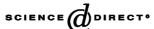


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# A new estimation method for the intrinsic thermal conductivity of nonmetallic compounds A case study for MgSiN<sub>2</sub>, AlN and β-Si<sub>3</sub>N<sub>4</sub> ceramics

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#### Abstract

A new method for estimating the maximum achievable thermal conductivity of non-electrically conducting materials is presented. The method is based on temperature dependent thermal diffusivity data using a linear extrapolation method enabling discrimination between phonon-phonon and phonon-defect scattering. The thermal conductivities estimated in this way for MgSiN<sub>2</sub>, AlN and  $\beta$ -Si<sub>3</sub>N<sub>4</sub> ceramics at 300 K equal 28, 200 and 105 W m<sup>-1</sup> K<sup>-1</sup>, respectively in favourable agreement with the highest experimental values of 23, 266 and 106–122 W m<sup>-1</sup> K<sup>-1</sup>. This suggests the general applicability of the proposed estimation method for non-metallic compounds. It is expected that when optic phonons contribute to the heat conduction (as is the case for AlN) the intrinsic thermal conductivity at lower temperatures (e.g. 300 K) is underestimated. However, the reliability and accuracy of the presented 'easy to use' estimation method seems to be much better than several other estimation methods. Furthermore the needed input for this method can provide information about which processing parameters should be optimised to obtain the highest thermal conductivity.

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Keywords: Thermal properties; Thermal conductivity; Nitrides; Substrates; Theoretical estimate; MgSiN<sub>2</sub>; AlN; Si<sub>3</sub>N<sub>4</sub>

# 1. Introduction

Several ceramic materials have been investigated intensively for substrate applications because of their potentially high thermal conductivity in combination with a high electrical resistivity. AlN especially has drawn a lot of attention  $^{2-4}$ , but recently also the nitride materials  $\beta\text{-Si}_3N_4^{5-7}$  and  $MgSiN_2^{8,9}$  have been considered to be potentially interesting. To estimate the intrinsic thermal conductivity one often uses Slack's equation for non-metallic materials  $^{10}$ . During our work on  $MgSiN_2$  we concluded that his theoretical approximation only provides a rough indication of the maximum achievable thermal conductivity, and that a more reliable and simpler estimation method would be useful.

Another (experimental) method to estimate the maximum achievable thermal conductivity is based on linear extrapolation of the measured inverse thermal conductivity (thermal resistivity)<sup>11</sup> versus the absolute temperature. Usually, it is assumed that the slope is determined by the lattice characteristics (intrinsic properties) and the intercept at 0 K by defects (impurities, grain boundaries, etc.)<sup>11–13</sup>. It will be shown that this last assumption is only partially correct, making this method not generally applicable. However, by combining some of the concepts of both approaches a new estimation method for the intrinsic thermal conductivity for non-metallic compounds was developed.

In this paper we will show that an estimation of the maximum achievable thermal conductivity of non-metallic crystals (i.e. heat transport takes place by lattice vibrations), based on temperature dependent thermal diffusivity data, gives not only more accurate information, but is also applicable over a wider temperature range. The method is applied to experimental data obtained in our own group for MgSiN $_2^{14}$  and to a large amount of data for AlN and  $\beta\text{-Si}_3\text{N}_4$  obtained from the literature.

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# 2. The temperature dependence of the thermal diffusivity and conductivity

The thermal conductivity ( $\kappa$  [W m<sup>-1</sup> K<sup>-1</sup>]) of a material can be calculated using:<sup>15</sup>

$$\kappa = a\rho_{\rm m}C_{\rm V} \tag{1}$$

in which a [m<sup>2</sup> s<sup>-1</sup>] is the thermal diffusivity,  $\rho_{\rm m}$  [mol m<sup>-3</sup>] the molar density and  $C_{\rm V}$  [J mol<sup>-1</sup> K<sup>-1</sup>] the heat capacity at constant volume. The density is only a weak function of temperature, so the temperature dependence of the thermal conductivity is determined by that of the thermal diffusivity and the heat capacity.

For a phonon conductor (i.e. heat transport predominantly takes place by lattice vibrations) the thermal diffusivity a equals:  $^{15,16-18}$ 

$$a = \frac{1}{3} v_{\rm s} l_{\rm tot} \tag{2}$$

in which  $v_s$  [m s<sup>-1</sup>] is the average phonon velocity (i.e. essentially the velocity of sound) and  $l_{tot}$  [m] the total mean free path of the phonons. The average phonon velocity  $v_s$  is almost temperature independent<sup>19</sup>, so that  $a \sim l_{tot}$ . If secondary phases are not taken into account then the total phonon mean free path is determined by the lattice characteristics (intrinsic properties) as well as defects and grain boundaries present in the material (extrinsic properties), and can be written as a summation of resistivities  $^{11,20-22}$ :

$$\frac{1}{l_{\text{tot}}} = \frac{1}{l_{\text{pp}}} + \frac{1}{l_{\text{pd}}} + \frac{1}{l_{\text{gb}}} + \sum_{x} \frac{1}{l_{x}}$$
 (3)

in which  $l_{\rm pp}$  [m] is the mean free path due to thermal phonon-phonon scattering,  $l_{\rm pd}$  [m] is the mean free path due to phonon-defect scattering (vacancies, impurities, isotopes),  $l_{\rm gb}$  [m] is the mean free path due to phonon-grain boundary scattering and  $l_x$  [m] the mean free path due to other scattering mechanisms induced by e.g. stacking faults, dislocations, etc.

