

# Eutectic reaction between copper oxide and titanium dioxide

Fu-Hsing Lu \*, Fu-Xuan Fang, Yan-Shiaw Chen

*Department of Materials Engineering, National Chung Hsing University, 250 Kuo Kuang Road, Taichung 402, Taiwan, ROC*

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## Abstract

Eutectic reaction between copper oxide (CuO) and titanium dioxide (TiO<sub>2</sub>) was investigated by using directly Cu and TiO<sub>2</sub> samples and by employing optical microscopy, X-ray diffraction (XRD), scanning electron microscopy, and electron probe for microanalysis (EPMA). Different types of samples including Cu plate/TiO<sub>2</sub> pellet samples and TiO<sub>2</sub>/Cu/TiO<sub>2</sub> sandwiched samples were prepared. The samples would react with each other at as considerably low as about 900°C in air, which is due to a eutectic reaction. The reaction diagram was generated, in which different reaction categories were denoted at various temperatures (300–1070°C) and times. After annealing, the weight changes normalized to the original Cu samples were also analyzed to verify the eutectic reaction. The eutectic was identified to be the CuO–TiO<sub>2</sub> system characterized from XRD and EPMA analyses. Annealing in N<sub>2</sub>/O<sub>2</sub>=9 at the same temperature as in air resulted in similar but not so drastic eutectic melting phenomena. The eutectic reaction would enhance significantly the grain growth of TiO<sub>2</sub> and the oxidation of Cu. The changes in the microstructures and the morphologies of the samples were also investigated. The eutectic temperatures of CuO and other oxide systems were compared and discussed. The eutectic points as well as the phase diagram of the CuO–TiO<sub>2</sub> system were calculated and analyzed. Several potential applications of the reactions were also proposed. © 2001 Elsevier Science Ltd. All rights reserved.

**Keywords:** Cu; CuO; Eutectic reaction; Microstructure-final; TiO<sub>2</sub>

## 1. Introduction

The metal–ceramic reactions at high temperature under controlled atmosphere are of technological importance. Cu is a widely used material in industry and an important material for future interconnects in ICs. Moreover TiO<sub>2</sub> is also a widely used material for its excellent optical, chemical, and many other properties. Hence the Cu–TiO<sub>2</sub> system was chosen for the study. Nevertheless very few studies concerning the reactions of Cu and TiO<sub>2</sub> at high temperature under controlled oxygen partial pressures have been systematically investigated before. This part of the research focuses on the reactions mainly in air and partly in N<sub>2</sub>/O<sub>2</sub>=9 where eutectic reactions would occur. It is worth noting that little information on the eutectic reactions between CuO and TiO<sub>2</sub> is available in the literature.

The objective of this research is to investigate the eutectic reaction of the CuO–TiO<sub>2</sub> system mostly in air.

The changes in the appearance, the weight, the crystal structure, and the microstructure after annealing have been analyzed to study the eutectic reaction. Another gas with different oxygen partial pressure such as N<sub>2</sub>/O<sub>2</sub>=9 has also been used for comparing the microstructural changes. For the ease of sample preparation and the increase of reaction areas, two types of samples: Cu plates were directly placed on the top of TiO<sub>2</sub> pellets and TiO<sub>2</sub>/Cu/TiO<sub>2</sub> sandwiched samples were prepared. The eutectic temperatures of copper oxides and other oxide systems available in the literature have been compared and discussed. The CuO–TiO<sub>2</sub> phase diagram including the eutectic points has been calculated assuming that the quasi-binary system exhibits complete miscibility in the liquid state and virtually complete immiscibility in the solid state. The applicability of the eutectic reactions has also been discussed.

## 2. Experiments

The eutectic reactions of CuO and TiO<sub>2</sub> were investigated mainly by using directly Cu and TiO<sub>2</sub> samples for

\* Corresponding author. Tel.: +886-4-2851455; fax: +886-4-2857017.

E-mail address: [fhl@dragon.nchu.edu.tw](mailto:fhl@dragon.nchu.edu.tw) (F.-H. Lu).

the ease of sample preparation. For comparison, CuO samples were also prepared from the oxidation of Cu plates in air at 1020°C for at least 3 h. Surface CuO phase was confirmed by X-ray diffraction. The copper (JIS H 3100 C1201R-1/4H, 99.9% + purity) plates were first mechanically ground and polished. Then the plates were electrolytically polished by using  $\text{H}_3\text{PO}_4\text{:H}_2\text{O}$  (7:3) as the electrolyte. To avoid pitting occurring on the substrates, the operation voltage was maintained at 2.0 V and the polishing time was about 5 min. After that the copper plates (10×10×0.5 mm) were embedded in the  $\text{TiO}_2$  powders (Showa Denko, 99.9%, ~0.3  $\mu\text{m}$ ) and then cold pressed into the disks with the size of about 17 mm in diameter and 5 mm in thickness. The main advantage of this type of simple sample preparation is to increase the reaction area between Cu and  $\text{TiO}_2$ . Another type of sample was also prepared, i.e. Cu plates with the same size were placed directly on the top of the  $\text{TiO}_2$  pellets (17 mm in diameter and 2 mm in thickness), which were prepared from pressing the  $\text{TiO}_2$  powders. The measured green density of the  $\text{TiO}_2$  pellets was about 60% of the theoretical density.

