

# Preparation of nano-structured Ni–Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> anode materials for solid oxide fuel cells via the water-in-oil (W/O) micro-emulsion route

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## Abstract

Highly dispersed nano-crystalline NiO–Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> (GDC) anode powders were synthesized through a novel water-in-oil (W/O) micro-emulsion route, that has not been previously reported. The spherical-shaped NiO–Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> nano-powders exhibited a high degree of dispersion, and the morphology of the NiO–Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> particles was controlled by varying the aqueous to oil phase ratio. The polarization resistance at 800 °C with humidified H<sub>2</sub> fuel and the activation energy of ME10 anode synthesized by the micro-emulsion method with the aqueous to oil phase volume ratios of 1:12 were 0.02 Ω cm<sup>2</sup> and 0.55 eV, respectively, which were significantly lower than those of other Ni-ceria-based anodes. These properties contributed to a smaller particle size and better dispersion compared to conventional anode materials, leading to an increased number of reaction sites. In accordance with the polarization resistance results, single cells containing ME10 anodes exhibited a high maximum power density of 0.36 W cm<sup>−2</sup> at 800 °C with humidified H<sub>2</sub> fuel.

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## 1. Introduction

Solid oxide fuel cells (SOFCs) are highly efficient energy conversion devices that directly convert chemical energy to electricity with varying theoretical efficiencies. A typical SOFC consists of a dense electrolyte sandwiched between two porous electrodes (an anode and a cathode) [1,2]. Currently, nickel–yttria stabilized zirconia (Ni–YSZ) cermet anodes are state-of-the-art materials for SOFC [3–7]. In general, nickel can be used in a SOFC anode due to its high electro-catalyst activity for the electrochemical oxidation of hydrogen. Nickel also has a relatively high electrical conductivity, which is necessary for optimal SOFC performances.

In addition, YSZ acts as an ionic conductor, and transfers oxygen ions to the reaction site to complete the catalytic cycle.

Recently, intermediate temperature SOFCs (IT-SOFCs), which operate in the range of 500–800 °C, have garnered attention because lower temperatures minimize problems associated with thermal expansion mismatch and chemical reactivity among components. It is well known that Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> (Gd doped ceria, GDC) has a higher ionic conductivity than YSZ at low temperatures [8,9]. In addition, GDC displays catalytic activity due to its mixed ionic-electronic conduction behavior in reducing atmospheres. Therefore, Ni–GDC cermets have been extensively investigated as anode materials for IT-SOFCs.

The performance of SOFCs depends strongly on both the microstructure of its electrodes and the intrinsic properties of its materials due to the limited electrochemical reaction that takes place at the electrolyte, gas, and anode triple-phase boundary (TPB). To improve the overall performance of SOFCs, the TPB length can be extended by tailoring the

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anode morphology. Nano-structured anode powders offer a high specific surface area, which increases the number of reaction sites. Various synthetic routes can be implemented to obtain nano-crystalline anode powders, including co-precipitation, sol–gel, combustion, hydrothermal, mechano-chemical, and emulsion methods [8–17]. Among these methods, micro-emulsion techniques are unique due to the variety of micellar structures that can be obtained, ranging from simple droplets to complex cubic compositions. The thermodynamic stability of micro-emulsions can be used to improve the formulation stability and to synthesize various compounds consisting of highly dispersed nano-participles with tailored morphologies. Moreover, low-energy mixing equipment may be used to prepare micro-emulsions [18–21]. Despite numerous investigations on the synthesis of single-component compounds such as NiO and YSZ micro-emulsions, the preparation of NiO–GDC powders with micro-emulsion method are scarce in the literature, and systematic investigations of factors that control their electro-catalytic activity towards anode reactions are rare. Thus, we present herein the synthesis of nano-structured NiO–GDC powders, the morphology of which can be tailored by controlling the water-in-oil (W/O) micro-emulsion process. We characterized the electrochemical performance of the obtained nano-structured NiO–GDC powders, and correlated their morphology with the electrochemical performance.

## 2. Experimental procedures

Nano-crystalline NiO–GDC cermet anode powders were synthesized by a simple water-in-oil (W/O) micro-emulsion route using  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Alfa Aesar, 98%),  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  (Aldrich, 99% metal basis),  $\text{Gd}(\text{NO}_3)_3 \cdot x\text{H}_2\text{O}$  ( $x \sim 6$ , Alfa Aesar, 99.9%, REO), cyclohexane ( $\text{C}_6\text{H}_{12}$ , Alfa Aesar, 99+%), Triton<sup>®</sup>X-100 ( $\text{C}_{14}\text{H}_{22}\text{O}(\text{C}_2\text{H}_4\text{O})_n$ , Alfa Aesar), pentanol ( $\text{C}_5\text{H}_{12}\text{O}$ , Alfa Aesar, 98+%), NaOH (Samchun chemicals, 98.0%), and acetone (Samchun chemicals, 99.5%). De-ionized water was used for the aqueous phase. A detailed description of the synthetic procedure for the micro-emulsion is provided in Fig. 1. Three types of NiO–GDC micro-emulsions were prepared by changing the volume ratio of the aqueous (W) to oil (O) phases (W:O = 1:12, 2:12, and 3:12) and were designated ME10, ME20 and ME30, respectively.