For the temperature dependence of the phonon mean free path due to thermal phonon-phonon scattering,  $l_{\rm pp}$ , of pure crystalline materials it is known that approximately  $^{16,23}$ :

$$l_{\rm pp} = l_0 \left[ \exp\left(\frac{\tilde{\theta}}{bT}\right) - 1 \right] \quad \text{with} \quad \tilde{\theta} = \frac{\theta}{n^{1/3}}$$
 (4)

in which  $l_0$  [m] is a pre-exponential factor,  $\theta$  [K] a characteristic temperature (the so-called reduced Debye temperature) below which Umklapp processes start to disappear<sup>10,24</sup>, b is a constant  $\approx 2^{16,17,23,25}$ , T [K] is the absolute temperature,  $\theta$  [K] is the Debye temperature and n is the number of atoms per primitive unit cell.

For most materials only the first three terms of Eq. (3) are considered to be of importance  $^{11,21,26}$ . However, for the present discussion it is sufficient to assume that  $l_x$  is temperature independent. The temperature dependence of phonon-defect scattering  $l_{\rm pd}$  has been studied by Klemens  $^{20,27}$  and

Ambegaokar<sup>28</sup>. It was shown that this term is (almost) temperature independent for low defect concentrations. The phonon-grain boundary scattering term  $l_{\rm gb}$  is also temperature independent if the influence of the thermal expansion is neglected. So, the temperature dependence of  $l_{\rm tot}$  is dominated by the  $l_{\rm pp}$  term, whereas the other terms can be assumed to be temperature independent to a first approximation<sup>11,20,29</sup>. This implies that in general at low temperature  $l_{\rm tot}$  is determined by temperature independent extrinsic scattering processes (at defects and grain boundaries), whereas at high temperatures it is dominated by the temperature dependent intrinsic phonon-phonon scattering process.

If the temperature is sufficiently high  $(T > \tilde{\theta}/b)$  we can write (including all the above mentioned phonon scattering mechanisms) for the inverse of the thermal diffusivity approximately:

$$\frac{1}{a} \sim \frac{1}{l_{\text{lot}}} \sim \frac{A}{\left[\exp(\tilde{\theta}/bT) - 1\right]} + B$$

$$= \left(\frac{bT}{\tilde{\theta}}\right) A \left[1 - \frac{1}{2}\left(\frac{\tilde{\theta}}{bT}\right) + \frac{1}{12}\left(\frac{\tilde{\theta}}{bT}\right)^2 + \cdots\right]$$

$$+ B \approx A \left[\left(\frac{bT}{\tilde{\theta}}\right) - \frac{1}{2}\right] + B = \left(\frac{bA}{\tilde{\theta}}\right) T + \left(B - \frac{1}{2}A\right)$$
(5)

The constant A in Eq. (5) is related to the temperature dependent phonon-phonon scattering processes (intrinsic lattice diffusivity) and B to the temperature independent phonon scattering processes (impurities, defects, grain boundaries, etc.). It is obvious that Eq. (5) shows a linear relation between  $a^{-1}$  and T:

$$a^{-1} = A'T + B' \quad \left( \text{for } T > \frac{\tilde{\theta}}{b} \right)$$
 (6)

in which the slope  $A' = bA/\tilde{\theta}$  [m<sup>-2</sup> s K<sup>-1</sup>] is determined by the intrinsic lattice characteristics, and the intercept B' = B - 1/2 A [m<sup>-2</sup> s] by the impurities and microstructure as well as the intrinsic lattice characteristics (A). From Eq. (6) it can be concluded that for pure defect free materials (B = 0) a plot of the inverse of the thermal diffusivity versus the absolute temperature for measurements at  $T > \tilde{\theta}/b$  extrapolated to 0 K, should result in a straight line with (negative) intercept -1/2A and which intercepts the temperature axis at  $T = 1/2A/A' = \tilde{\theta}/2b$ .

If the temperature is sufficiently high so that the heat capacity is temperature independent  $(T > \theta^{30})$  then  $\kappa \sim a$   $(\sim l_{\rm tot})$  and the well known linear relation for the thermal resistivity  $\kappa^{-1}$  results<sup>11–13</sup>:

$$\kappa^{-1} = A''T + B'' \quad \text{(for } T > \theta) \tag{7}$$

This equation is often interpreted as being A'' ( $\sim bA/\tilde{\theta}$ ) determined by the intrinsic lattice diffusivity, which is correct, and the intercept value B'' ( $\sim (B-1/2A)$ ) as being only

determined by the microstructure and impurities, which is incorrect. This results in the erroneous conclusion that for a pure defect free single crystalline material (for  $T > \theta$ ) the thermal resistivity ( $\kappa^{-1}$ ) versus the absolute temperature plot gives a straight line through the origin<sup>5,12,13,31</sup> as B = 0 instead of B'' = 0.

It is noted that at very high temperatures, where the phonon mean free path is limited by the inter-atomic distances, Eqs. (5) and (6) are no longer valid<sup>32</sup> because they predict a decrease of the phonon mean free path to zero. For most materials n > 1 so that  $\tilde{\theta} < \theta$ . Considering the above discussion it is clear that the linear temperature dependence for the inverse thermal diffusivity  $a^{-1}$  can be observed at much lower temperatures  $(T > \tilde{\theta}/b)$  than for the thermal resistivity  $\kappa^{-1}$  as for  $T < \theta$  the heat capacity is temperature dependent. Furthermore the thermal diffusivity is directly related to the total phonon mean free path, which has to be maximised in order to optimise the thermal conductivity. So for identifying the dominant scattering mechanisms it is much more interesting to study the temperature dependence of the thermal diffusivity rather than that of the thermal conductivity.

