

# Microstructural and electrical characteristics of $\text{Y}_2\text{O}_3$ -doped $\text{ZnO-Bi}_2\text{O}_3$ -based varistor ceramics

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## Abstract

The microstructural and electrical characteristics of  $\text{ZnO-Bi}_2\text{O}_3$ -based varistor ceramics doped with  $\text{Y}_2\text{O}_3$  in the range from 0 to 0.9 mol% have been investigated. The addition of  $\text{Y}_2\text{O}_3$  resulted in the formation of a fine-grained  $\text{Bi-Zn-Sb-Y-O}$  phase along the grain boundaries of the  $\text{ZnO}$  grains which inhibits the grain growth. The mean  $\text{ZnO}$  grain size decreased from 11.3 to 5.4  $\mu\text{m}$  with increasing amounts of  $\text{Y}_2\text{O}_3$ . The threshold voltage ( $V_T$ ) of the ceramics increased from 150 to 274 V/mm, the non-linear coefficient  $\alpha$  was not influenced and remained at approximately 40, and the leakage current also increased with the amount of  $\text{Y}_2\text{O}_3$  added. On the basis of the Mukae et al. (Mukae, K., Tsuda, K. and Nagasawa, I., Capacitance-vs-voltage characteristics of  $\text{ZnO}$  varistors. *J. Appl. Phys.*, 1979, **50**, 4475–4476) Schottky barrier model of  $\text{ZnO}$  varistors, the addition of  $\text{Y}_2\text{O}_3$  resulted in a slight increase in the density of interface states ( $N_S$ ) and a more pronounced increase in the donor density ( $N_D$ ), causing a decrease of the barrier height ( $\Phi_B$ ) and the depletion layer width ( $t$ ). The increase of the leakage current ( $I_L$ ) with higher amounts of  $\text{Y}_2\text{O}_3$  added can be ascribed to the increase in donor density ( $N_D$ ) as well as to the increased amount of  $\text{Y}_2\text{O}_3$ -containing phase at the grain boundaries of  $\text{ZnO}$ .  
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## 1. Introduction

$\text{ZnO}$ -based varistors are characterised by highly non-linear current-voltage characteristics and a high energy-absorption capability. As a result they are widely used as surge absorbers in electronic circuits, devices and electrical power systems to protect against dangerous over-voltage surges. In the classical  $\text{ZnO}$ -based varistor,  $\text{Bi}_2\text{O}_3$  is used as the varistor-former, while other oxides such as  $\text{Sb}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$ ,  $\text{Mn}_3\text{O}_4$ ,  $\text{NiO}$  and others are added in small amounts to further enhance the non-linearity of the varistor's behaviour. The non-linear current-voltage characteristics of  $\text{ZnO}$  varistor ceramics results from the formation of double Schottky barriers at the grain boundaries. These non-ohmic  $\text{ZnO-ZnO}$  grain boundaries each have a break-down voltage of 3V and so the overall break-down voltage of the varistor builds up from the non-ohmic grain boundaries between

the electrodes of the varistor and can be controlled either by the varistor thickness or the  $\text{ZnO}$  grain size.<sup>1</sup> High-voltage varistor ceramics require a fine-grained microstructure and  $\text{Sb}_2\text{O}_3$  is usually added to inhibit the  $\text{ZnO}$  grain growth.<sup>2,3</sup> Recently it has been reported that the breakdown voltage and energy characteristics of varistor elements can be significantly increased by the introduction of various rare-earth oxides (REO) and  $\text{Y}_2\text{O}_3$  to the varistor ceramics.<sup>4</sup>

In the present work, the influence of the amount of added  $\text{Y}_2\text{O}_3$  on the microstructure, current-voltage ( $I$ - $V$ ) and capacitance-voltage ( $C$ - $V$ ) characteristics of  $\text{ZnO-Bi}_2\text{O}_3$ -based varistor ceramics has been investigated.

