

# Reaction kinetics in $\text{Ti}_3\text{SiC}_2$ synthesis studied by time-resolved neutron diffraction

E. Wu<sup>a,b</sup>, D.P. Riley<sup>a</sup>, E.H Kisi<sup>a,\*</sup>, R.I. Smith<sup>c</sup>

<sup>a</sup> School of Engineering, The University of Newcastle, Callaghan, NSW 2308, Australia

<sup>b</sup> Shenyang National Laboratory for Materials Science, Shenyang 110016, PR China

<sup>c</sup> ISIS Facility, Rutherford Appleton Laboratory, Chilton, Didcot, Oxon OX11 0QX, UK

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## Abstract

The reactive sintering of  $3\text{Ti}/\text{SiC}/\text{C}$  to form the ternary carbide  $\text{Ti}_3\text{SiC}_2$ , previously found to involve the intermediate phases  $\text{TiC}_x$  and  $\text{Ti}_5\text{Si}_3\text{C}_x$ , was investigated by time-resolved neutron powder diffraction. The kinetics of  $\text{Ti}_3\text{SiC}_2$  formation from the intermediate phases  $\text{TiC}_x$ ,  $\text{Ti}_5\text{Si}_3\text{C}_x$  ( $x \leq 1$ ) and a small amount of free C was determined. The crystallization rate of the  $\text{Ti}_3\text{SiC}_2$  phase was determined through quantitative analyses of the diffraction patterns collected at different temperatures and is initially well-described by the Mehl–Avrami–Johnson equation. The activation energy was found to be  $380 \pm 10$  kJ/mol and the Avrami exponent  $3.0 \pm 0.2$ . The Avrami exponent decreases to close to 1 when more than half of the crystallization process was completed. This indicates a change in the mechanism of  $\text{Ti}_3\text{SiC}_2$  crystal growth from unrestricted two or three-dimensional growth in the  $a$ – $b$  planes to one-dimensional growth only, due to interaction of the growing disk-like crystals and cessation of growth in the preferred direction.

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## 1. Introduction

The last few years have seen strong interest in studies of the ternary carbide  $\text{Ti}_3\text{SiC}_2$  because of its unique combination of properties.<sup>1–8</sup>  $\text{Ti}_3\text{SiC}_2$  has been prepared using several different methods.<sup>9–15</sup> Among them the reactive sintering of  $3\text{Ti}/\text{SiC}/\text{C}$  to form  $\text{Ti}_3\text{SiC}_2$  has been extensively studied since, when coupled with hot pressing, this process can produce fully dense near-single phase  $\text{Ti}_3\text{SiC}_2$  ceramic.<sup>1,11</sup> To understand the reaction mechanism and its time and temperature dependence, we have studied the process using in situ neutron diffraction techniques.<sup>16,17</sup> By conducting the experiments in situ, the microstructural processes and phase transitions occurring in bulk ceramics are revealed in a time-resolved sequence. The reaction paths re-

vealed by in situ neutron diffraction during the heating of  $3\text{Ti}/\text{SiC}/\text{C}$  mixtures at  $10^\circ\text{C}/\text{min}$  and reactive sintering at  $1600^\circ\text{C}$  to synthesise  $\text{Ti}_3\text{SiC}_2$  were discussed in our previous papers.<sup>16,17</sup> There two well-separated reaction stages were observed. In the first stage the two intermediate phases identified by El-Raghy and Barsoum,<sup>18</sup>  $\text{TiC}_x$  and  $\text{Ti}_5\text{Si}_3\text{C}_x$  ( $x \leq 1$ ), occurred in the sample according to the overall reaction  $9\text{Ti} + 3\text{SiC} + 3\text{C} \rightarrow 4\text{TiC}_x + \text{Ti}_5\text{Si}_3\text{C}_x + \text{C}$  ( $x \leq 1$ ). By  $1400^\circ\text{C}$  all of the Ti has been consumed. In the second stage the two intermediate phases plus a small amount of carbon become the only phases in the system prior to the appearance of the product phase. The intermediate phases react to form  $\text{Ti}_3\text{SiC}_2$  according to the overall reaction  $4\text{TiC}_x + \text{Ti}_5\text{Si}_3\text{C}_x + \text{C}$  ( $x \leq 1$ )  $\rightarrow 3\text{Ti}_3\text{SiC}_2$ .<sup>17</sup> Based on the concentrations of the  $\text{Ti}_3\text{SiC}_2$  phase calculated from quantitative phase analysis of the diffraction patterns, formation of  $\text{Ti}_3\text{SiC}_2$  is slow at temperatures near  $1200^\circ\text{C}$  and, fairly rapid at higher temperatures.<sup>16</sup> However, the kinet-