Therefore, temperature dependent thermal diffusivity measurements when performed in a suitable temperature region  $(\tilde{\theta}/b(=\theta/bn^{1/3}) \leq T)$  can be a powerful tool in understanding and optimising the thermal conductivity of promising materials.

# 3. Experimental

For MgSiN<sub>2</sub> the thermal diffusivity a as a function of the temperature T (300–900 K) was measured on small ceramic samples ( $\varnothing$  11 mm  $\times$  1 mm) cut from several large, fully dense ceramic pellets processed under different conditions (for details see Refs. 33–35) using the photo/laser flash method<sup>36</sup> (laser flash equipment, Compotherm Messtech-

nik GmbH). By carefully grinding and polishing, samples with a uniform thickness and a low roughness were obtained. Samples varying in microstructure, oxygen content and processed with and without additive were investigated (Table 1). The accuracy of the measurement was estimated to be within 5%. Some samples were coated with a thin layer of gold and/or carbon before measuring the thermal diffusivity. The thin gold layer prevents direct transmission of the laser beam and aids the energy transfer to the sample. Carbon was used to increase the absorptivity of the front surface, and the emissivity of the back surface. These additional layers reduce the measured thermal diffusivity only slightly. A gold layer is always coated with a carbon layer because the gold layer reflects the laser flash. The radiative heat losses were minimised by measuring the samples in vacuum. The molar density  $\rho_{\rm m}$  and heat capacity at constant volume  $C_V$  required for calculating the thermal conductivity were obtained from our previous work (density<sup>37</sup> and heat capacity<sup>37,38</sup> assuming that  $C_V = C_P$ , resulting in a maximum relative error of approximately 10%<sup>39</sup>).

For AlN and  $\rm Si_3N_4$  many temperature dependent thermal diffusivity or conductivity data are reported in literature. Several AlN<sup>4,31,40–46</sup> and  $\rm Si_3N_4^{6,47–51}$  ceramics, with different processing conditions and thermal properties, were evaluated (see Tables 2 and 3). When necessary, the thermal diffusivity as a function of the temperature was calculated from the temperature dependence of the thermal conductivity, the density and heat capacity reported in the literature<sup>37</sup>.

# 4. Results for MgSiN<sub>2</sub>, AlN and β-Si<sub>3</sub>N<sub>4</sub>

4.1. The temperature dependence of the thermal diffusivity a

As expected, the thermal diffusivity for the MgSiN<sub>2</sub> samples processed in different ways decreases for higher

Table 1
Preparation characteristics, slope and intercept values (with *R*-value and intercept with the *T*-axis) of linearly fitted inverse thermal diffusivity ( $a^{-1}$ ) vs. the absolute temperature (T), and measured room temperature (T), thermal conductivity T00 for several MgSiN<sub>2</sub> ceramic samples processed in different ways<sup>33</sup>

Sample	Densification method and reaction conditions	Additives	Oxygen content (wt.%)	Grain size (µm)	Slope $A'$ (m <sup>-2</sup> s K <sup>-1</sup> )	Intercept B' (m <sup>-2</sup> s)	<i>R</i> -value	Intercept T-axis (K)	(W m <sup>-1</sup> K <sup>-1</sup> )
RB02	Hot-pressing: 1823 K, N <sub>2</sub> , 75 MPa, 2 h	None	3.8	-	$424.6 \pm 7.5$	$5.3 \pm 4.6 \times 10^3$	0.9992	_	19
RB11	Hot-pressing: 1823 K, N <sub>2</sub> , 75 MPa, 2 h	None	1.8	-	$409.8 \pm 8.0$	$27.7 \pm 4.9 \times 10^3$	0.9990	-	16
RB13	Reaction hot-pressing: 1873 K, N <sub>2</sub> , 75 MPa, 2 h	None	1.0	~0.5	$411.8 \pm 9.5$	$4.0 \pm 5.8 \times 10^3$	0.9987	_	20
RB32	Reaction hot-pressing: 1873 K, N <sub>2</sub> , 75 MPa, 2 h	4.2 wt.% Mg <sub>3</sub> N <sub>2</sub>	1.0	-	$394.5 \pm 6.6$	$-1.7 \pm 4.0 \times 10^3$	0.9993	4	21
RB34	Reaction hot-pressing: 1973 K, N <sub>2</sub> , 75 MPa, 2 h	None	1.0	~1.5	$402.8 \pm 4.4$	$-13.6 \pm 2.7 \times 10^3$	0.9997	34	23
RB37	Reaction hot-pressing: 1873 K, N <sub>2</sub> , 75 MPa, 2 h	6.0 wt.% Y <sub>2</sub> O <sub>3</sub>	_	_	$437.2 \pm 5.1$	$-19.7 \pm 3.1 \times 10^3$	0.9997	45	22
Mean	_	_	_	_	$413.5 \pm 14.0$	_	_	_	_