The nano-crystalline NiO–GDC anode powders were characterized by X-ray diffraction (XRD) using  $\text{Cu-K}\alpha$  radiation. The morphology of the powders was evaluated by transmission electron microscopy (TEM, JEM-2010, JEOL, Japan). The BET surface area of the powders was measured with a surface area and pore size analyzer (Autosorb-1, Quantachrom instruments, USA). Microstructural characterization of the sintered samples was carried out using a scanning electron microscope (SEM, SN-3000 Hitachi, Japan). To verify the micro-emulsion process, thermogravimetric analysis (TGA, TA Q600, TA instruments, USA) and Fourier transform infrared spectroscopy (FT-IR, Spectrum GX, Perkin Elmer, USA) were employed. TGA was performed in air at temperatures ranging from 30 to 800 °C and a heating rate of 10 °C min<sup>−1</sup>.

Electrochemical performance was evaluated with electrolyte-supported single cells. Commercial GDC powder (CGO90/10 UHSA, Fuel Cell Materials, USA) was compressed via cold isostatic pressing (CIP) and was subsequently fired at 1450 °C for 4 h to fabricate a 0.5-mm thick GDC electrolyte pellet. The  $\text{Ba}_{0.5}\text{Sr}_{0.5}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_{3-\delta}\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  (50 wt%:50 wt%) cathode powder was synthesized by a previously described combustion method [22]. The anode and cathode pastes were produced by mixing the powder and binder (Heraeus V006) at a ratio of 70:30 wt% and the pastes were screen-printed on both sides of the GDC pellet to fabricate electrodes with a geometrical area of 0.49 cm<sup>2</sup>. The anode and cathode layers were fired at 1250 °C and 1050 °C for 2 h, respectively. Prior to the electrochemical test, NiO in the anode was reduced to Ni in humidified H<sub>2</sub>. *I*–*V* measurements of single cells were performed at 800 °C. A Pt mesh pushed onto the electrode with a spring-loaded alumina tube was used as the current corrector, a PYREX<sup>®</sup> glass ring was used as a seal between the single cell and the alumina tube. Humidified H<sub>2</sub> (~3% H<sub>2</sub>O at 30 °C) and air were supplied as the fuel and oxidant, respectively, at a rate of 100 cm<sup>3</sup> min<sup>−1</sup>. AC impedance analysis was also carried out using a universal potentiostat with a frequency response analyzer (Bio-logic science instrument) in a three-electrode configuration under humidified H<sub>2</sub> at 700 °C, 750 °C, and 800 °C. Pt paste was used as a reference electrode with a geometrical area of 0.21 cm<sup>2</sup> on the anode side. The applied frequency ranged between 1 mHz and 1 MHz at a voltage amplitude of 10 mV.

## 3. Results and discussion

W/O micro-emulsions are thermodynamically stable and possess an optically isotropic dispersion of water nano-droplets in the oil phase. Aqueous droplets formed in such micro-emulsions can be implemented as nano-reactors for the formation of nano-crystalline particles with tailored morphologies. To obtain a stable micro-emulsion of the cyclohexane ( $\text{C}_6\text{H}_{12}$ )–Triton<sup>®</sup>X-100+pentanol–H<sub>2</sub>O system, we investigated a pseudo-ternary phase diagram, in which Triton<sup>®</sup>X-100 was used as a non-ionic surfactant due to its amphiphilic properties. The phase diagram of the three component system, which consisted of H<sub>2</sub>O, Triton<sup>®</sup>X-100+pentanol, and cyclohexane ( $\text{C}_6\text{H}_{12}$ ), is shown in Fig. 2. The ratio of  $\text{C}_6\text{H}_{12}$ , Triton<sup>®</sup>X-100, and pentanol was set to 100:12:11, which resulted in a stable transparent oil phase. Subsequently, a nitrate salt solution (aqueous phase) was gradually added to the oil mixture. McEvoy reported a similar stable region for the formation of micro-emulsions. [23]. In the present study, we were able to prepare stable W/O micro-emulsions between ME10 and ME30 without any evidence of phase separation.

Maintaining the weight fraction of the precursor is essential for maintaining the stability of micro-emulsions prior to treatment with NaOH, which was used as a precipitating reagent for crystal growth. Thus, FT-IR analysis of ME10 samples was carried out step-by-step to understand the mechanism of micro-emulsion formation (Fig. 3). Although peaks associated with functional groups were clearly visible due to the presence of organics oil phases, the peaks in the finger print region (500–1500 cm<sup>−1</sup>)