\* Corresponding author. Tel.: +61 2 4921 6213; fax: +61 2 4921 6946.  
E-mail address: Erich.Kisi@newcastle.edu.au (E.H Kisi).

ics were not quantified in these earlier continuous heating experiments<sup>16,17</sup>—kinetic information is far more readily obtained from isothermal experiments. Knowledge of the reaction kinetics is needed not only for a quantitative description of the temperature–time paths of the reaction, but also for a better understanding of the mechanism of the synthesis process. This paper reports the kinetics of  $\text{Ti}_3\text{SiC}_2$  formation from the intermediate phases  $\text{TiC}_x$ ,  $\text{Ti}_5\text{Si}_3\text{C}_x$  and C in the second sintering stage based upon recent in situ time-resolved neutron diffraction experiments.

## 2. Experimental procedure and analysis

The experimental procedure is very similar to that used previously.<sup>17</sup> Ti (Aldrich 99.98%), SiC (Performance Ceramics 99.9%) and C (graphite Fluka Chemika 99.9%) powders were mixed in stoichiometric proportions and hand ground under argon. Cylindrical pellets of 16 mm diameter and 15 mm high were cold pressed to (180 MPa) in a hard steel die. Two pellets were stacked vertically to increase the mass of sample within the neutron beam and thereby reduce data collection times. Time-of-flight (TOF) neutron powder diffraction data were collected on the POLARIS<sup>19</sup> medium resolution powder diffractometer at the ISIS pulsed neutron spallation source, Rutherford Appleton Laboratory, UK. A coarse mesh cage made from 0.25 mm diameter Mo wire was used to suspend the samples in the neutron beam inside an evacuated ( $\sim 10^{-5}$  Torr) Ta element furnace during the in situ synthesis studies. The furnace was heated up to a predetermined holding temperature at an average rate of  $10^\circ\text{C}/\text{min}$  to ensure that the correct mixture of intermediate phases was formed. The samples were then held at temperature for 2.5 h followed by slow cooling to room temperature. The furnace temperature was measured and controlled by two type W5 thermocouples positioned  $\sim 1$  cm above the sample, in order to limit the amount of extraneous material in the neutron beam. Four heating ramps with holding temperatures of 1450, 1500, 1550 and  $1600^\circ\text{C}$  were employed, respectively, and TOF neutron diffraction patterns were collected as repeated scans of 2.7 min throughout the synthesis process. Provision of collimating slits between the sample and the detector combined with the TOF technique, which enables a complete diffraction pattern to be collected at a single fixed detector position, reduced significantly the intensities and numbers of Bragg reflections arising from the Ta furnace elements and heat shields which appear in the diffraction patterns collected in the  $2\theta \sim 90^\circ$  ZnS detector bank.