Table 2
Preparation characteristics as reported in the literature, slope and intercept values (with *R*-value and intercept with the *T*-axis) of linearly fitted inverse thermal diffusivity ( $a^{-1}$ ) vs. the absolute temperature (T), and measured room temperature (T) and measured room temperature (T) of several AlN ceramic samples processed in different ways

Sample	Ref.	Densification method and reaction conditions	Additives	Slope $A'$ (m <sup>-2</sup> s K <sup>-1</sup> )	Intercept $B'$ (m <sup>-2</sup> s)	Intercept <i>T</i> -axis (K)	$({ m W}{ m m}^{-1}{ m K}^{-1})$
Single crystal W-201	40,61	Sublimation-recondensation: 2523 K, 95% N <sub>2</sub> /5% H <sub>2</sub>	None	$100.0 \pm 1.0$	$-22.79 \pm 0.86 \times 10^3$	228	285
Shapal	41,62	Not reported		$83.5 \pm 1.5$	$-8.08 \pm 1.10 \times 10^{3}$	97	141
AlN without additive	4	Hot-pressing: 2123 K, 10 min Annealing: 2123 K, 100 min	None	$104.8 \pm 3.0$	$3.38 \pm 1.75 \times 10^3$	_	70
BP research AlN	31,62	Not reported		$81.6 \pm 1.0$	$-14.33 \pm 0.45 \times 10^3$	176	228
Shapal SH-04	31,62	Not reported		$85.6 \pm 1.6$	$-11.66 \pm 0.77 \times 10^3$	136	167
Shapal SH-15		-		$91.9 \pm 1.5$	$-14.62 \pm 0.77 \times 10^3$	159	144
Super Shapal				$84.4 \pm 1.9$	$-14.79 \pm 0.94 \times 10^3$	175	212
Toshiba TAN-170	31,62	Not reported		$85.0 \pm 1.5$	$-11.69 \pm 0.69 \times 10^3$	138	170
Carborundum AlN	31,62	Not reported		$82.4 \pm 1.1$	$-13.81 \pm 0.51 \times 10^3$	168	212
AlN	42	Pressureless sintering: 2023 K, N <sub>2</sub> , 10 h	4 wt.% Y <sub>2</sub> O <sub>3</sub>	$89.3 \pm 9.0$	$-16.11 \pm 4.21 \times 10^3$	180	208
$B(N_2)$	43	Pressureless sintering: 2133 K, N <sub>2</sub> , 1 h	1 wt.% Y <sub>2</sub> O <sub>3</sub>	$87.0 \pm 1.9$	$-4.72 \pm 1.05 \times 10^3$	54	119
$H(N_2)$			3 wt.% Y <sub>2</sub> O <sub>3</sub>	$91.6 \pm 2.4$	$-13.41 \pm 1.35 \times 10^3$	146	159
$G(N_2)$			$10 \text{ wt.}\% \text{ Y}_2\text{O}_3$	$94.3 \pm 1.1$	$-12.74 \pm 0.58 \times 10^3$	135	148
C1	43,44	Pressureless sintering: 2098 K, N <sub>2</sub> , 1 h	$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 0 \text{ wt.}\% \text{ CaO}$	$89.2 \pm 1.0$	$-10.50 \pm 0.56 \times 10^3$	118	144
I1	43	<del>-</del>	$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 1 \text{ wt.}\% \text{ CaO}$	$91.5 \pm 0.5$	$-9.11 \pm 0.30 \times 10^3$	100	129
B1	43,44		$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 2 \text{ wt.}\% \text{ CaO}$	$100.0 \pm 1.0$	$-10.97 \pm 0.52 \times 10^3$	110	124
$H(N_2)$	43,45	Pressureless sintering: 2133 K, N <sub>2</sub> , 1 h	$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 0 \text{ wt.}\% \text{ SiO}_2$	$91.6 \pm 2.4$	$-13.41 \pm 1.35 \times 10^3$	146	159
$N(N_2)$	43		$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 0.3 \text{ wt.}\% \text{ SiO}_2$	$88.5 \pm 0.6$	$-8.19 \pm 0.32 \times 10^3$	93	129
$O(N_2)$	43,45		$3 \text{ wt.} \% \text{ Y}_2\text{O}_3 + 1 \text{ wt.} \% \text{ SiO}_2$	$96.0 \pm 1.5$	$-6.62 \pm 0.83 \times 10^3$	69	106
$Q(N_2)$	43,45		$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 2 \text{ wt.}\% \text{ SiO}_2$	$148.9 \pm 5.3$	$9.10 \pm 2.93 \times 10^3$	_	46
$S(N_2)$	43,45		$3 \text{ wt.}\% \text{ Y}_2\text{O}_3 + 5 \text{ wt.}\% \text{ SiO}_2$	$200.4 \pm 11.4$	$45.83 \pm 6.30 \times 10^3$	_	24

Table 3
Preparation characteristics and resulting β-fraction as reported in the literature, slope and intercept values (with *R*-value and intercept with the *T*-axis) of linearly fitted inverse thermal diffusivity  $(a^{-1})$  vs. the absolute temperature (T), and measured room temperature (T) and measured room temperature (T) and measured room temperature (T).