Annealing in air was performed in a muffle furnace. For comparison, three samples including a Cu/ $\text{TiO}_2$  sample, a single Cu plate, and a single  $\text{TiO}_2$  pellet were placed in the furnace during each annealing run. The ramping rates were about 6°C/min. The temperatures were monitored by an R-type thermocouple and were calibrated to the melting point of Au (99.99%), i.e. 1064°C. Annealing in  $\text{N}_2/\text{O}_2=9$  was done in a tube furnace equipped with an oxygen sensor (15%CaO-doped  $\text{ZrO}_2$ ). After annealing, the changes in the appearance of the samples were examined by using both a stereo microscope and an optical microscope. The weight changes were also recorded. The changes in the crystal structure were determined by the MacScience MXP3 X-ray diffractometer. The microstructure and the morphology were examined by the JEOL JSM-5400 scanning electron microscope (SEM) equipped with the LINK ISIS energy dispersive spectrometer (EDS). When necessary, a JEOL 8900R Electron Probe Micro-analyzer (EPMA) with 20 kV accelerating voltage was also used to identify the change in the composition.

### 3. Results and discussion

#### 3.1. Changes in the appearance and weight

The Cu plate/ $\text{TiO}_2$  pellet (a Cu plate was placed directly on the top of a  $\text{TiO}_2$  pellet) samples were annealed in air for 10 min and 1 h at temperatures varying from 300 to 1070°C. After the anneal samples were first examined by using a stereo microscope and an optical microscope. The reaction results concerning the appearance of the samples are given in Fig. 1. In the

figure, the notation “partly reaction” refers to that the Cu plates are oxidized and the resulted oxides react with the adjacent  $\text{TiO}_2$ , then the melts diffuse into part of the  $\text{TiO}_2$  pellets. Since the occurring diffusion is so fast (the calculated diffusion coefficient, by using  $x^2 \sim D \cdot t$ , would be larger than  $10^{-5} \text{ cm}^2/\text{s}$ ) that only liquid state diffusion would be possible. Furthermore the reaction temperatures are much lower than the melting points of Cu (1083°C<sup>1</sup>) and  $\text{TiO}_2$  (1825°C<sup>1</sup>) as well as the eutectic point of Cu– $\text{Cu}_2\text{O}$  (1066°C<sup>2</sup>) and  $\text{Cu}_2\text{O}$ –CuO (1091°C<sup>2</sup>). Hence the melts that turn black in appearance are most possibly the eutectic melts. The melting denoted in the figure then refers to a eutectic melting. The boundary temperature between no apparent reaction and apparent reactions (including partly reaction and melting) is about 900°C which may be considered as the eutectic temperature.

Fig. 2 shows the normalized weight changes of the Cu/ $\text{TiO}_2$  samples and the Cu plates alone after annealing at above various temperatures for 10 min. The weight changes are normalized to the original Cu sample for comparison. Since the weight changes of the Cu/ $\text{TiO}_2$

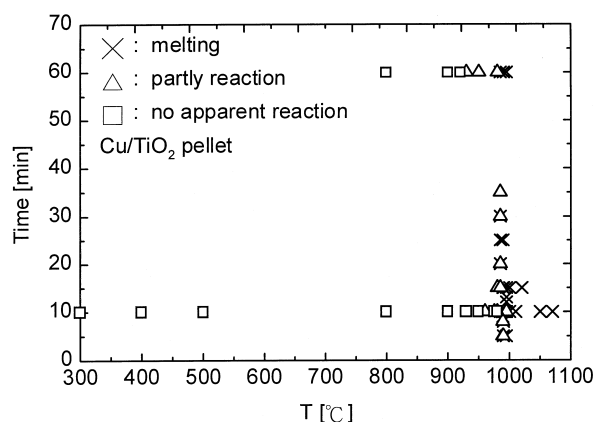


Fig. 1. The reaction diagram in which the resulted appearance of Cu/ $\text{TiO}_2$  samples after annealing at various temperatures and times was denoted.