## 2. Experimental

$\text{ZnO-Bi}_2\text{O}_3$ -based varistor samples with the nominal composition  $(96.2-x)$  mol%  $\text{ZnO} + 0.9$  mol%  $\text{Bi}_2\text{O}_3 + 2.9$  mol%  $(\text{Sb}_2\text{O}_3 + \text{Co}_3\text{O}_4 + \text{Mn}_3\text{O}_4 + \text{NiO} + \text{Cr}_2\text{O}_3) + x\text{Y}_2\text{O}_3$  for  $x = 0, 0.1, 0.3, 0.45$  and 0.9 (sample labeled Y0, Y1,

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Y3, Y5 and Y9, respectively) were prepared by the classical ceramic procedure. Reagent-grade oxides were mixed in proper ratios and homogenized in absolute ethanol using a planetary mill. The powders were dried at 70°C and pressed with 200 MPa into discs 10 mm in diameter and 2 mm thick. The pellets were fired in an alumina crucible at 1230°C for 2 h with heating and cooling rates of 5°C/min in air. Selected samples were also fired at 800 or 900°C for 1 h to determine their phase composition at the onset of sintering.

Densification characteristics were recorded using a heating-stage microscope up to 1300°C at a heating rate 10 K/min. The phase constitution of the samples was analysed by X-ray powder diffraction analysis (XRD). The samples' microstructures were examined using a scanning electron microscope (SEM) in backscattered electron mode. Phase compositions of the samples and the composition of the individual phases were determined by energy-disperse X-ray spectroscopy (EDS) in the SEM. The average ZnO grain size ( $D$ ) was determined for each sample using 500–800 measurements of grain size per sample. The surface of each grain was measured and its size was calculated as a diameter for circular geometry.

For DC current–voltage ( $I$ – $V$ ) characterisation, silver electrodes were painted on both surfaces of the disk and fired at 590°C in air. The nominal varistor voltages ( $V_N$ ) at 1 and 10 mA were measured and the threshold voltage  $V_T$  (V/mm) and non-linear coefficient  $\alpha$  were determined. The leakage current ( $I_L$ ) was measured at 0.75  $V_N$  (1 mA).

The  $C$ – $V$  characteristics of the varistor samples were measured at room temperature with an LCR meter (Hewlett Packard 4270 A) at a frequency of 10 kHz and a bias voltage in the 0–180 V range, controlled by a digital V-meter (Hewlett Packard 3456 A). According to the Schottky-barrier model and its  $C$ – $V$  relation, the donor density ( $N_D$ ), barrier height ( $\Phi_B$ ), density of interface states ( $N_S$ ) and the depletion-layer width ( $t$ ) were determined.  $N_D$  and  $\Phi_B$  were determined from the slope and the intercept of the  $C$ – $V$  line of the graph  $(1/C_B - 1/2C_{B0})^2$  vs.  $V_G$ , and  $N_S$ , and  $t$  were calculated from equations given elsewhere.<sup>5–7</sup>

### 3. Results and discussion

XRD patterns of the investigated samples are given in Fig. 1. In the sample without  $Y_2O_3$ , three phases were identified: the ZnO phase,  $\gamma$ - $Bi_2O_3$  phase and the  $Zn_7Sb_2O_{12}$ -type spinel phase. However, in samples doped with  $Y_2O_3$ , additional peaks are evident and their intensity increases with increasing amounts of  $Y_2O_3$  in the starting composition. Fig. 2 shows microstructures of the investigated samples. As can be seen from these back-scattered SEM micrographs, the three phases

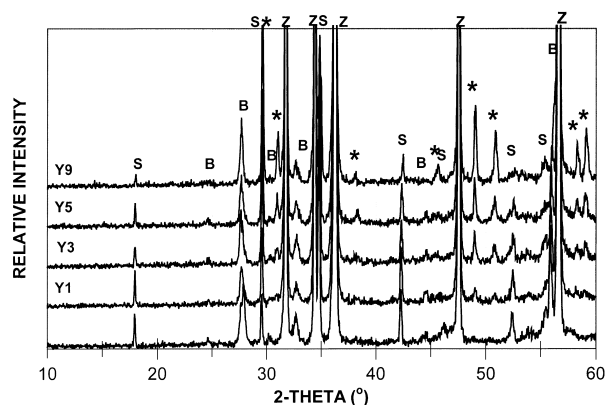


Fig. 1. XRD patterns of ZnO– $Bi_2O_3$ -based varistor ceramics doped with  $Y_2O_3$  and fired at 1230°C for 2 h; (a) Y0 (0 mol%), (b) Y1 (0.1 mol%), (c) Y3 (0.3 mol%), (d) Y5 (0.45 mol%) and (e) Y9 (0.9 mol%). Z: ZnO phase, B:  $\gamma$ - $Bi_2O_3$  phase, S:  $Zn_7Sb_2O_{12}$ -type spinel phase, \*:  $Y_2O_3$ -containing phase.