Structure refinements were conducted by Rietveld analysis using the program GSAS<sup>20</sup> and the refined scale factors were used to conduct quantitative phase analysis (QPA).<sup>21</sup> In the analysis, the refined parameters were: global parameters (diffractometer zero, the coefficients of a polynomial background), parameters refined for all phases (scale factor and lattice parameters) and ones refined only for majority

phases (the Gaussian and Lorentzian broadening components of the convoluted TOF profile, thermal parameters, structural variables and  $x$ —the site occupancy variable of  $\text{TiC}_x$  and  $\text{Ti}_5\text{Si}_3\text{C}_x$ ).

Based on the concentrations of the  $\text{Ti}_3\text{SiC}_2$  phase in the sample calculated from QPA of the TOF diffraction patterns, and assuming that the reaction is described by the Avrami kinetic equation, the kinetics of  $\text{Ti}_3\text{SiC}_2$  formation expressed as the mol-fraction of the transformed new phase  $f$  at any time  $t$  can be modeled using the Mehl–Avrami–Johnson (MAJ) equation:<sup>22–25</sup>

$$f(t) = 1 - \exp[-(Kt)^n] \quad (1)$$

here  $n$  is the Avrami exponent and  $K$  is the reaction rate constant, which is related to the activation energy of the process,  $E$ , through an Arrhenius temperature dependence:

$$K(T) = K_0 \exp(-E/RT) \quad (2)$$

where  $K_0$  is the frequency factor,  $R$  the gas constant and  $T$  the absolute temperature.

Taking the logarithm of Eq. (1) twice:

$$\ln[-\ln(1 - f)] = n \ln K + n \ln t \quad (3)$$

A plot of  $\ln[-\ln(1 - f)]$  versus  $\ln t$  for different isotherms will give  $n$  and  $K$ , and from these the activation energy of the process  $E$  can be determined.

Besides those intermediate phases  $\text{TiC}_x$  and  $\text{Ti}_5\text{Si}_3\text{C}_x$  ( $x \leq 1$ ), the growth of  $\text{Ti}_3\text{SiC}_2$  crystals requires a small amount of free C for the solid state reaction.<sup>16,17</sup> The free C is not crystalline, and can not be determined from quantitative analysis of the diffraction patterns, thus the derived fraction of the transformed  $\text{Ti}_3\text{SiC}_2$  crystals  $f$  could be affected by ignoring this factor. The effect of free C on the calculated fraction  $f$  is estimated by adding a stoichiometric amount of free C in the calculation and assuming that the free C is reduced to null while the fraction of the transformed  $\text{Ti}_3\text{SiC}_2$  crystals  $f$  reaches the maximum.

The solid state reaction leading to  $\text{Ti}_3\text{SiC}_2$  formation requires an incubation time at constant temperature for appreciable reaction products to be observed. It is possible to describe the reaction time as comprised from two components  $t = t_i + t_c$ , where  $t_i$  is incubation time and  $t_c$  is the crystallization time. However,  $t$  is difficult to measure in our experiments, even though they were conducted isothermally. Due to the large heat capacity of the sample, a considerable period of time is required before the temperature of the sample equilibrated with the furnace temperature, such that in some cases the reaction initiated before sample equilibration at the hold temperature. This incubation time spent at lower temperatures could become quite significant at the higher temperatures when the reaction rate is high.

An iterative method was adopted in our calculation to correct for the effect and access the true incubation time at constant temperature. It can be assumed that the incubation time required for the reaction at low temperature during an exper-

iment would be, in effect, equivalent to a shorter period of time at the hold temperature of the experiment, which can be defined as  $t_0$ , so the total reaction time will become  $t = t_m + t_0$ , where  $t_m$  is measured time, and Eq. (1) becomes:

$$f = 1 - \exp[-(K(t_m + t_0))^n] \quad (4)$$

where  $t_0$  is not known, but was defined as 0 for the initial iteration. An initial  $n$  and  $K$  were derived for each temperature from Eq. (3), and an average activation energy  $E$  estimated. Eq. (2) was then used to calculate a new  $K$ , which was used in Eq. (4) to calculate a new  $t_0$  for each temperature. Then the new  $t_0$  was used to do the second iteration and so on, until convergence was achieved, in this case, after only three iterations.