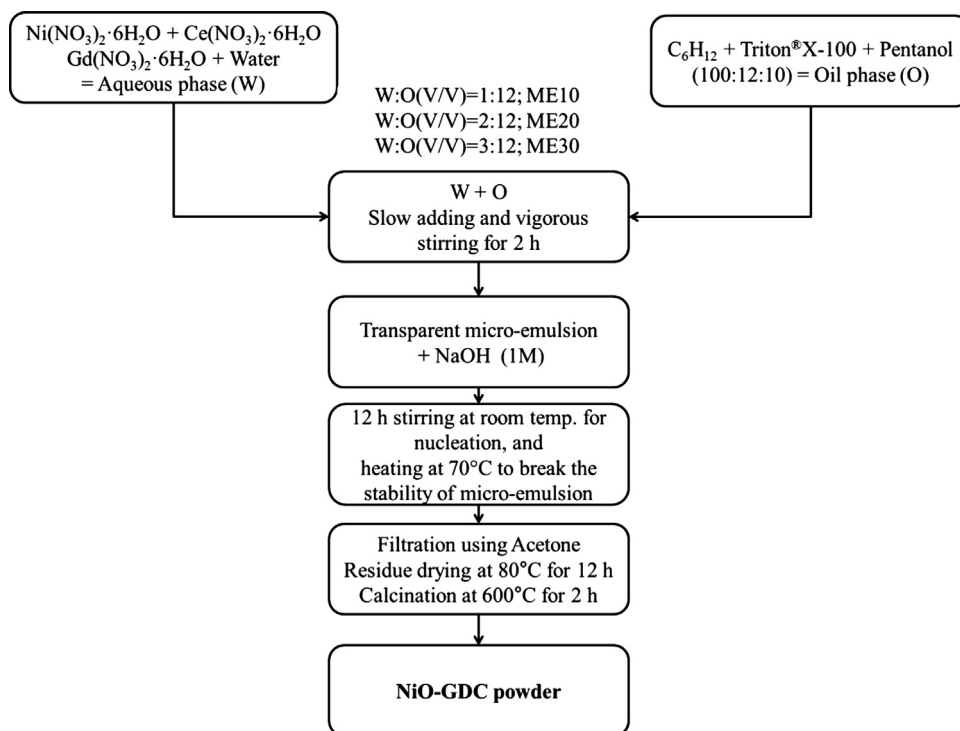


Fig. 1. Flow chart for the synthesis of nano-crystalline NiO–GDC powders using a (W/O) micro-emulsion method.

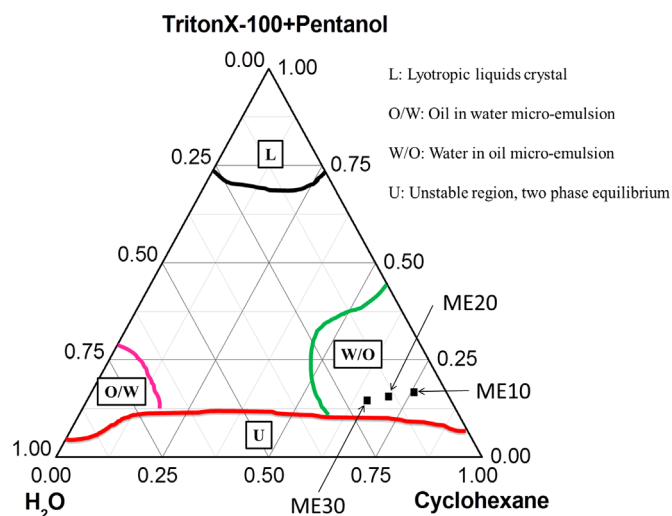


Fig. 2. Phase diagram of the three component system, which consisted of H<sub>2</sub>O, Triton®X-100+pentanol, and cyclohexane (C<sub>6</sub>H<sub>12</sub>).

were very complex. Specifically, in the oil phase, the three organic solvents (cyclohexane, pentanol, and Triton®X-100) were physically mixed without any chemical reaction in the normal state; however, the surface tension, viscosity, and solubility of the mixture may have changed due to the characteristics of the surfactant and co-surfactants. The doublet at 2850 and 2927 cm<sup>−1</sup> was attributed to the asymmetrical and symmetrical stretching mode of CH<sub>2</sub>, whereas the intense peak at 1450 cm<sup>−1</sup> in the finger print region was associated with C–H scissoring [24]. Several other notable peaks of low intensity were

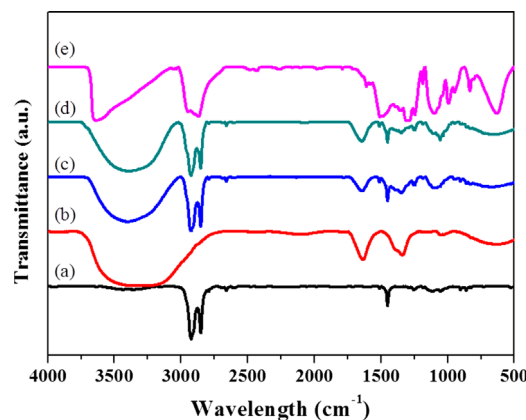


Fig. 3. FT-IR spectra of the (a) oil phase, (b) aqueous phase, (c) micro-emulsion prior to precipitation, (d) micro-emulsion after precipitation, and (e) final residue in dry form for the ME10 sample.

also observed, including peaks at 1050 cm<sup>−1</sup>, 1188 cm<sup>−1</sup>, 1128 cm<sup>−1</sup>, 1456 cm<sup>−1</sup>, 1512 cm<sup>−1</sup>, 1610 cm<sup>−1</sup>, 2660 cm<sup>−1</sup>, and 279 cm<sup>−1</sup>, which corresponded to primary alcohol O–H stretches, C–C stretches and C–H rocking, CH<sub>2</sub> twists, CH<sub>2</sub> wags, C–H scissoring, C–C stretches, 1st overtone of CH deformation, and C–O stretches of CHO groups, respectively [24–28]. In the aqueous solution, we observed broad peaks at 635 cm<sup>−1</sup> and 3320 cm<sup>−1</sup>, which corresponded to M–O and M–OH bonding vibrations and the typical H–OH stretch of H<sub>2</sub>O, respectively. The intense peaks at 1390 cm<sup>−1</sup> and 1634 cm<sup>−1</sup> corresponded to the ν<sub>as</sub>NO<sub>3</sub> stretch of salts precursors and the in-plane deformation of δH<sub>2</sub>O, respectively [29,30]. Because the micro-emulsion was formed by physical mixing of the aqueous and oil phases and was