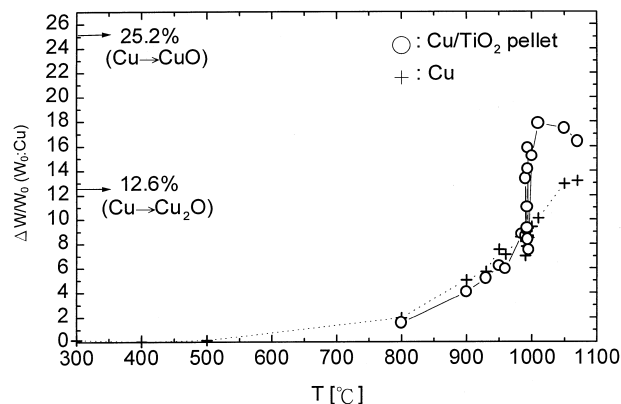


Fig. 2. The normalized (to original Cu samples) weight changes of Cu/ $\text{TiO}_2$  samples and Cu samples after annealing at various temperatures for 10 min.

samples are mainly due to both the oxidation of Cu and the  $\text{Cu}_x\text{O}$  ( $\text{Cu}_2\text{O}$  or  $\text{CuO}$ )– $\text{TiO}_2$  eutectic reaction (the weight changes of  $\text{TiO}_2$  after annealing are minimal), the difference in the normalized weight changes between the  $\text{Cu}/\text{TiO}_2$  sample and the single Cu plate at corresponding conditions would mainly attribute to the eutectic reaction. In the figure, it is shown that the major difference in the weight changes of the two samples occurs at  $990^\circ\text{C}$ . The temperature is near but lower than the boundary temperature as described earlier. Since the difference in the normalized weight change would not be so obvious when the eutectic melting starts to occur and is not so drastic, it is reasonable that the difference temperature concerning the normalized weight change would be lower than the boundary temperature concerning the resulted appearance. Nevertheless the major difference of the normalized weight changes is also another clear evidence of the eutectic reaction in the system. Very similar results concerning the resulted appearance and the normalized weight change at above temperatures were also obtained for the  $\text{TiO}_2/\text{Cu}/\text{TiO}_2$  sandwiched samples.

It is worth noting that the calculated weight change is 12.6% when pure Cu is completely oxidized into  $\text{Cu}_2\text{O}$  (25.2% for  $\text{CuO}$ ). As shown in the figure the weight change for pure Cu samples would be only slightly larger than 12.6% even the annealing temperature reaches  $1070^\circ\text{C}$ . But the normalized weight change of the Cu (in contact with  $\text{TiO}_2$ ) samples could reach about 18% (about 50% weight increase) at similar temperatures. That also indicates the only a small amount of  $\text{CuO}$  exists in the single Cu sample but a large amount of  $\text{CuO}$  is present in the  $\text{Cu}/\text{TiO}_2$  sample at corresponding conditions.

After annealing in air at  $1020^\circ\text{C}$  for 30 min, Cu plates alone could only be partially oxidized into both  $\text{Cu}_2\text{O}$  and  $\text{CuO}$  phases as revealed by XRD. It has been reported in the literature that it would take about 30 days at  $1000^\circ\text{C}$  in oxygen to completely oxidize Cu foils with the thickness about 0.1 mm into  $\text{CuO}$ .<sup>3</sup> It is reported that the oxidation of Cu to  $\text{Cu}_2\text{O}$  in air or oxygen occurs much faster compared to that of  $\text{Cu}_2\text{O}$  to  $\text{CuO}$ . Since mostly the  $\text{CuO}$  phase beside  $\text{TiO}_2$  is present in the annealed  $\text{Cu}/\text{TiO}_2$  samples, the eutectic reaction apparently enhances the oxidation of Cu. This may be due to the quick exposure of Cu plates to air after the repetitive consumption of the plates during the eutectic reaction.

### 3.2. Changes in the crystal structures and microstructures

Since the eutectic reaction could be possibly due to either  $\text{Cu}_2\text{O}$ – $\text{TiO}_2$  or  $\text{CuO}$ – $\text{TiO}_2$ , the samples were examined by X-ray diffraction. Both types of the samples (Cu placed on  $\text{TiO}_2$  pellets and  $\text{Cu}/\text{TiO}_2/\text{Cu}$  sandwiched samples) were checked. The diffraction results at the

$\text{TiO}_2$  sides show that only  $\text{CuO}$  and  $\text{TiO}_2$  (rutile) phases are present as revealed in Fig. 3. Moreover as described earlier, the color turns black which also indicates the presence of  $\text{CuO}$ . Hence the eutectic refers to the  $\text{CuO}$ – $\text{TiO}_2$  system.