### 3. Results and discussion

An example of the neutron diffraction data and associated Rietveld refinement fit used for quantitative phase analysis is shown in Fig. 1. The agreement between the calculated and the observed data points is very good. The final plots of  $\ln[-\ln(1-f)]$  versus  $\ln t$  at different temperatures after three iterations are shown in Fig. 2. The value of  $n$  for the formation of  $\text{Ti}_3\text{SiC}_2$  from  $4\text{TiC}_x + \text{Ti}_5\text{Si}_3\text{C}_x + \text{C}$  determined from the measurement of the slopes is  $3.0 \pm 0.2$  and the reaction rate constant  $K$  is  $1.35 \times 10^{-4} \text{ s}^{-1}$  (1450 °C),  $2.84 \times 10^{-4} \text{ s}^{-1}$  (1500 °C),  $5.76 \times 10^{-4} \text{ s}^{-1}$  (1550 °C) and  $1.13 \times 10^{-3} \text{ s}^{-1}$  (1600 °C), respectively. The activation energy  $E = 380 \pm 10 \text{ kJ/mol}$  and  $K_0 = 4.45 \times 10^7 \text{ s}^{-1}$  in Eq. (2) are derived from the three slopes at 1450, 1500 and 1550 °C in Fig. 2.

In a perfect isothermal experiment at uniform temperature intervals, the lines representing the Arrhenius temperature dependence of the reaction rate constant  $K$  on Fig. 2 would be

parallel. As seen in Fig. 2, this is most closely observed for the lower portion of the data at 1450 and 1500 °C. As for the plot at 1550 °C, although the correct spacing between the plots is observed, deviations from linearity occur earlier and are larger. For the data at 1600 °C, the deviation is too large and the spacing is not as expected. The plot is much closer to the data for 1550 °C and the raw Arrhenius temperature relation is not valid for data recorded at 1600 °C. The primary reason for this is the incubation time of the reaction. During the lower temperature isothermal holds (1450 and 1500 °C) the reaction rate was relatively low and the bulk of the reaction occurred at the stated temperature. The small fraction of the incubation time that was spent at a lower temperature can therefore be estimated and compensated for according to our corrected timescale. At 1550 °C the fraction of the incubation time occurring before the start of the isothermal hold increased further. However, for the 1600 °C data, the sample actually completed its incubation time while still at lower temperatures and a small amount of  $\text{Ti}_3\text{SiC}_2$  formed even before the isothermal hold at 1600 °C began. There is potentially an additional effect present in all measurements due to the fact that because the thermocouple was not in contact with the sample, a further lag occurred between the thermocouple indicating the hold temperature and the bulk of the sample reaching this temperature. Hence, the plot for the measurements at 1600 °C actually reflects the reaction at a lower sample temperature. Based on the position of the plot, we can estimate that the sample behaviour during the 1600 °C measurement reflects an actual sample temperature of 1565 °C, some 35 °C lower than the indicated temperature. Assuming this correction to be valid, the  $K$  derived from the plot corresponding to 1565 °C is  $7.07 \times 10^{-4} \text{ s}^{-1}$ . The derived relationship between the fraction of the  $\text{Ti}_3\text{SiC}_2$  phase and the total reaction time at various temperatures fitted by the MAJ equation is shown in Fig. 3.