mediated by surfactants, forming a thermodynamically stable and transparent solution, solvents should not have reacted with each other nor changed their chemical structure during the formation of the micro-emulsion. Thus, cyclohexane, pentanol, and Triton<sup>®</sup>X-100 coexisted in the oil phase during the formation of the micro-emulsion, and served to confine the aqueous phases to generate an aqueous core. Furthermore, while the surfactant (Triton<sup>®</sup>X-100) separated the aqueous phase from the oil phase to become a semipermeable membrane, the co-surfactant (cyclohexane) enhanced the solubility limit of the aqueous phase. Therefore, if the prepared micro-emulsion was stable, one can expect the resulting FT-IR spectra to match the peaks corresponding to either an oil mixture phase or aqueous phase. As shown in Fig. 3 (c), all of the peaks in the FT-IR spectra of ME10 matched those of the oil and aqueous phases in Fig. 3(a) and (b), respectively. However, the peak corresponding to the in-plane deformation of  $\delta\text{H}_2\text{O}$  at  $1643\text{ cm}^{-1}$  exhibited a red-shift after micro-emulsion formation due to the surface absorption of the surfactant terminal [26]. Conversely, the peak at  $1350\text{ cm}^{-1}$  corresponding to the  $\nu\text{ANO}_3^-$  stretch exhibited a blue-shift, which was attributed to coagulation of the aqueous core containing  $\text{NO}_3^-$  species along with precursor metal ions [31]. Although significant differences were not detected in the spectra of NiO–GDC micro-emulsions before and after precipitation, we did observe several changes with respect to the peak intensity and generation of new peaks. Specifically, we observed a new shoulder peak at  $2957\text{ cm}^{-1}$  corresponding to the  $\text{sp}^3$  C–H stretches near the doublet of  $\text{CH}_2$  asymmetric and symmetric stretches [25]. The appearance of this spectral line was due to the transformation of the carbon atom from  $\text{sp}^2$  to  $\text{sp}^3$  hybridization. Meanwhile, the peaks at  $1050\text{ cm}^{-1}$  and  $1258\text{ cm}^{-1}$  corresponding to the primary alcohol O–H stretches and C–O bending became more intense and distinct, which may be due to an increase in the pH and subsequent phase separation in the micro-emulsion. Fig. 3(e) shows the FT-IR spectra of a dry residue composed of an amorphous NiO, GDC, and hydroxide phase of the metal containing organic residues. A sharp peak at  $3654\text{ cm}^{-1}$  was observed and was attributed to non-hydrogen bonded O–H groups corresponding to  $\beta\text{-Ni}(\text{OH})_2$  [31,32]. All of the peaks between  $1500\text{ cm}^{-1}$  and  $3000\text{ cm}^{-1}$  corresponded to the vibrational modes of the functional groups of organic residues [33]. In addition, the intense peaks at  $480\text{ cm}^{-1}$  and  $627\text{ cm}^{-1}$  corresponded to the Ni–O stretch and the phonon band of  $\delta\text{Ce–O–C}$  or  $\delta\text{Ni–O–H}$  vibrations, respectively [31–35].

TGA plots of micro-emulsion mediated NiO–GDC precipitates pre-calcined at  $300^\circ\text{C}$  for 6 h are shown in Fig. 4. The pre-calcination process was carried out prior to TGA because composition effects due to weight losses greater than 85% are difficult to detect for organic components without the application of a pre-calcination process. Two major forms of weight loss were distinctly visible in the TGA plots. The first weight loss occurred between room temperature and approximately  $300^\circ\text{C}$  and was due to the loss of water and organic components that remained after pre-calcination. The weight losses for ME10, ME20 and ME30 were 1.95%, 2.02%, and 2.39%, respectively. According to TGA, the amount of the first weight loss was proportional to the aqueous phase of the

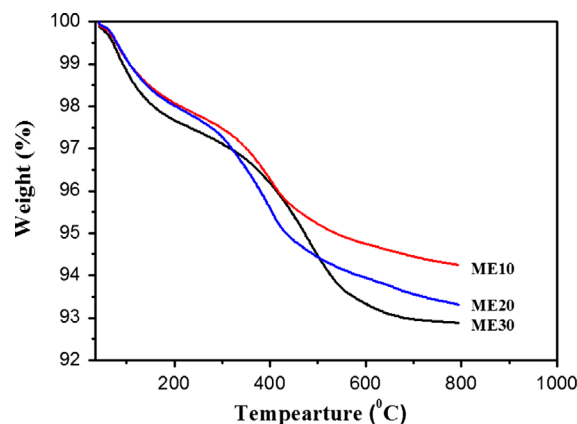


Fig. 4. TGA data for NiO–GDC precipitates pre-calcined at  $300^\circ\text{C}$  for 6 h.

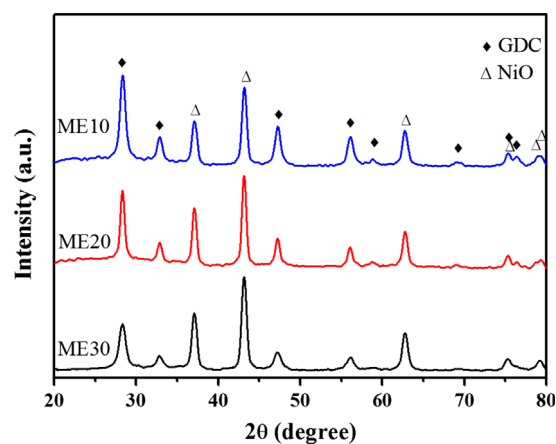


Fig. 5. XRD patterns of NiO–GDC powders calcined at  $600^\circ\text{C}$  for 2 h.

micro-emulsion. However, the second weight loss for ME10, ME20 and ME30 occurred between  $300^\circ\text{C}$  and  $600^\circ\text{C}$  and was 3.33%, 4.21%, and 4.50%, respectively. The second weight loss series corresponded to the decomposition of  $\text{Ni}(\text{OH})_2$  to NiO,  $\text{Ce}(\text{OH})_4$  to  $\text{CeO}_2$ , and  $\text{Gd}(\text{OH})_3$  to  $\text{Gd}_2\text{O}_3$ . Therefore, a high aqueous to oil phase ratio in the micro-emulsions, which corresponded to an increased abundance of Ni, Ce, and Gd micelles, resulted in increased weight loss. The TGA data also revealed that a calcination temperature of greater than  $600^\circ\text{C}$  should be used to obtain pure NiO–GDC powders.