The cross-sectional view (backscattered electron image, BEI/SEM) of the sample in which copper plates were embedded in the  $\text{TiO}_2$  powders, then cold pressed, and annealed in air at  $1020^\circ\text{C}$  for 30 min is shown in Fig. 4(a). As shown in the figure, a large void is present inside the sandwiched sample. This is because that the original Cu plate was oxidized, then the resulted oxide reacted with the adjacent  $\text{TiO}_2$ , and finally the eutectic melts diffused away from the original Cu plate region into the  $\text{TiO}_2$  region. Meanwhile, the original  $\text{TiO}_2$  region can be distinguished into two phases: dark and light phases as given in the figure. An enlarged back-scattered electron image of Fig. 4(a) at the original  $\text{Cu}/\text{TiO}_2$  interface is given in Fig. 4(b). Combining the information obtained from BEI and XRD as well as EPMA, it is known that large  $\text{TiO}_2$  grains (dark phase) are dispersed in the  $\text{CuO}$ – $\text{TiO}_2$  eutectic (light phase) matrix. To verify the eutectic structure, the above samples were further annealed in a very reducing  $\text{N}_2/\text{H}_2 = 9$  atmosphere at  $1000^\circ\text{C}$  for 2 h. After the reduction, the samples turned from black ( $\text{CuO}$  color) into red (Cu color). In the samples only Cu and  $\text{TiO}_2$  phases are present confirmed by XRD, which indicates a complete reduction of  $\text{CuO}$  into Cu. The crosssectional view (BEI) of the samples after the reduction is shown in Fig. 4(c). The dark phase is  $\text{TiO}_2$  and the eutectic structure could be then observed in the previous light region of Fig. 4(b). Similar melting phenomena and microstructure changes could also be observed in the reactions of the samples in which Cu plates with and without the prior oxidation were placed directly on the top of  $\text{TiO}_2$  pellets.

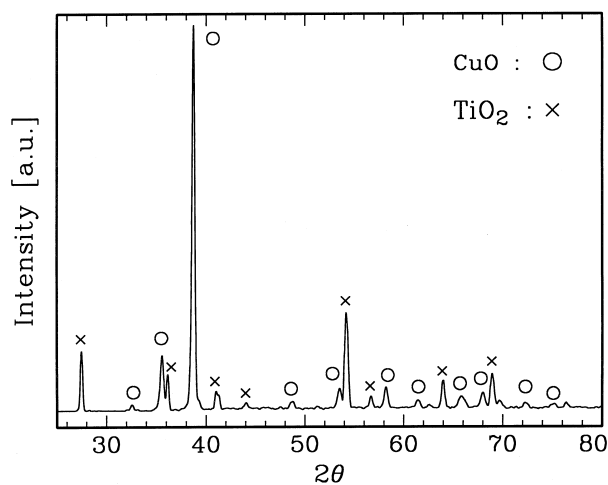
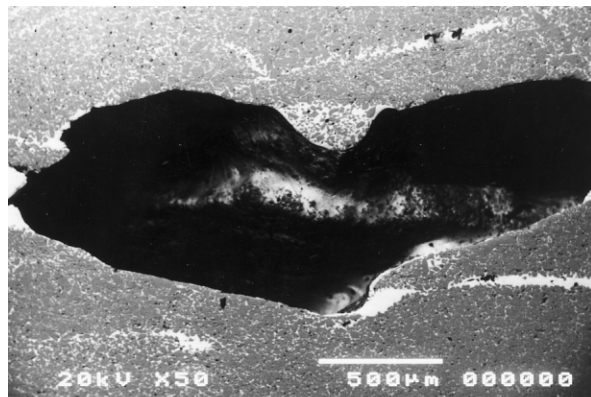
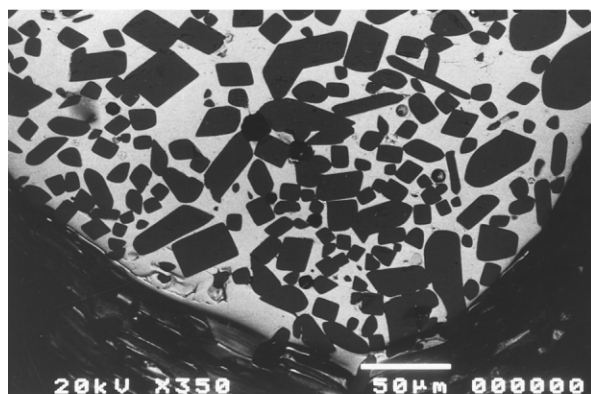


Fig. 3. XRD results of the  $\text{TiO}_2$  side in the  $\text{TiO}_2/\text{Cu}/\text{TiO}_2$  sandwiched samples after annealing at  $1020^\circ\text{C}$  for 30 min in air.

