared by the CVD method, J. Cryst. Growth 233 (2001) 823–828.
- [29] J. Abrahamson, The surface energies of graphite, Carbon 11 (1973) 337–362.
- [30] H. Hu, C.J. Peng, S.B. Krupanidhi, Effect of heating rate on the crystallization behavior of amorphous PZT thin films, Thin Solid Films 223 (1993) 327–333.
- [31] R. Andrews, D. Jacques, D. Qian, E.C. Dickey, Purification and structural annealing of multi-walled carbon nanotubes at graphitization temperatures, Carbon 39 (2001) 1681–1687.

- [32] E. Minoux, O. Groening, K.B.K. Teo, S.H. Dalal, L. Gangloff, J.P. Schnell, L. Hudanski, I.Y.Y. Bu, P. Vincent, P. Legagneux, G.A. J. Amaratunga, W.I. Milne, Achieving high-current carbon nanotube emitters, Nano Lett. 11 (2005) 2135–2138.
- [33] Z.Q. Guo, G. Blugan, T. Graule, M. Reece, J. Kuebler, The effect of different sintering additives on the electrical and oxidation properties of Si₃N₄-MoSi₂ composites, J. Eur. Ceram. Soc. 27 (2007) 2153–2161.
- [34] J.J. Hauser, Electrical, structural and optical properties of amorphous carbon, J. Non-Cryst, Solids 23 (1977) 21–41.
- [35] K.L. Kaiser, Electromagnetic Shielding, CRC Press, Boca Raton, United States 1–52.
- [36] P.S. Neelakanta, Handbook of Electromagnetic Materials: Monolithic and Composite Versions and their Applications, CRC Press, Boca Raton, 1995.
- [37] C.R. Paul, in: Introduction to Electromagnetic Compatibility, second edition, Wiley, Hoboken, NJ, 2006.
- [38] D.D.L. Chung, Materials for electromagnetic interference shielding, J. Mater. Eng. Perform. 9 (2000) 350–354.

- [39] M.H. Al-Saleh, U. Sundararaj, Electromagnetic interference shielding mechanisms of CNT/polymer composites, Carbon 47 (2009) 1738–1746.
- [40] W.S. Jou, H.Z. Cheng, C.F. Hsu, The electromagnetic shielding effectiveness of carbon nanotubes polymer composites, J. Alloys Compd. 434–435 (2007) 641–645.
- [41] M.H. Al-Saleh, U. Sundararaj, X-band EMI shielding mechanisms and shielding effectiveness of high structure carbon black/polypropylene composites, J. Phys. D: Appl. Phys. 46 (2013) 035304.
- [42] M. Arjmand, T. Apperley, M. Okoniewski, U. Sundararaj, Comparative study of electromagnetic interference shielding properties of injection molded versus compression molded multi-walled carbon nanotube/polystyrene composites, Carbon 50 (2012) 5126–5134.
- [43] X.W. Yin, Y.Y. Xue, L.T. Zhang, L.F. Cheng, Dielectric, electromagnetic absorption and interference shielding properties of porous yttria-stabilized zirconia/silicon carbide composites, Ceram. Int. 38 (2012) 2421–2427.