The XRD patterns of NiO–GDC powders calcined at  $600^\circ\text{C}$  for 2 h are shown in Fig. 5. All of the NiO–GDC powders exhibited a single phase without any secondary phases or impurity phases, and all of the peaks matched that of cubic NiO (Fm3m, JCPDF #47–1049) and cubic  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  (Fm3m, JCPDF #34–0394). According to the Scherrer's formula, the calculated mean crystallite sizes of NiO for ME10, ME20, and ME30 NiO–GDC powders were 13.2 nm, 14.8 nm, and 13.4 nm, while those of GDC were 11.7 nm, 13.7 nm, and 10.6 nm, respectively. It has been reported that crystallite sizes of NiO and GDC in NiO–GDC synthesized by direct thermal treatment of a polymeric sol–gel at  $800^\circ\text{C}$  for 2 h was 24 nm and 18 nm, respectively [36].



Ding et al. reported that NiO and GDC have 30.5 nm and 27.3 nm of crystallite size in the NiO–GDC composite powders synthesized by a hydroxide co-precipitation method [37]. Similarly, Wandekar et al. also reported that NiO–GDC powders prepared by solution combustion synthesis consisted of 30–58 nm sized NiO and 40–50 nm sized GDC [38]. Interestingly, NiO–GDC powders synthesized by the micro-emulsion method showed smaller crystallite size than those prepared by other synthesis methods.

Although significant differences in the crystallite size were not observed, the overall morphology of the NiO–GDC powders was dependent on the aqueous to oil phase ratio, as shown in Fig. 6. The particle size of spherical NiO–GDC powders, which ranged from 12 to 20 nm, increased with an increase in the aqueous to oil phase ratio (ME10 < ME20 < ME30). Meanwhile, the ME10 powder with the lowest aqueous to oil phase ratio exhibited the highest degree of dispersion compared to the other powders, which may be due to the relatively low concentration of micelles. However, further reactions in the aqueous to oil phase ratio were difficult to achieve due to yield losses. Thus, a trade-off between the powder quality and yield may be necessary to identify the optimal composition of the micro-emulsion process.

Unlike the particle size, the surface area of NiO–GDC powders decreased with an increase in the aqueous to oil phase ratio. Specifically, the BET surface areas of ME10, ME20, and ME30 anode powders were  $16.8 \text{ m}^2 \text{ g}^{-1}$ ,  $12.9 \text{ m}^2 \text{ g}^{-1}$ , and  $8.4 \text{ m}^2 \text{ g}^{-1}$ , respectively. Considering that the catalytic reaction occurs on the anode surface, one may expect that the ME10 anode with the largest surface area should exhibit the best electrochemical performance.

The AC impedance spectra of Ni–GDC anodes in humidified  $\text{H}_2$  are shown in Fig. 7. An equivalent circuit consisting of an inductor (L), a resistor ( $R_o$ ), and two RQ elements ( $R_1Q_1$  and  $R_2Q_2$ ) were used to fit the impedance data, as described in Fig. 7

(a). The left intercept with the impedance semi-circle on the  $Z_{re}$  axis at high frequencies indicates the ohmic resistance,  $R_o$ , while the right intercept on the  $Z_{re}$  axis corresponds to the total resistance,  $R_{tot}$ . The polarization resistance,  $R_p$ , is the overall size of the arcs ( $R_{tot} - R_o$ ). The calculated  $R_p$  values at 700 °C, 750 °C, and 800 °C are listed in Table 1. The  $R_p$  value at a given temperature in  $\text{H}_2$  increased linearly as the aqueous to oil phase ratio increased. Considering the TPB length, one would expect that ME10 anodes with small particle sizes and high degrees of dispersion would exhibit the best electrochemical performance, as shown in Fig. 6. It has been reported that the polarization resistance of Ni–GDC anode synthesized by GNP method was  $0.06 \Omega \text{ cm}^2$  at 600 °C under humidified  $\text{H}_2$  with GDC electrolyte supported cell [39]. Recently, Choi et al. also reported that the polarization resistance value of the Ni–GDC anode supported cell at 650 °C is about  $0.40 \Omega \text{ cm}^2$  [40]. Although it is hard to compare the polarization resistance values of various Ni–GDC anodes directly due to a difference in the cell configuration, the electro-catalytic activity of the Ni–GDC anode synthesized by the micro-emulsion method could be comparable to that of other Ni–GDC anodes synthesized by various solution based methods.

The temperature dependencies of the ohmic ( $R_o$ ) and polarization ( $R_p$ ) resistances are shown in Fig. 8, and the calculated activation energies,  $E_a$ , are provided in Table 1. The activation energy of the Ni–GDC anode synthesized in the present study by the proposed micro-emulsion method was significantly lower than that of previously investigated Ni-ceria-based anodes. As previously reported, the activation energy of Ni–GDC anodes prepared by impregnation is 0.91 eV at temperatures of 700–1000 °C [41]. Similarly, Muecke et al. reported that nano-crystalline Ni–GDC thin film anodes have an activation energy of 1.45 eV at a temperatures of 400–600 °C [42], while Wang et al. reported an activation energy value of 1.01 eV for Ni– $\text{Sm}_{0.15}\text{Ce}_{0.85}\text{O}_{2-\delta}$  anodes at temperatures of 600–800 °C [43].