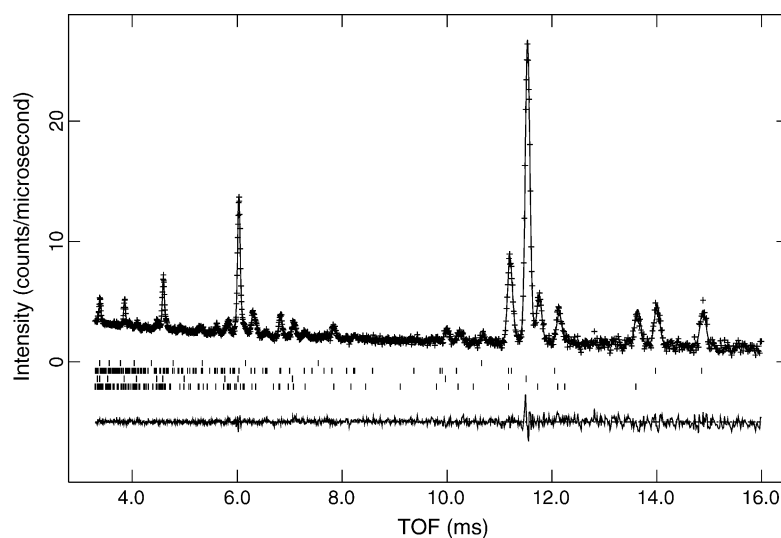


Fig. 1. Rietveld fit to TOF neutron diffraction pattern collected at 1500 °C. Data points are shown as (+) and the calculation as a solid line. The difference profile for the refinement along with reflection markers for the phases  $\text{Ti}_3\text{SiC}_2$  (bottom),  $\text{TiC}_{1.0}$  (middle lower),  $\text{Ti}_5\text{Si}_3\text{C}_{0.64}$  (middle higher) and reflections from the Ta furnace element (top) are shown below the pattern. TOF (ms) may be converted to  $d$ -spacing (Å) by multiplying by  $2.19 \times 10^{-4}$ .

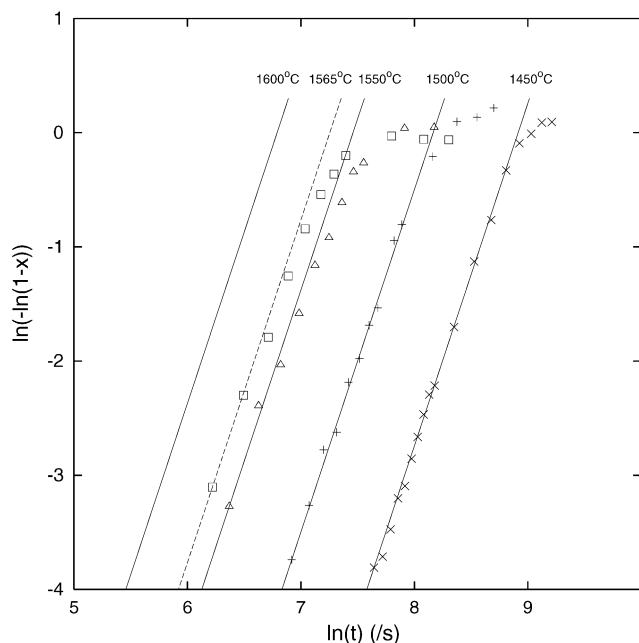


Fig. 2. The function  $\ln[-\ln(1-f)]$  vs.  $\ln t$  at different temperatures. The straight line at each temperature is drawn according to the fitted values of  $k_0$  and  $E$ . The symbol corresponding to each temperature is: ( $\times$ ) 1450 °C, (+) 1500 °C, ( $\Delta$ ) 1550 °C and ( $\square$ ) 1600 °C.

Recalling that the reaction of  $\text{TiC}_x$ ,  $\text{Ti}_5\text{Si}_3\text{C}_x$  and free C to form  $\text{Ti}_3\text{SiC}_2$  proceeds in the solid state, the reaction kinetics presented here relate to the precipitation and growth of  $\text{Ti}_3\text{SiC}_2$  crystals. From the plots in Figs. 2 and 3, it can also be noted that the linear Avrami relation between  $\ln(-\ln(1-f))$