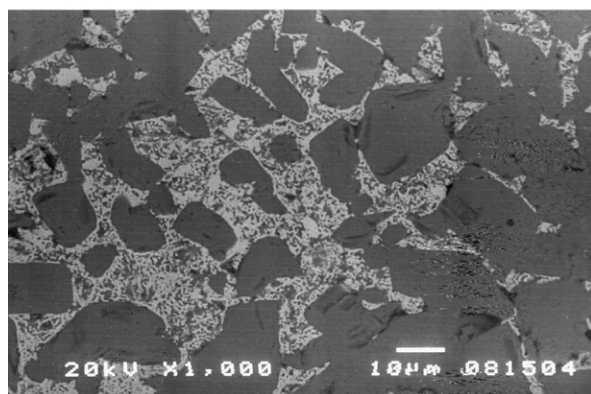
In the melted samples the grain size of the  $\text{TiO}_2$  ranges from a few microns to  $50\text{ }\mu\text{m}$ , which is much larger than that of  $\text{TiO}_2$  samples without being in contact with Cu at corresponding conditions. The averaged grain size of the  $\text{TiO}_2$  samples is about  $0.3\text{ }\mu\text{m}$  before sintering and



(a)



(b)



(c)

Fig. 4. Cross-sectional view (SEM/BEI) of the  $\text{TiO}_2/\text{Cu}/\text{TiO}_2$  sandwiched samples after annealing in air at  $1020^\circ\text{C}$  for 30 min. (a) A large void is present inside the sandwiched sample; (b) Enlarged image of (a) at the original  $\text{Cu}/\text{TiO}_2$  interface. The dark phase is the  $\text{TiO}_2$  and the light phase is the  $\text{CuO-TiO}_2$  eutectic; (c) The sample was further reduced in  $\text{N}_2/\text{H}_2=9$  at  $1000^\circ\text{C}$  for 2 h. The dark phase is  $\text{TiO}_2$  and the eutectic structure could be observed in the previous light region.

remains about the same size after annealing. Hence the eutectic reaction could aid drastically the grain growth of  $\text{TiO}_2$ . Moreover as seen in Fig. 4(b) almost no porosity could be observed in the  $\text{Cu}/\text{TiO}_2$  samples. This is quite interesting since there still exists about 10–20% porosity in the pure  $\text{TiO}_2$  samples alone after sintering at  $1000\text{--}1300^\circ\text{C}$ .

In addition to air, another gas mixture  $\text{N}_2/\text{O}_2=9$  was also used for comparison. The oxygen partial pressure in the gas mixture is 0.1 atm confirmed by the oxygen sensor. The oxygen partial pressure is slightly smaller than that in air ( $=0.21\text{ atm}$ ). After annealing at  $1020^\circ\text{C}$  in the gas mixture for more than 3 h, no drastic melting could be observed in the sandwiched  $\text{TiO}_2/\text{Cu}/\text{TiO}_2$  samples although the whole samples also turn black. Only  $\text{CuO}$  and rutile  $\text{TiO}_2$  phases could be identified at the  $\text{TiO}_2$  sides of the samples by XRD. The cross-sectional view of the samples in the SEM/BEI mode is given in Fig. 5. The light phase in the original  $\text{TiO}_2$  region is the  $\text{CuO-TiO}_2$  eutectic and the dark phase is  $\text{TiO}_2$  similar to that described earlier. As shown in the figure, the original embedded Cu plates do not disappear unlike those annealed in air although the annealing time is much longer. As shown in the figure, the eutectic melts diffuse apparently in liquid state through cracks, which might be resulted from thermal mismatch between  $\text{TiO}_2$  and the copper sample. This less drastic melting phenomenon could be possibly due to a higher eutectic temperature since the oxygen partial pressure is lower compared to that in air.

### 3.3. Calculation of the eutectic points

The phase diagram of the  $\text{Cu-Ti-O}$  system is rather scarce. Only a few phase diagrams are available concerning the existence of several intermediate phases, e.g. in Refs. 4,5. The intermediate phases in the  $\text{Cu-Ti-O}$  system contain  $\text{Cu}_3\text{TiO}_4$ ,<sup>4</sup>  $\text{Cu}_2\text{Ti}_4\text{O}$ ,  $\text{Cu}_3\text{Ti}_3\text{O}$ ,<sup>5</sup> etc. The

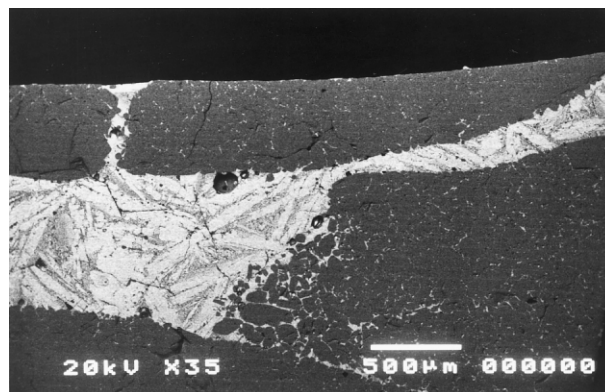


Fig. 5. Cross-sectional view (SEM/BEI mode) of the  $\text{TiO}_2/\text{Cu}/\text{TiO}_2$  sandwiched samples after annealing in  $\text{N}_2/\text{O}_2=9$  gas mixture at  $1020^\circ\text{C}$  for 3 h. No void is present and the trace of the diffusion of eutectic melts through cracks could be observed.