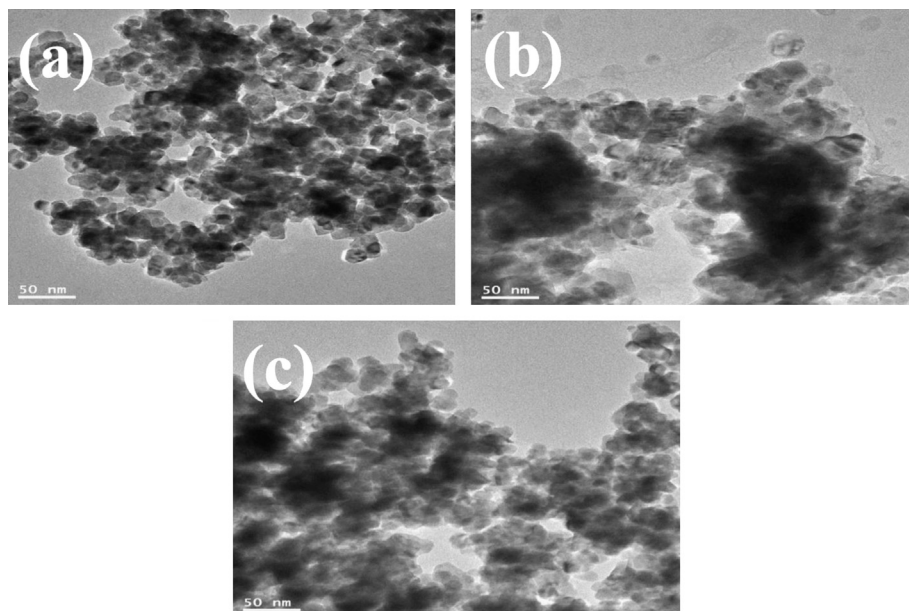


Fig. 6. TEM micrographs of NiO–GDC powders calcined at 600 °C for 2 h of (a) ME10, (b) ME20, and (c) ME30.

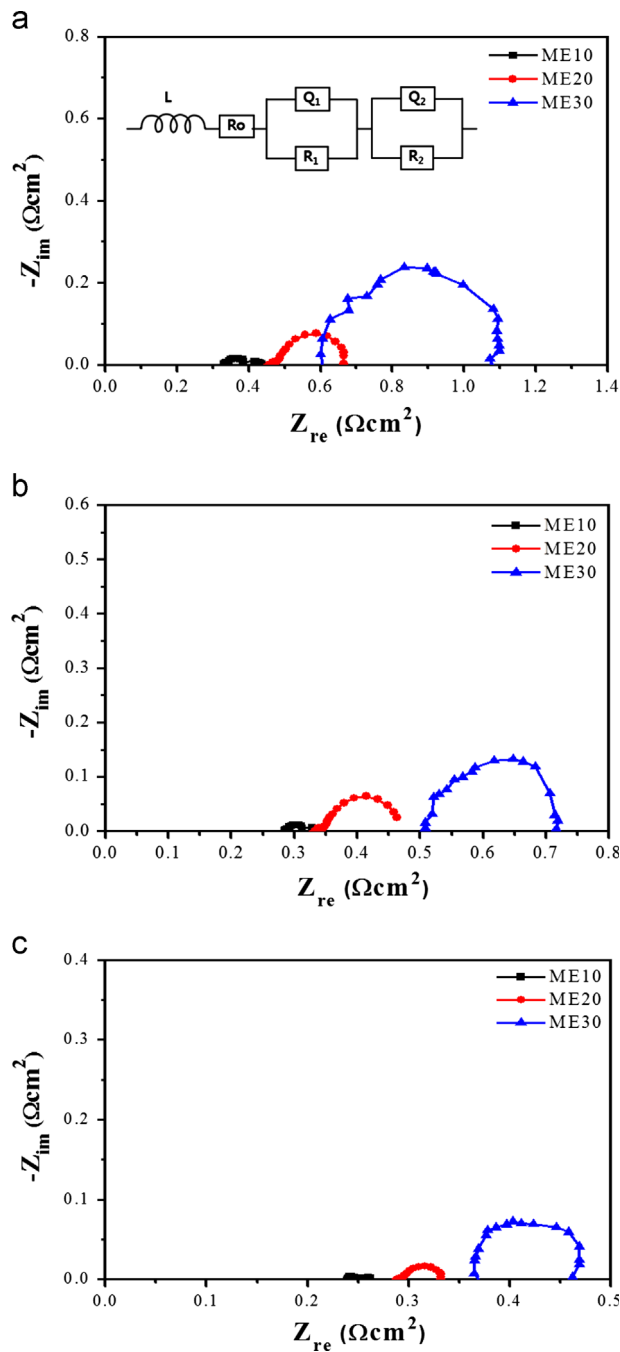


Fig. 7. Typical AC impedance spectra of Ni-GDC anodes at (a) 700 °C, (b) 750 °C, and (c) 800 °C in humidified H<sub>2</sub>.

Table 1

Polarization resistance and activation energy of Ni-GDC anodes at various operating temperatures in humidified H<sub>2</sub>.