Sample		Densification method and reaction conditions	Additives	β-Fraction (%)	Slope $A'$ (m <sup>-2</sup> s K <sup>-1</sup> )	Intercept $B'$ (m <sup>-2</sup> s)	Intercept T-axis (K)	$\kappa_{300}$ (W m <sup>-1</sup> K <sup>-1</sup> )
SN5	50	Gas-pressure sintered: 2473 K, 30 MPa (N <sub>2</sub> ), 4 h	$0.5  \text{mol}\%    \text{Y}_2 \text{O}_3  + 0.5  \text{mol}\%    \text{Nd}_2 \text{O}_3$	100	129.1 ± 2.9	$-22.84 \pm 3.14 \times 10^3$	177	122
	51	HIPped: 2673 K, 200 MPa (N <sub>2</sub> ), 2 h	3.5 wt.% Y <sub>2</sub> O <sub>3</sub>	100	98.9	$-10.27 \times 10^3$	104	107
A	47	High pressure hot-pressing: 2173 K, 3 GPa, 1 h	None	100	$125.7 \pm 6.3$	$42.57 \pm 4.49 \times 10^3$	-	30
В			4 wt.% MgO	100	$143.6 \pm 5.1$	$38.46 \pm 3.51 \times 10^3$	_	29
D			4 wt.% Al <sub>2</sub> O <sub>3</sub>	100	$251.3 \pm 19.3$	$106.38 \pm 13.67 \times 10^{3}$	_	14
С		High pressure hot-pressing: 2073 K, 3 GPa, 1 h	4 wt.% Y <sub>2</sub> O <sub>3</sub>	100	$159.0 \pm 9.5$	$64.24 \pm 6.71 \times 10^3$	-	22
	48	Capsule-HIPped: 1973 K, 60 MPa (Ar), 1 h	$3mol\%\ Y_2O_3\ +3mol\%\ Al_2O_3$	~25	$210.6 \pm 4.3$	$20.36 \pm 3.18 \times 10^3$	-	28
0			$2 \text{ mol}\% \text{ Y}_2\text{O}_3 + 4 \text{ mol}\% \text{ Al}_2\text{O}_3$	~34	$199.8 \pm 6.6$	$31.35 \pm 4.82 \times 10^3$	_	26
<b>A</b>			$4 \text{ mol}\% \text{ Y}_2\text{O}_3 + 2 \text{ mol}\% \text{ Al}_2\text{O}_3$	~67	$146.2 \pm 5.4$	$48.01 \pm 3.91 \times 10^3$	_	24
-100	48	Capsule-HIPped: 2023 K, 60 MPa (Ar), 1 h	$3 \text{ mol}\% \text{ Y}_2\text{O}_3 + 3 \text{ mol}\% \text{ Al}_2\text{O}_3$	100	$143.5 \pm 4.4$	$38.24 \pm 4.02 \times 10^3$	-	28
<b>-</b> 90		Capsule-HIPped: 1973 K, 60 MPa (Ar), 1 h	$3mol\%\ Y_2O_3\ +3mol\%\ Al_2O_3$	~90	$143.8 \pm 6.6$	$53.44 \pm 4.82 \times 10^3$	-	22
- 34		Capsule-HIPped: 1823 K, 60 MPa (Ar), 1 h	$3mol\%\ Y_2O_3\ +3mol\%\ Al_2O_3$	~34	$169.2 \pm 10.4$	$83.86 \pm 7.56 \times 10^3$	-	16
+ 6/0	48	Capsule-HIPped: 2023 K, 60 MPa (Ar), 1 h	$6mol\%\ Y_2O_3\ + 0mol\%\ Al_2O_3$	100	$112.1 \pm 1.3$	$-3.77 \pm 1.20 \times 10^3$	34	73
+ 5/1			$5 \text{ mol}\% \text{ Y}_2\text{O}_3 + 1 \text{ mol}\% \text{ Al}_2\text{O}_3$	100	$116.0 \pm 1.2$	$6.40 \pm 1.10 \times 10^3$	_	53
+ 4/2			$4 \text{ mol}\% Y_2O_3 + 2 \text{ mol}\% Al_2O_3$	100	$127.7 \pm 3.6$	$26.94 \pm 3.30 \times 10^{3}$	_	35
+ 3/3			$3 \text{ mol}\% \text{ Y}_2\text{O}_3 + 3 \text{ mol}\% \text{ Al}_2\text{O}_3$	100	$143.5 \pm 4.4$	$38.24 \pm 4.02 \times 10^3$	_	28
+ 2/4			$2 \text{ mol}\% Y_2O_3 + 4 \text{ mol}\% Al_2O_3$	100	$150.9 \pm 4.7$	$50.57 \pm 4.34 \times 10^3$	_	23
+ 1/5			$1 \text{ mol}\% Y_2O_3 + 5 \text{ mol}\% Al_2O_3$	100	$137.5 \pm 7.4$	$67.91 \pm 6.71 \times 10^3$	_	21
+ 0/6			$0  \text{mol}\%   Y_2 O_3  + 6  \text{mol}\%   Al_2 O_3$	100	$146.2 \pm 6.1$	$92.43 \pm 5.53 \times 10^3$	_	17
Tape cast	6	Hot-pressed: 2073 K, 40 MPa, 2 h and subsequently HIPped: 2773 K, 200 MPa (N <sub>2</sub> ), 2 h	5 wt.% $Y_2O_3 + 5$ vol.% rod-like $\beta\text{-Si}_3N_4$ seeds	-	84.5 ± 2.1	$-8.96 \pm 1.52 \times 10^3$	106	155
					$187.0 \pm 4.8$	$-22.29 \pm 3.10 \times 10^{3}$	119	70