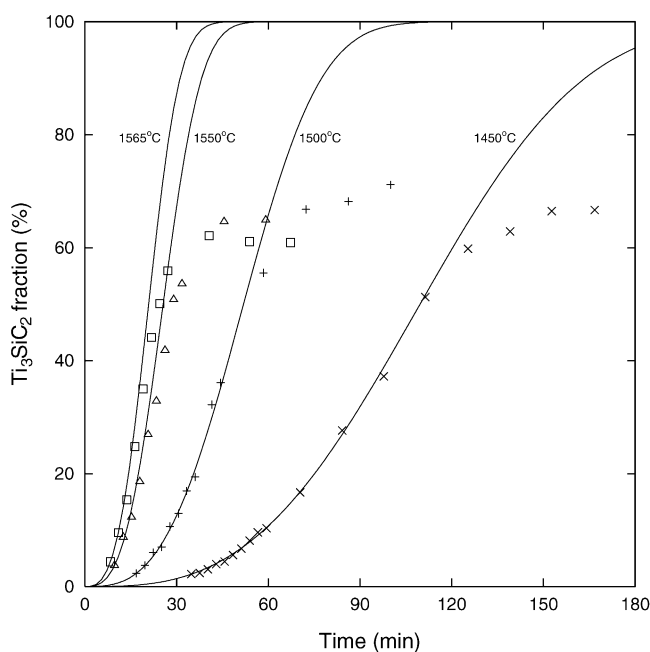


Fig. 3. The fraction of  $\text{Ti}_3\text{SiC}_2$  vs. the total reaction time at various temperatures. The line at each temperature is fitted according to the MAJ equation. The symbols are the same as in Fig. 2.

and  $\ln t$  is actually only properly held for the early stages of the crystal growth process, where the Avrami exponent  $n$  can be calculated as  $\sim 3$ . During the later stages of the crystallization, when the fraction of  $\text{Ti}_3\text{SiC}_2$ ,  $f$ , exceeds  $\sim 0.5$  (i.e.  $\ln(-\ln(1-f)) \sim -0.37$ ), the plots start to deviate from the linear relation as shown in Fig. 2, and the Avrami exponent  $n$  changes to about 1, and further to about 0, i.e. growth ceases altogether. The Avrami exponent  $n$  is a characteristic parameter linked to the morphology of the crystallization process,<sup>26</sup> and a change in the Avrami exponent during the growth of the new phase indicates a change in the mechanism of crystal growth. According to the MAJ theory,<sup>27,28</sup> a value of 3 for the Avrami exponent corresponds to a bulk crystallization process involving either two-dimensional growth with constant nucleation rate, or three-dimensional growth of a constant number of nuclei. In contrast, a value close to 1 corresponds to a predominantly one dimensional crystal growth process. These observations suggest that, after an initial stage of relatively unrestricted growth, there is a mechanism change or other shift in the crystal growth process. Anisotropic crystal growth on different planes is likely to be the predominant factor in this case. It has been demonstrated (see, for example, Fig. 24 of reference<sup>29</sup>) that crystals of  $\text{Ti}_3\text{SiC}_2$  are always anisotropic, forming sheet or disk shaped grains, the orientation of which corresponds to the basal planes of the hexagonal crystal structure of  $\text{Ti}_3\text{SiC}_2$ , i.e. the  $\text{Ti}_3\text{SiC}_2$  crystals grows preferentially in the  $a$ - $b$  plane and far slower along the  $c$ -axis. During the early stages of growth, the  $\text{Ti}_3\text{SiC}_2$  crystals are surrounded by a matrix of intermediate phases  $\text{TiC}_x$  and  $\text{Ti}_5\text{Si}_3\text{C}_x$  which are gradually separated by the new phase into isolated regions. However, as the  $\text{Ti}_3\text{SiC}_2$  crystals grow larger they intersect each other and cease growing laterally. In the latter stages of the reaction (i.e.  $f > 0.5$ ), they will have formed a three-dimensional framework, leaving only basal plane faces available for additional growth. The remaining intermediate phases then continue to react and deposit layers on the basal planes of the pre-existing  $\text{Ti}_3\text{SiC}_2$  by a much slower one-dimensional crystal growth mechanism.