Anode material	Polarization resistance (Ω cm <sup>2</sup> )			Activation energy (eV)
	700 °C	750 °C	800 °C	
ME10	0.095	0.047	0.021	0.55
ME20	0.217	0.137	0.054	0.58
ME30	0.464	0.216	0.110	0.61

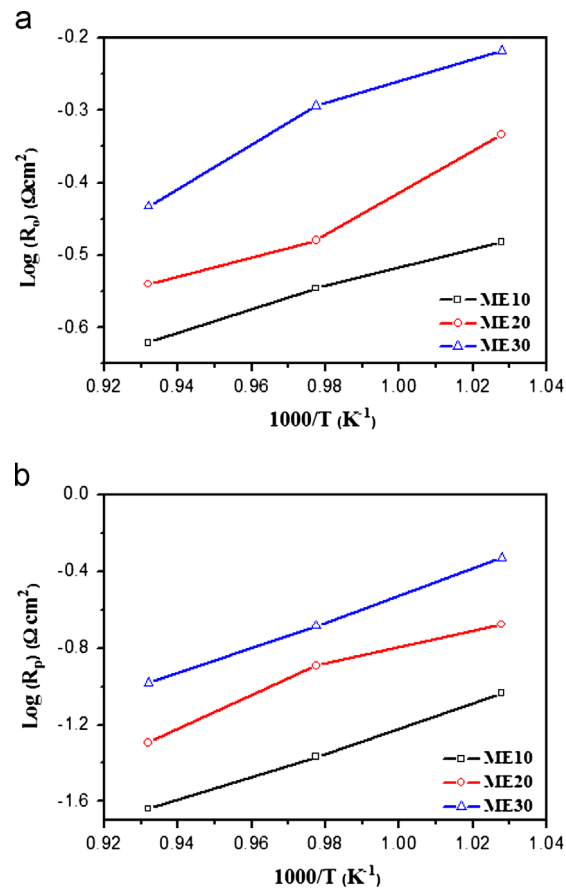


Fig. 8. Temperature dependence of the (a) ohmic ( $R_o$ ) and (b) polarization ( $R_p$ ) resistances of Ni-GDC anodes in humidified H<sub>2</sub>.

Meanwhile, the total polarization resistance ( $R_p$ ) was separated by  $R_1$  and  $R_2$  which correspond to the high-frequency semi-circle and the low-frequency semi-circle, respectively, to verify the individual electrode reaction processes. The separated polarization resistance values for the composite anodes in humidified H<sub>2</sub> atmosphere are listed in Table 2. The ME10 anode showed the lowest  $R_1$  and  $R_2$  values. Interestingly, the  $R_1$  value is lower than the  $R_2$  value for all the compositions. Nakagawa et al. reported that the semi-circle on the high-frequency side ( $R_1$ ) corresponded to the activation process and that the semi-circle at the low-frequency side ( $R_2$ ) corresponded to the diffusion process [44]. Therefore, the diffusion process could be the rate-determining step for the Ni-GDC anode synthesized by micro-emulsion method. Meanwhile, the  $R_1$  value of ME10 anode was significantly lower than those of ME20 and ME30 at 800 °C. Since the oxidation reaction of fuel at the anode side is strongly affected by the electrode microstructure, which restrains the reaction sites such as TPB, the ME10 anode with the smaller grain size and the better-distributed pore structure, as shown in Fig. 9, exhibits the lowest  $R_1$  value.

Fig. 9 compares the SEM micrographs of Ni-GDC anodes synthesized by the proposed micro-emulsion method after the electrochemical performance test. The grain size of the anodes

Table 2

The separated polarization resistance values for the composite anodes humidified H<sub>2</sub>.

Anode material	Temperature (°C)	Polarization resistance ( $\Omega \text{ cm}^2$ )	
		$R_1$	$R_2$
ME10	700	0.045	0.050
	750	0.007	0.040
	800	0.003	0.018
ME20	700	0.105	0.112
	750	0.051	0.086
	800	0.025	0.029
ME30	700	0.120	0.344
	750	0.081	0.135
	800	0.049	0.061

increased with an increase in the aqueous to oil phase ratio (ME10 < ME20 < ME30), suggesting that highly dispersed GDC particles may block the grain growth of Ni particles. Moreover, compared with ME20 and the ME30 anodes, the ME10 anode exhibited a porous structure with meso- and micro-pores, suggesting that the TPB area was enlarged throughout the porous anode structure compared to that of the other anodes. The observed differences in the microstructures of sintered anodes may have been induced by the initial morphology of the powders as evidenced in Fig. 6 and the BET analysis.

The cell voltages and power densities of Ni–GDC anodes synthesized by the proposed micro-emulsion method are shown in Fig. 10. The open circuit voltages at 800 °C were  $0.76 \pm 0.02$  V. The relatively low open circuit voltage could mainly be due to the reduction of GDC electrolytes in a reducing atmosphere rather than gas leakage. Zha et al. calculated theoretical electromotive force (EMF) of a SOFC based on fluorite structure electrolyte such as YSZ and GDC by defect chemistry analysis [45]. In case of GDC ( $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$ ), the calculated EMF value was 0.85 V at 800 °C with 3%H<sub>2</sub>O–H<sub>2</sub> gas at anode side and pure O<sub>2</sub> gas at cathode side [45]. The open circuit voltage of 0.76 V at 800 °C in this study could be reasonable value considering air atmosphere at the cathode side. It has been also reported that the open circuit voltage of single cell with GDC electrolyte was 0.77 V at 800 °C with a mixture of 1.5%H<sub>2</sub>O–H<sub>2</sub> and air as fuel and oxidant gases, respectively [46]. Meanwhile, the open circuit voltage depends on the thickness of a mixed conducting electrolyte such as doped ceria. Duncan et al. reported that the open circuit voltage of Ni–GDC/GDC/LSCF–GDC cell increased with an increase in the thickness of GDC electrolyte and then saturated around 100  $\mu\text{m}$  [47]. Therefore, a 500- $\mu\text{m}$  thick GDC electrolyte may not affect the open circuit voltage in this study. The maximum power density of a single cell containing the ME10 anode was  $0.36 \text{ W cm}^{-2}$ , which was higher than that of single cells containing ME20 and ME30 anodes. The observed changes in the power density in a humidified H<sub>2</sub> atmosphere due to changes in the aqueous to oil phase ratio were consistent with the general trends in the AC impedance data. Although Ni–GDC anodes synthesized by the proposed micro-emulsion method exhibited relatively improved electrochemical