$\text{Cu}_3\text{TiO}_4$  phase, which is only stable in a narrow range of temperatures and oxygen partial pressures, can only be prepared from quenching the  $\text{CuO}$ ,  $\text{Cu}_2\text{O}$  and  $\text{TiO}_2$  samples.  $\text{Cu}_2\text{Ti}_4\text{O}$ ,  $\text{Cu}_3\text{Ti}_3\text{O}$  compounds observed as products of reactions at  $\text{Ag-Cu-Ti/Al}_2\text{O}_3$  interface also exhibit a narrow phase stability range.<sup>5</sup>

The eutectic points of the copper oxides and titanium dioxides are not available in the literature. Hence it is interesting to compare the eutectic temperatures in the copper oxides and other simple oxide systems. The eutectic temperatures for  $\text{CuO}$ ,  $\text{Cu}_2\text{O}$  and other oxide ( $\text{M}_x\text{O}_y$ ) system at  $p_{\text{O}_2} = 1$  atm and 0.21 atm were compiled in Table 1. The melting temperatures of the oxide  $\text{M}_x\text{O}_y$  are also given. The simple oxide systems, denoted as a terminal oxide in the table, include  $\text{Al}_2\text{O}_3$ ,<sup>6</sup>  $\text{B}_2\text{O}_3$ ,<sup>7</sup>  $\text{CaO}$ ,<sup>6</sup>  $\text{Cr}_2\text{O}_3$ ,<sup>7</sup>  $\text{Fe}_2\text{O}_3$ ,<sup>8</sup>  $\text{NiO}$ ,<sup>9</sup>  $\text{PbO}$ ,<sup>10</sup>  $\text{SiO}_2$ ,<sup>10</sup>  $\text{TeO}_2$ ,<sup>7</sup>  $\text{ZrO}_2$ ,<sup>8</sup> etc. As given in the table, the eutectic temperatures are higher than  $1010^\circ\text{C}$  when the melting points of  $\text{M}_x\text{O}_y$  are larger than  $1000^\circ\text{C}$ . It is worth noting that  $\text{CuO}$  decomposes into  $\text{Cu}_2\text{O}$  at about  $1031^\circ\text{C}$  in air.<sup>2</sup> Consider the  $\text{Cu}_x\text{O}$  and simple oxide system like  $\text{PbO}$ ,  $\text{SiO}_2$ ,  $\text{TeO}_2$  and  $\text{ZrO}_2$  where no intermediate phases occur; the eutectic temperature tends to increase when the melting point of the simple oxide is higher. Since no intermediate phases have been observed in air for the

$\text{CuO-TiO}_2$  system, the eutectic temperature in the system as previously observed from the microstructural changes is considerably low concerning the high melting point of  $\text{TiO}_2$  ( $T_m = 1825^\circ\text{C}$ ).

Assume the quasi-binary system exhibits complete miscibility in the liquid state and virtually complete immiscibility in the solid state, the liquidus curves and the eutectic points can be calculated providing the eutectic reactions occur.<sup>11</sup> Consider the  $\text{CuO-TiO}_2$  system exhibits this type of phase diagram. If the liquid solutions are Raoultian, when pure  $\text{CuO}$  is in equilibrium with the liquid solution of the liquidus composition, the standard Gibbs free energy change can be expressed as

$$\begin{aligned}\Delta G_{\text{m}(\text{CuO})}^\circ &= G_{\text{CuO(l)}}^\circ - G_{\text{CuO(s)}}^\circ \\ &= -RT \ln X_{\text{CuO}(\text{liquidus})} = \Delta H_{\text{m}(\text{CuO}), T_m}^\circ \\ &\quad + \int_{T_m}^T \Delta C_{\text{p, CuO}} dT \\ &\quad - T \left( \Delta S_{\text{m}(\text{CuO}), T_m}^\circ + \int_{T_m}^T \frac{\Delta C_{\text{p, CuO}}}{T} dT \right)\end{aligned}$$

where  $X_{\text{CuO}(\text{liquidus})}$  is the composition of the  $\text{CuO}$  liquidus at  $T$ ,  $\Delta C_p = C_{\text{p(l)}} - C_{\text{p(s)}}$ ,  $T_m$  is the melting point. Using the thermodynamic data available in the literature<sup>1</sup> as given in Table 2, the liquidus curves could be calculated.

$$\begin{aligned}\Delta G_{\text{m}(\text{CuO})}' &= -RT \ln X_{\text{CuO}(\text{liquidus})} = -1834 + 52.45T \\ &\quad + 3.1 \times 10^{-3} T^2 - 7.66 T \ln T\end{aligned}$$