already identified by XRD analysis were observed in sample without  $Y_2O_3$ , while in samples doped with  $Y_2O_3$  an additional phase was detected. EDS analysis revealed this to be a Bi–Zn–Sb–Y–O phase with traces of oxides of Cr, Mn, Co and Ni. Determination of the exact composition by EDS analysis is difficult due to the small grains of  $Y_2O_3$ -containing phase which have a size below 2  $\mu m$ . However, in all the samples a cation ratio of Bi:Zn:Sb:Y:O close to 0.4:1:1:1 was determined for the  $Y_2O_3$ -containing phase.  $Y_2O_3$  was not detected in the ZnO phase nor in  $Bi_2O_3$ -rich and  $Zn_7Sb_2O_{12}$ -type spinel secondary phases above the detection limit for EDS analysis, which is at roughly 0.1 wt.%. Formation of the  $Y_2O_3$ -containing phase was already observed at lower temperatures. In samples fired at 800°C, a Bi–Zn–Y–O phase was identified by EDS analysis in addition to the ZnO phase and the  $Zn_7Sb_2O_{12}$ -type spinel phase in the fine-grained microstructure of the  $Y_2O_3$ -doped samples. After firing at 900°C, the Bi–Zn–Sb–Y–O-type phase is already present with the  $Bi_2O_3$ -rich and  $Zn_7Sb_2O_{12}$ -type spinel secondary phases. The  $Bi_2O_3$ -rich phase melts at 740°C and in samples fired at 900°C the presence of a liquid phase resulted in a significantly coarser ZnO grain size in comparison with the  $Y_2O_3$ -doped samples fired at 800°C. In the sample without  $Y_2O_3$  (Y0), the  $Bi_2O_3$ -rich phase is present in addition to the  $Zn_7Sb_2O_{12}$ -type spinel and  $Bi_3Zn_2Sb_3O_{11}$ -type pyrochlore secondary phases at 800°C. The  $Y_2O_3$ -containing phase bounds the  $Bi_2O_3$  and influences the sintering of the samples. In samples with a higher amount of  $Y_2O_3$  in the starting composition the onset of sintering is shifted to a higher temperature, as can be seen from the densification curves in Fig. 3.

The amount of  $Y_2O_3$ -containing phase increased with the amount of  $Y_2O_3$  in the starting composition. It is fine grained with a grain size significantly smaller than the  $Zn_7Sb_2O_{12}$ -type spinel phase, distributed uniformly