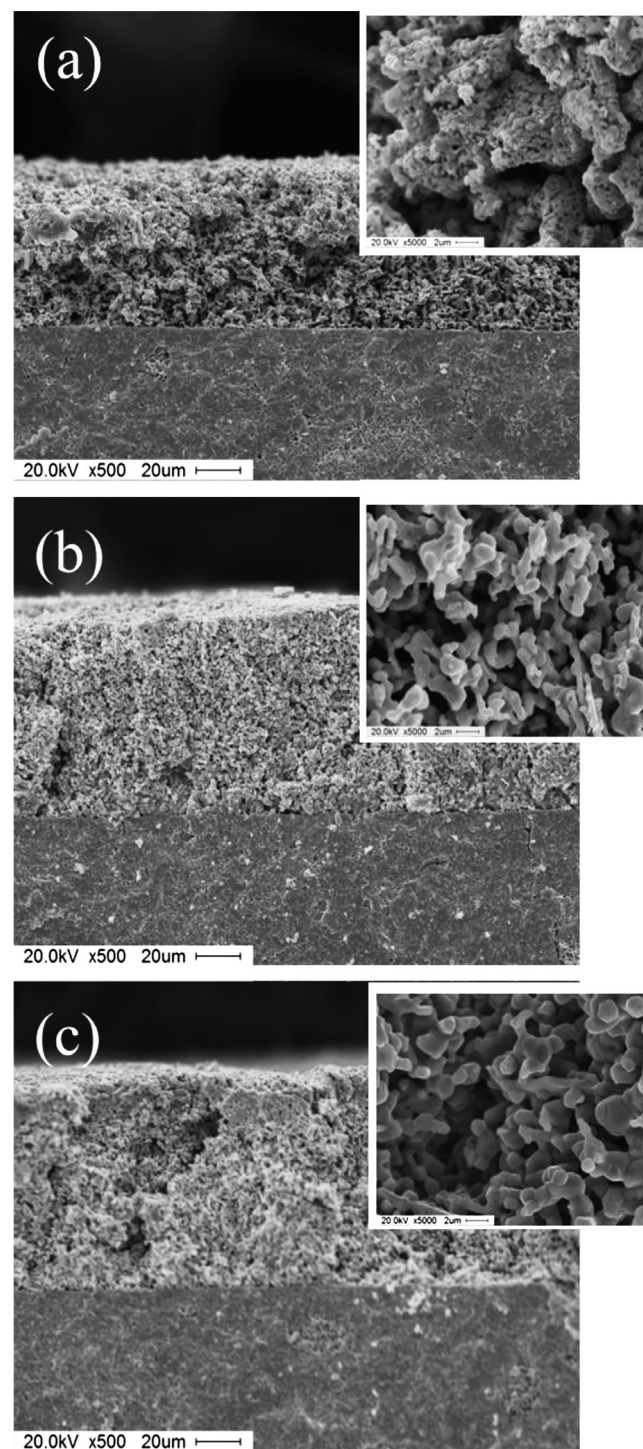


Fig. 9. SEM micrographs of NiO–GDC anodes of (a) ME10, (b) ME20, and (c) ME30 fired at 1250 °C for 2 h. The inset shows an enlarged micrograph of the anode region.

performance compared to that of other conventional anode materials, the overall electrochemical performance of the single cell was relatively poor, which was attributed to the use of a 500- $\mu\text{m}$  thick electrolyte. Further studies using an ultra-thin electrolyte may be beneficial, considering the ohmic resistance of the electrolyte. In addition, if the operation of the  $\text{Ba}_{0.5}\text{Sr}_{0.5}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_{3-\delta}\text{--Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  cathode is optimized, the electrochemical performance may be further improved.



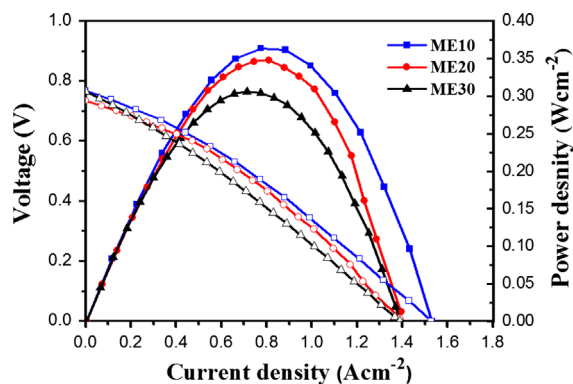


Fig. 10. Comparison of  $I$ - $V$  curves (open symbols) and power densities (closed symbols) of Ni-GDC anodes at 800 °C.

#### 4. Conclusions

NiO-GDC cermet powders without any impurities were successfully synthesized by a water-in-oil (W/O) micro-emulsion route. The nano-sized powders possessed a spherical shape with a high degree of dispersion. The morphology of the powders was controlled by varying the synthetic conditions, including the aqueous to oil phase ratio. However, during the optimization of the micro-emulsion process, a trade-off between the powder quality and yield was observed. The polarization resistance and activation energy of the Ni-GDC anodes synthesized in the present study by the proposed micro-emulsion method were significantly lower than those of conventional Ni-ceria-based anodes due to the enlarged TPB area. The single cell containing an ME10 anode exhibited a maximum power density of  $0.36 \text{ W cm}^{-2}$ . Thus, the water-in-oil (W/O) micro-emulsion method, which can be used to control the nano-structure and powder morphology, may be useful for the preparation of SOFC electrode materials.

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