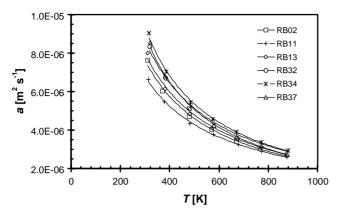


Fig. 1. The thermal diffusivity (a) plotted vs. the absolute temperature (T) for several MgSiN<sub>2</sub> samples (see Table 1).

temperatures (Fig. 1). The same is true for the AIN (Table 2) and  $Si_3N_4$  (Table 3). For all three materials the observed thermal conductivity at 300 K varied over a relatively broad range (MgSiN<sub>2</sub>: 16–23 W m<sup>-1</sup> K<sup>-1</sup> (Table 1); AIN: 24–285 W m<sup>-1</sup> K<sup>-1</sup> (Table 2);  $\beta$ -Si<sub>3</sub>N<sub>4</sub>: 14–122 W m<sup>-1</sup> K<sup>-1</sup> (Table 3)), indicating large differences in impurity content and microstructure for the different samples. The difference in thermal diffusivity between the samples is less pronounced at higher temperatures (see e.g. Fig. 1) as then intrinsic phonon scattering processes are dominating the thermal diffusivity (so A'T > B').

# 4.2. Inverse thermal diffusivity $a^{-1}$ versus temperature T plots

As expected from theory (see Section 2), for all three compounds a linear fit of the inverse of the thermal diffusivity plotted against the absolute temperature (Figs. 2–8) resulted in a good description of the temperature dependence (typically R > 0.99) (Tables 1–3). The indicated uncertainties for the slope and the intercept correspond with the 95% confidence interval.

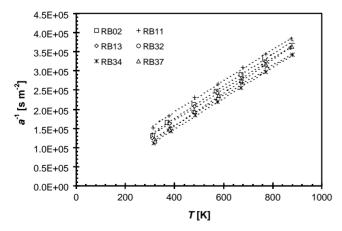


Fig. 2. The inverse thermal diffusivity  $(a^{-1})$  vs. the absolute temperature (T) plot for MgSiN<sub>2</sub> ceramic samples processed in different ways (see Table 1).

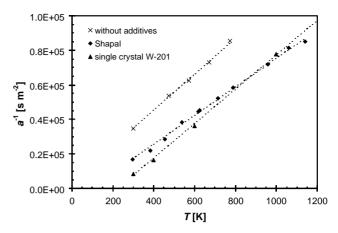


Fig. 3. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data for AlN samples without additive  $(\times)^4$ , a typical sample  $(\spadesuit)^{41,62}$  and a single crystal  $(\blacktriangle)^{40}$  (see Table 2).

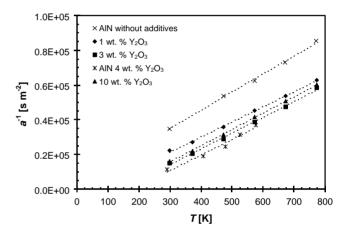


Fig. 4. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data for AlN ceramics, processed with different amounts of  $Y_2O_3$  as a sintering additive. Data obtained from 4 (without additives), 42 (4 wt.%  $Y_2O_3$ ) and 43 (1, 3 and 10 wt.%  $Y_2O_3$ ) (see Table 2).

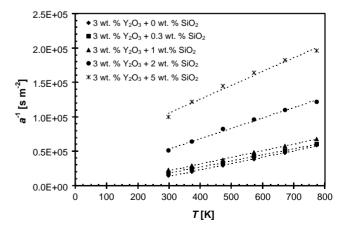


Fig. 5. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data<sup>43,45</sup> for AlN ceramics, processed with 3 wt.%  $Y_2O_3$  and different amounts of SiO<sub>2</sub> as sintering additives (see Table 2).

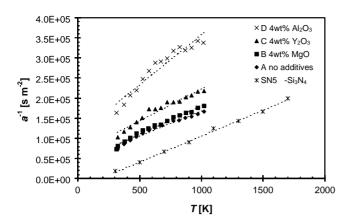


Fig. 6. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data for  $\beta$ -Si<sub>3</sub>N<sub>4</sub> ceramics processed in different ways. Data obtained from Ref. 47 (sample A–D) and Ref. 50 (sample SN5) (see Table 3).

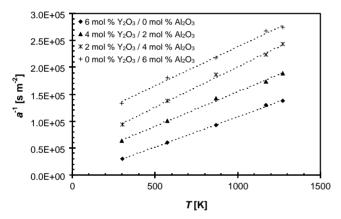


Fig. 7. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data<sup>48</sup> (see Table 3) for  $\beta$ -Si<sub>3</sub>N<sub>4</sub> ceramics using mixtures of Y<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> as sintering additives.

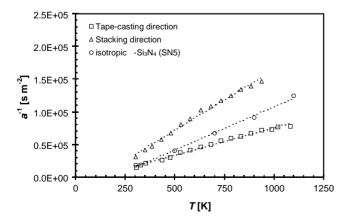


Fig. 8. The inverse thermal diffusivity  $(a^{-1})$  vs. temperature (T) plot as obtained from literature data for  $\beta$ -Si<sub>3</sub>N<sub>4</sub> ceramics along the casting and stacking direction as compared to an isotropic sample. Data obtained from<sup>6</sup> (casting and stacking direction) and<sup>50</sup> (sample SN5) (see Table 3).