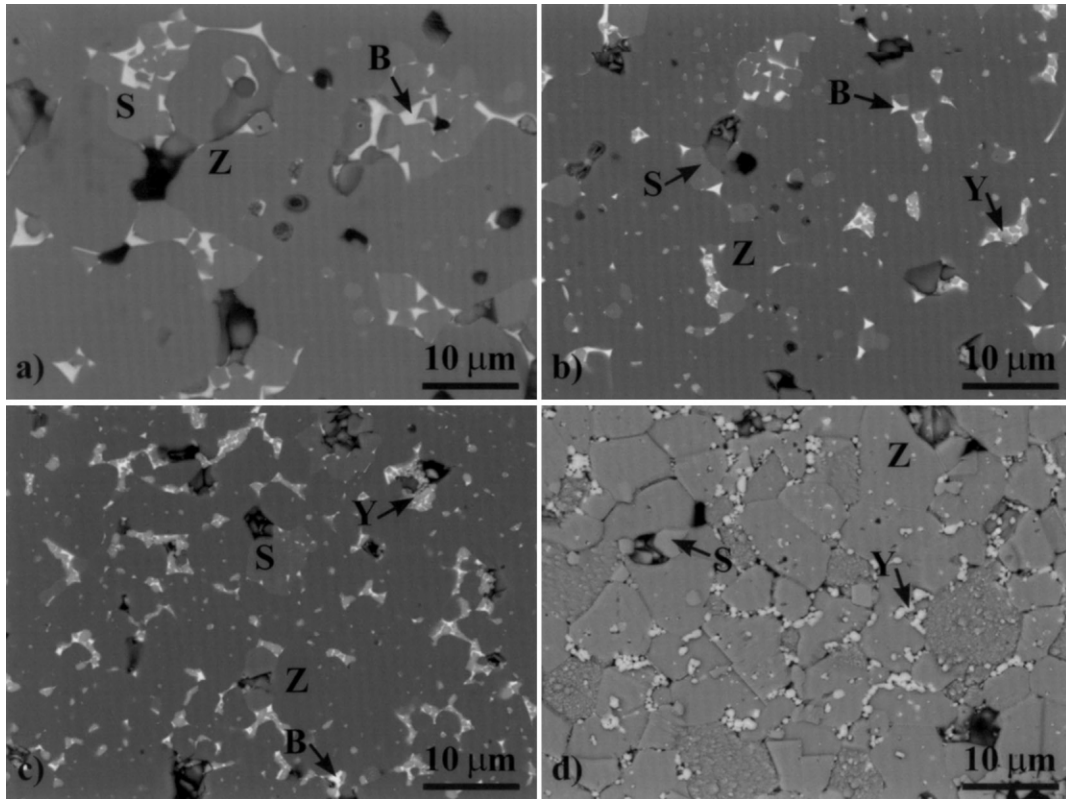


Fig. 2. Microstructures of ZnO–Bi<sub>2</sub>O<sub>3</sub> based varistor ceramics fired at 1230°C for 2 h, doped with varying amounts of Y<sub>2</sub>O<sub>3</sub>; (a) 0 mol% (Y0), (b) 0.3 mol% (Y3), (c) 0.9 mol% (Y9) and (d) 0.9 mol% (Y9 — microstructure etched with diluted hydrochloric acid). Z: ZnO phase, B: Bi<sub>2</sub>O<sub>3</sub>-rich phase, S: Zn<sub>7</sub>Sb<sub>2</sub>O<sub>12</sub>-type spinel phase, Y: Y<sub>2</sub>O<sub>3</sub>-containing phase.

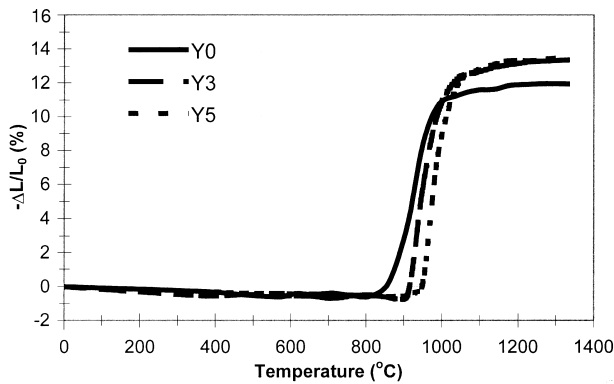


Fig. 3. Densification curves of ZnO–Bi<sub>2</sub>O<sub>3</sub> based varistor samples doped with varying amounts of Y<sub>2</sub>O<sub>3</sub>.

along the grain boundaries of the ZnO (Fig. 2d) and may inhibit grain growth effectively. The size of ZnO grains uniformly decreased with the amount of Y<sub>2</sub>O<sub>3</sub> added. This resulted in a significant increase in the threshold voltage ( $V_T$ ) of the varistor ceramics and is also shown in Fig. 4. Doping with Y<sub>2</sub>O<sub>3</sub> did not influence the non-linear coefficient  $\alpha$ , which was approximately 40 ( $\pm 3$ ) for all the investigated samples. However, the leakage current ( $I_L$ ) of the samples increased with