Incompleteness of reaction between intermediate phases was a common feature of early attempts at bulk  $\text{Ti}_3\text{SiC}_2$  synthesis and was also the case in these experiments (Fig. 3). The growth sequence outlined above may give some insight into the cessation (or extreme slowing) of the reaction. If some of the remaining intermediate phases are completely segregated (i.e.  $\text{TiC}_x$  or  $\text{Ti}_5\text{Si}_3\text{C}_x$  only) due to isolation of the regions by the growing  $\text{Ti}_3\text{SiC}_2$  crystals, they would be unable to react except by long-range diffusion of C and/or Si through the  $\text{Ti}_3\text{SiC}_2$  crystals. Another contributing factor to incomplete reaction may have been evaporative loss of Si due to the use of a vacuum furnace.

In our previous in situ neutron diffraction study of the sintering of 3Ti/SiC/C mixtures using constant wavelength (CW) neutrons<sup>16</sup> a weak diffraction peak from  $\text{Ti}_3\text{SiC}_2$  was detected between 2 and 4 h of heating at 1200 °C. However, in the current TOF experiment no  $\text{Ti}_3\text{SiC}_2$  peak was found in



the diffraction patterns for 3Ti/SiC/C samples held at temperatures between 1200 and 1320 °C for 2 h and 10 min. Based on the kinetic information derived from the current measurements, the reaction rate  $K$  for the formation of  $\text{Ti}_3\text{SiC}_2$  at 1200 °C would be  $\sim 1.5 \times 10^{-6} \text{ s}^{-1}$ , which is about an order of magnitude lower than the estimate ( $K(1200^\circ\text{C}) = (k \sim 2 \times 10^{-8})^{1/n} = 1.5 \times 10^{-5} \text{ s}^{-1}$ ) made from the analysis of a single diffraction peak in our previous CW neutron diffraction data.<sup>16</sup> However, in our CW measurement at 1200 °C for a prolonged holding time the Avrami exponent derived for the reaction is  $\sim 1.6$ , and those earlier data should be treated with caution as only one weak peak from two diffraction patterns were used to construct the figures. The possible involvement of other competing reactions, e.g.  $\text{Ti} + \text{SiC} \rightarrow \text{Ti}_5\text{Si}_3\text{C} + \text{TiC}_x$  at this lower temperature, and the difference of the sample environment (Ar gas for previous measurement, and vacuum in the TOF measurement) may have also played a role in the different behaviours of the samples at the same temperatures. This requires further investigation.

The value obtained for the reaction enthalpy (380 kJ/mol) is insensitive to the corrections made to the time scale and the upper temperature and so we have some confidence in it.

#### 4. Conclusion

The kinetics of the growth of  $\text{Ti}_3\text{SiC}_2$  crystals by solid state reaction of the intermediate phases  $\text{TiC}_x$ ,  $\text{Ti}_5\text{Si}_3\text{C}_x$  ( $x \leq 1$ ) and a small amount of free C, determined from quantitative analysis of in situ neutron diffraction data collected at different temperatures may be modelled by the by Mehl–Avrami–Johnson equation.

Based on fitting the data with the Avrami equation, the value for the activation energy is  $380 \pm 10 \text{ kJ/mol}$ , and the corresponding Avrami exponent is  $3.0 \pm 0.2$  for the initial stages of crystal growth. The Avrami exponent decreases to approximately 1 after more than 0.5–0.6 of the reaction has completed. This phenomenon suggests a change in the mechanism of  $\text{Ti}_3\text{SiC}_2$  crystal growth from three-dimensional to one-dimensional and indicates the importance of anisotropic crystal growth in the development of  $\text{Ti}_3\text{SiC}_2$  microstructures.

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