#### 4.2.1. MgSiN<sub>2</sub>

For all MgSiN<sub>2</sub> samples about the same slope A' of 414  $\pm$  14 m<sup>-2</sup> s K<sup>-1</sup> is observed (Table 1 and Fig. 2) indicating that the lattice characteristics are not influenced by the processing conditions used. In contrast, the intercept B' shows a relatively large variation, as the samples differ in impurity content and grain size<sup>33</sup>. As expected, the samples with the highest purity and grain size have in general the lowest intercept values (Table 1).

#### 4.2.2. AlN

The AlN ceramics processed with several different additives have a typical slope value of  $80\text{--}90\,\text{m}^{-2}\,\text{s}\,\text{K}^{-1}$  (Table 2). These values are somewhat smaller than the value observed for the hot-pressed AlN sample without sintering additive ( $104.8 \pm 3.0\,\text{m}^{-2}\,\text{s}\,\text{K}^{-1}$ ). This difference can be ascribed to the presence of oxygen containing secondary phases. Also for the best heat-conducting sample (single crystal W- $201^{40}$ ) a somewhat larger slope is observed ( $100.0 \pm 1.0\,\text{m}^{-2}\,\text{s}\,\text{K}^{-1}$ ) as compared to the typical value (Fig. 3). However, this observation may be related to the fact that this sample is a single crystal for which the thermal conductivity was determined along the c-axis.

The slope is not much influenced by the addition of small amounts of  $Y_2O_3$  ( $\leq 10$  wt.%) (Fig. 4) and CaO ( $\leq 2$  wt.% together with 3 wt.% Y<sub>2</sub>O<sub>3</sub> (Table 2)), whereas the slope changes drastically for larger amounts SiO2 addition  $(>2 \text{ wt.}\% \text{ together with } 3 \text{ wt.}\% \text{ } Y_2O_3) \text{ (Fig. 5)}$ . From these observations it can be concluded that Y2O3 and CaO additions mainly influence the defect chemistry and microstructure of the AlN ceramics (phonon-defect and phonon-grain boundary scattering), whereas SiO<sub>2</sub> addition also results in a change of the lattice characteristics (phonon-phonon scattering). In complete agreement with this conclusion for these samples, de Baranda et al. 45 reported that for an SiO<sub>2</sub> addition of 2 wt.% and above, together with a 3 wt.% Y<sub>2</sub>O<sub>3</sub> additive, sialon polytypoids with an AlN like structure are formed, resulting in the formation of a different lattice and thus a different slope value (Table 2 and Fig. 5).

For samples with the typical slope value of 80– $90 \,\mathrm{m}^{-2} \,\mathrm{s}$  K<sup>-1</sup>, the intercept value B' is the smallest for the (almost) defect free single crystal and largest for hot-pressed ceramics processed without additives containing many defects due to the oxygen impurities dissolved into the AlN lattice (Fig. 3 and Table 2). By suitable processing (Table 2: AlN<sup>42</sup>) the defect concentration in the AlN lattice is reduced resulting in a decrease of the intercept approaching the value for the (almost) defect free single crystal.

With increasing  $Y_2O_3$  addition the intercept value B' first decreases and subsequently increases again (Table 2 and Fig. 4) in agreement with other observations<sup>52,53</sup> that with increasing  $Y_2O_3$  addition the thermal conductivity first increases (till about 4–6 wt.% addition<sup>53</sup>) and subsequently decreases. This indicates that (as expected)  $Y_2O_3$  is an effective sintering aid for sintering of AlN by reducing the defect concentration (Al vacancies) in the AlN lattice. For

higher dopant levels the thermal conductivity decreases because the thermal conductivity of the formed yttrium aluminates (and  $Y_2O_3$ ) is much lower than that for  $AIN^{4,52}$ , resulting in some increase of the observed slope value too.

## 4.2.3. $\beta$ -Si<sub>3</sub>N<sub>4</sub>

The lowest slope value A' for the isotropic  $\beta\text{-}Si_3N_4$  samples equals  $100\text{--}130\,\text{m}^{-2}\,\text{s}\,\text{K}^{-1}$  (Table 3). The slope observed for the sample with the highest thermal diffusivity (SN5) equals  $129.1\pm2.9\,\text{m}^{-2}\,\text{s}\,\text{K}^{-1}$ . The addition of MgO and  $Y_2O_3$  has only a limited influence on the slope, whereas in contrast the addition of  $Al_2O_3$  has a strong effect (Fig. 6). The reason for this different behaviour is that the  $Al_2O_3$  addition can dissolve into the  $\beta\text{-}Si_3N_4$  lattice resulting in the formation of a  $\beta\text{-}sialon$  ( $Si_{6-z}Al_zO_zN_{8-z}$ ), whereas  $Y_2O_3$  and MgO can only react with  $SiO_2$  on the surface of the  $Si_3N_4$  grains to form a separate secondary phase. The relatively large scattering in the data points for the samples A–D, especially at higher temperatures (Fig. 6), can be partially ascribed to the inaccuracy introduced when obtaining the data from a plot of Ref. 47.