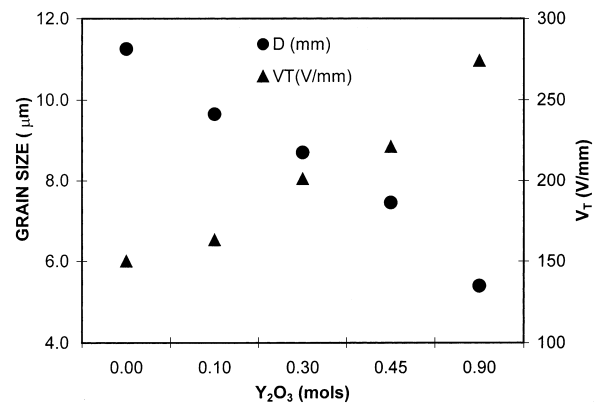


Fig. 4. ZnO grain size  $D$  ( $\mu\text{m}$ ) and threshold voltage  $V_T$  (V/mm) vs. amount of Y<sub>2</sub>O<sub>3</sub> added to the ZnO–Bi<sub>2</sub>O<sub>3</sub>-based varistor ceramics fired at 1230°C for 2 h.

increasing amounts of Y<sub>2</sub>O<sub>3</sub> (Table 1). The increase is particularly significant in the sample with the largest addition of Y<sub>2</sub>O<sub>3</sub> (0.9 mol%). It can be assumed that such an increase of leakage current in this sample is at least to some extent related to a pronounced increase in the amount of Y<sub>2</sub>O<sub>3</sub>-containing phase at the grain boundaries of ZnO. The electrical characteristics (resistivity) of this Bi–Zn–Sb–Y–O (Cr, Co, Mn, Ni) phase, however, are not known at present. It should also be

Table 1  
C–V characteristic parameters of ZnO–Bi<sub>2</sub>O<sub>3</sub>-based varistor ceramics doped with Y<sub>2</sub>O<sub>3</sub> and leakage current  $I_L$  at 0.75  $V_N$  (1 mA)

Y <sub>2</sub> O <sub>3</sub> (mol)	$N_D$ ( $\times 10^{18} \text{ cm}^{-3}$ )	$N_S$ ( $\times 10^{12} \text{ cm}^{-2}$ )	$\Phi_B$ (eV)	$t$ (nm)	$I_L$ ( $\times 10^{-3} \text{ A}$ )
0	0.79	2.88	1.12	37	0.04
0.1	1.17	3.00	0.82	26	0.05
0.3	0.70	2.34	0.83	33	0.07
0.45	1.22	2.90	0.74	24	0.11
0.9	1.91	3.61	0.73	19	0.89

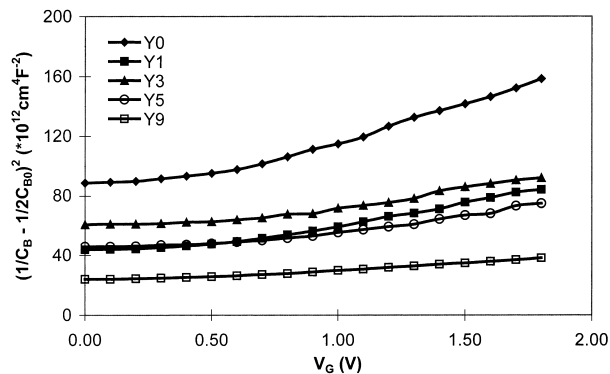


Fig. 5. C–V characteristics of ZnO–Bi<sub>2</sub>O<sub>3</sub>-based varistor ceramics doped with Y<sub>2</sub>O<sub>3</sub> in the range from 0 to 0.9 mol%;  $C_B$ : capacitance per unit area of a grain boundary,  $C_{BO}$ : value of  $C_B$  when  $V_G = 0$ ,  $V_G$ : applied voltage per grain boundary.

considered that this phase influences the distribution of all other varistor dopants along the grain boundaries of ZnO as well.