Similar to  $\text{CuO}$ , the  $\text{TiO}_2$  liquidus could be calculated

$$\begin{aligned}\Delta G_{\text{m}(\text{TiO}_2)}^\circ &= \Delta H_{\text{m}(\text{TiO}_2), T_m}^\circ + \int_{T_m}^T \Delta C_{\text{p, TiO}_2} dT \\ &\quad - T \left( \Delta S_{\text{m}(\text{TiO}_2), T_m}^\circ + \int_{T_m}^T \frac{\Delta C_{\text{p, TiO}_2}}{T} dT \right) \\ &= 5027 + 23.59T + 1.4 \times 10^{-4} T^2 - 2.18 \times 10^5 \frac{1}{T} \\ &\quad - 3.43 T \ln T = -RT \ln X_{\text{TiO}_2(\text{liquidus})}\end{aligned}$$

Table 1

The eutectic temperatures ( $T_{\text{EU}}$ ) in the  $\text{Cu}_x\text{O}$  and other oxide ( $\text{M}_x\text{O}_y$ ) system at mainly  $p_{\text{O}_2} = 1$  and 0.21 atm. The melting temperatures of the oxide ( $\text{M}_x\text{O}_y$ ),  $T_m(\text{M}_x\text{O}_y)$  are also given

$\text{Cu}_x\text{O}$	$\text{M}_x\text{O}_y/\text{terminal oxide}$	$T_{\text{EU}}$ ( $^\circ\text{C}$ )	$p_{\text{O}_2}$ (atm)	$T_m(\text{M}_x\text{O}_y)$ ( $^\circ\text{C}$ )	Ref.
$\text{Cu}_2\text{O}$	$\text{Cu}_2\text{O} \cdot \text{Al}_2\text{O}_3 / \text{Al}_2\text{O}_3$	1130	0.21	1238	6
$\text{CuO}$	$\text{CuO} \cdot \text{Al}_2\text{O}_3 / \text{Al}_2\text{O}_3$	1108	1	1240	
$\text{CuO}$	$3\text{CuO} \cdot \text{B}_2\text{O}_3 / \text{B}_2\text{O}_3$	950	0.21	1000	7
$\text{CuO}$	$\text{CuO} \cdot 2\text{CaO} / \text{CaO}$	1013	0.21	1030	6
$\text{CuO}$	$\text{CuO} \cdot 2\text{CaO} / \text{CaO}$	1052	1	1080	
$\text{Cu}_2\text{O}$	$\text{CuCrO}_2 / \text{Cr}_2\text{O}_3$	1130	0.21	—	7
$\text{CuO}$	$\text{CuFe}_2\text{O}_4 / \text{Fe}_2\text{O}_3$	1070	1	—	8
$\text{Cu}_2\text{O}$	$(\text{Cu}, \text{Ni})\text{O} / \text{NiO}$	1090	0.21	—	9
$\text{Cu}_2\text{O}$	$\text{PbO} / \text{PbO}$	680	—	850	10
$\text{Cu}_2\text{O}$	$\text{SiO}_2 / \text{SiO}_2$	1060	—	1713	10
$\text{Cu}_2\text{O}$	$\text{TeO}_2 / \text{TeO}_2$	610	(Ar)	733	7
$\text{Cu}_2\text{O}$	$\text{ZrO}_2 / \text{ZrO}_2$	1130	0.21	2715	8
$\text{CuO}$	$\text{ZrO}_2 / \text{ZrO}_2$	1097	1	2710	

Table 2

Thermodynamic data of  $\text{CuO}$  and  $\text{TiO}_2$ <sup>1</sup> for the calculation of the phase diagram.  $T_m$  is the melting point,  $\Delta H_{\text{m}, T_m}$  represents the heat of fusion, and  $C_p$  denotes the heat capacity

	$\text{CuO}$	$\text{TiO}_2$
$T_m$ ( $^\circ\text{C}$ )	1121 (1394 K) ( $p_{\text{O}_2} = 1$ atm)	1825 (2098 K)
$\Delta H_{\text{m}, T_m}$ (cal/g-mol)	2,820	11,400
$C_{\text{p(s)}}$ (cal/g-mol)	$14.34 + 6.2 \times 10^{-3} T$	$17.97 + 0.28 \times 10^{-3} T - \frac{4.35 \times 10^5}{T^2}$
$C_{\text{p(l)}}$ (cal/g-mol)	22	21.4

Hence the CuO and TiO<sub>2</sub> liquidus curves can be rewritten as

$$\ln X_{\text{CuO(liquidus)}} = \frac{926}{T} - 26.5 - 1.57 \times 10^{-3}T + 3.87T$$

$$\ln X_{\text{TiO}_2(\text{liquidus})} = \frac{1.10 \times 10^5}{T^2} - \frac{2539}{T} - 11.91 - 7.07 \times 10^{-5}T + 1.73 \ln T$$