The capacitance–voltage (C–V) characteristics of the investigated samples are shown in Fig. 5 and the characteristic C–V parameters, using the Mukae et al. analysis,<sup>5</sup> are given in Table 1. On the basis of this analysis, doping with Y<sub>2</sub>O<sub>3</sub> resulted in an increase of the donor density ( $N_D$ ) as well as the density of interface states ( $N_S$ ). Generally, the barrier height ( $\Phi_B$ ) increases with an increase of the density of interface states, however, a larger variation rate of donor concentration prevailed and the barrier height ( $\Phi_B$ ) decreased with larger amounts of Y<sub>2</sub>O<sub>3</sub>. The depletion-layer width was observed to decrease as well. An increase in the donor concentration can also contribute to an increase in the leakage current, and this is particularly significant in the sample with 0.9 mol% of Y<sub>2</sub>O<sub>3</sub>.

#### 4. Conclusions

Doping of ZnO–Bi<sub>2</sub>O<sub>3</sub>-based varistor ceramics with Y<sub>2</sub>O<sub>3</sub> results in the formation of a Bi–Zn–Sb–Y–O

phase with a cation ratio close to 0.4:1:1:1. Y<sub>2</sub>O<sub>3</sub> does not enter the ZnO grains and was not detected in either the Bi<sub>2</sub>O<sub>3</sub>-rich phase or the Zn<sub>7</sub>Sb<sub>2</sub>O<sub>12</sub>-type spinel phase. In samples with higher amounts of Y<sub>2</sub>O<sub>3</sub> in the starting composition and hence a higher amount of Y<sub>2</sub>O<sub>3</sub>-containing phase which bounds the Bi<sub>2</sub>O<sub>3</sub>, the onset of sintering is shifted to a higher temperature. The fine-grained Y<sub>2</sub>O<sub>3</sub>-containing phase present at the grain boundaries strongly inhibits ZnO grain growth. The ZnO grain size decreased from 11.3 to 5.4  $\mu\text{m}$  with increasing amounts of Y<sub>2</sub>O<sub>3</sub>. The decrease in the ZnO grain size resulted in an increase in the threshold voltage ( $V_T$ ) of the samples from 150 to 274 V/mm. Doping with Y<sub>2</sub>O<sub>3</sub> does not influence the non-linear coefficient  $\alpha$  of the varistor ceramics while the leakage current ( $I_L$ ) increases with increasing amounts of Y<sub>2</sub>O<sub>3</sub>.

Schottky barrier analysis of C–V data showed that Y<sub>2</sub>O<sub>3</sub> doping results in an increase in the density of interface states ( $N_S$ ) and an even greater rise in the donor density ( $N_D$ ). The barrier height ( $\Phi_B$ ) decreases with increasing amounts of Y<sub>2</sub>O<sub>3</sub>, from 1.12 eV in the Y<sub>2</sub>O<sub>3</sub>-free sample to  $0.78 \pm 0.05$  eV for the Y<sub>2</sub>O<sub>3</sub>-doped samples.

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#### References

- Clarke, D. R., Varistor ceramics. *J. Am. Ceram. Soc.*, 1999, **82**, 485–502.
- Asokan, T. G., Iyengar, N. K. and Nagabhushana, G. R., Studies on microstructure and density of sintered ZnO-based non-linear resistors. *J. Mater. Sci.*, 1987, **22**, 2229–2236.
- Kim, J., Kimura, T. and Yamaguchi, T., Microstructure development in Sb<sub>2</sub>O<sub>3</sub>-doped ZnO. *J. Mater. Sci.*, 1989, **24**, 2581–2586.
- Shichimiya, S., Yamaguchi, M., Furuse, N., Kobayashi, M. and Ishibe, S., Development of advanced arresters for GIS with new zinc-oxide elements. *IEEE Trans. Power Delivery*, 1998, **13**, 465–471.
- Mukae, K., Tsuda, K. and Nagasawa, I., Capacitance-vs-voltage characteristics of ZnO varistors. *J. Appl. Phys.*, 1979, **50**, 4475–4476.
- Fan, J. and Freer, R., The electrical properties and d.c. degradation characteristics of silver doped ZnO varistors. *J. Mater. Sci.*, 1993, **28**, 1391–1395.
- Sun, H. T., Zhang, L. Y. and Yao, X., Electrical nonuniformity of grain boundaries within ZnO varistors. *J. Am. Ceram. Soc.*, 1993, **76**, 1150–1155.