The liquidus curves are plotted in Fig. 6. The calculated eutectic point is at  $T=919^\circ\text{C}$  and  $X_{\text{TiO}_2}=16.7$  mol%. The eutectic temperature is rather low compared to that in other CuO-oxide systems. It is worth noting that the obtained phase diagram was calculated at  $p\text{O}_2=1$  atm where CuO, the only stable oxide phase of Cu in pure oxygen, melts at  $1121^\circ\text{C}$ . Since CuO may melt congruently or incongruently at quite different temperatures when  $p\text{O}_2$  changes,<sup>2</sup> the phase diagram apparently would be varied accordingly. In air CuO would not melt but decomposes at  $1031^\circ\text{C}$  into Cu<sub>2</sub>O which in turn melts incongruently at  $1134^\circ\text{C}$ .<sup>2</sup> Hence the diagram in air would be quite different. This is worth being further investigated.

### 3.4. Potential applications

Several potential applications of the eutectic reactions in the system have been proposed. As described earlier the CuO–TiO<sub>2</sub> eutectic reaction could aid significantly the grain growth of TiO<sub>2</sub>. Large-grained TiO<sub>2</sub> samples could be easily prepared by adding a small amount of Cu or CuO into TiO<sub>2</sub> during sintering. The grain size could increase more than 100 times (from 0.3 to 50 μm) comparing to that prepared from the normal sintering process. Since the eutectic reaction could also enhance the oxidation of Cu. A small amount of TiO<sub>2</sub> could be

added to Cu to prepare a large CuO crystal that is almost not possible when prepared directly from the oxidation of Cu.

When annealing the Cu/TiO<sub>2</sub> samples at  $900^\circ\text{C}$  for 10 min, CuO resulted from the reactions would diffuse into TiO<sub>2</sub> at the contact area to form a thin layer. After the CuO-diffused TiO<sub>2</sub> samples were annealed in a reducing gas such as  $\text{N}_2/\text{H}_2=9$  at the same temperature for about 30 min, CuO was completely reduced to Cu and Cu films then remained on the top of TiO<sub>2</sub> surface. The conductive films are continuous, which was verified by a resistance meter. This could provide another way to prepare Cu films on oxides by employing the reactions. Like many other systems, eutectic bonding of the Cu and TiO<sub>2</sub> is the nature candidate for the application of the reaction. Hence it is important to investigate systematically the reactions between Cu and TiO<sub>2</sub> under different oxygen partial pressures including the eutectic reactions in the CuO–TiO<sub>2</sub> and Cu<sub>2</sub>O–TiO<sub>2</sub> systems.

## 4. Summary

After annealing at various temperatures ranging from 300 to  $1070^\circ\text{C}$ , the changes in the appearance, the normalized (to original Cu) weight, the crystal structure, and the microstructure of the Cu/TiO<sub>2</sub> samples have been analyzed to investigate the eutectic reaction. The reaction diagram concerning the resulted appearance of the samples have been generated. The CuO–TiO<sub>2</sub> eutectic reaction could be observed at as low as  $900^\circ\text{C}$  which is considerably low compared to copper oxides and other high melting point oxides eutectic systems. Annealing in gases possessing lower oxygen partial pressures at corresponding conditions as in air would cause less drastic melting, which may attribute to a higher eutectic temperature. The CuO–TiO<sub>2</sub> eutectic reaction could enhance significantly the oxidation of Cu and the grain growth of TiO<sub>2</sub>. The eutectic point of the CuO and TiO<sub>2</sub> has been successfully calculated to be at  $T=919^\circ\text{C}$  and  $X_{\text{TiO}_2}=16.7$  mol% in  $p\text{O}_2=1$  atm. Several applications of the eutectic reactions have been proposed and demonstrated.

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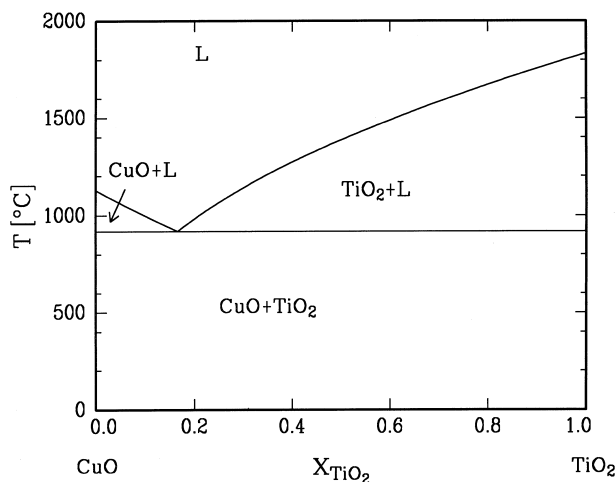


Fig. 6. The calculated CuO–TiO<sub>2</sub> phase diagram at  $p\text{O}_2=1$  atm. Eutectic point is at  $T=919^\circ\text{C}$  and  $X_{\text{TiO}_2}=16.7$  mol%.

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