For a lower  $\beta$  content of the  $\alpha/\beta$ -Si<sub>3</sub>N<sub>4</sub> composite ceramics the observed slope increases (Table 3). This observation can be explained in view of the difference between the crystal structure of the  $\alpha$ - and  $\beta$ -modifications of Si<sub>3</sub>N<sub>4</sub>. As the  $\alpha$ -modification is more complex than the  $\beta$ -modification ( $\alpha$ -Si<sub>3</sub>N<sub>4</sub>: n=28;  $\beta$ -Si<sub>3</sub>N<sub>4</sub>: n=14) it is expected for  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> to have a higher value for the slope A' (assuming that b, A, and  $\theta$  are about the same for both modifications) and thus a lower intrinsic thermal conductivity than  $\beta$ -Si<sub>3</sub>N<sub>4</sub>.

A nice illustration of the influence of the type and amount of additive on the slope and intercept values can be obtained from the data of Watari et al. 48 who studied the influence of  $Y_2O_3$  and  $Al_2O_3$  additions totalling 6 mol% on the thermal conductivity of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> (Table 3 and Fig. 7). It can be concluded that  $Y_2O_3$  without  $Al_2O_3$  is an effective additive for increasing the thermal conductivity of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> because it does not dissolve in the lattice (slope  $A' \approx \text{constant} \approx 110 \,\text{m}^{-2} \,\text{s K}^{-1}$ ) and decreases the intercept B' (<0), whereas with increasing  $Al_2O_3$  content a sialon is formed resulting in a change of the lattice characteristics (increase of the slope A' due to lowering  $\theta$  as a consequence of Si–N  $\rightarrow$  Al–O replacement) and defect concentration (increase of the intercept B' due to Al on Si site and O on N site acting as scattering centres for phonons) (Fig. 7 and Table 3).

A problem in the comparison of the different samples is that they often show a considerable anisotropy; in particular all recently produced samples with conductivities >100 W m $^{-1}$  K $^{-1}$  have elongated grains. The anisotropy was clearly demonstrated by Li et al. using thermoreflectance microscopy to measure the conductivity inside individual grains $^{54}$ . They found conductivity-values of 69 W m $^{-1}$  K $^{-1}$  along the a-axis and 180 W m $^{-1}$  K $^{-1}$  along the c-axis. The consequences of anisotropy for the  $a^{-1}$  versus T plot are clearly visible in Fig. 8 for a tape-cast sample. This plot shows two different slope values, the one in the casting

direction (predominantly along c-axis) below the typically observed value and the one in the stacking direction (predominantly along a-axis) above the typically observed slope value (Table 3).

#### 5. Discussion

From the results of the  $a^{-1}$  versus T plots it is clear that these plots can be very useful for optimisation of the thermal diffusivity. The data of a material processed in different ways can be used to study the influence of different additives. Increase of the slope indicates that the additive dissolves into the lattice, whereas a decrease in slope or intercept indicates that the additive improves the thermal conductivity.

## 5.1. Interpretation of the fitting parameters

In general the observed slopes A' for the three materials have a typical constant value (MgSiN<sub>2</sub>: 400–430 m<sup>-2</sup> s K<sup>-1</sup> (Table 1); AlN:  $80-90 \,\mathrm{m}^{-2} \,\mathrm{s} \,\mathrm{K}^{-1}$  (Table 2); and  $\beta$ -Si<sub>3</sub>N<sub>4</sub>:  $100-130 \,\mathrm{m}^{-2}\,\mathrm{s}\,\mathrm{K}^{-1}$  (Table 3)) and deviations from this constant value can be explained in view of the lattice characteristics. For the samples with the same lattice characteristics (constant A') but with different impurity content and microstructure a relatively large variation in the intercept value B' can be observed. Considering the large variation in thermal conductivity observed for the samples with an approximately constant slope, it can be concluded that all phonon scattering processes, except the intrinsic phonon-phonon scattering, are indeed (almost) temperature independent. As expected from the theory, also negative intercept values are found. Furthermore AlN with the lowest slope value A' shows the highest reduced Debye temperature  $\tilde{\theta}_0$  (Table 4). This indicates that the presented theoretical concept has a sound basis.

# 5.2. Thermal conductivity estimates for MgSiN<sub>2</sub>, AlN and $\beta$ -Si<sub>3</sub>N<sub>4</sub>

In order to estimate the maximum achievable theoretical thermal diffusivity (B=0), besides the slope A' the intercept with the  $a^{-1}$ -axis or the T-axis should be known. For the present discussion the intercept with the T-axis was used as this value is only dependent on  $\tilde{\theta}$  and b.

## 5.2.1. Determination of $\theta$ and b

Assuming that the acoustic phonons are the major heat carriers, the high temperature limit of the Debye temperature based on the acoustic phonons  $\theta_{\infty}^{A}$  is needed<sup>10</sup> to evaluate the reduced Debye temperature  $\tilde{\theta}$ . Since  $\theta_{\infty}^{A}$  is often not available it is normally approximated by the Debye temperature evaluated from elastic constants or heat capacity data near  $0 \, \mathrm{K}^{10,30,55}$  resulting in  $\theta_{0}$ . Therefore  $\theta_{0}$  data for MgSiN<sub>2</sub>, AlN and Si<sub>3</sub>N<sub>4</sub><sup>55</sup> obtained from elastic constants

Table 4
The measured slope A' (=  $bA/\tilde{\theta}$ ), the Debye temperature  $\theta$ , the number of atoms per primitive unit cell n, the resulting reduced Debye temperature  $\tilde{\theta}$  (= $\theta/n^{1/3}$ ) and the calculated intercept (=  $\tilde{\theta}/2b$  with b=2) for MgSiN<sub>2</sub>, AlN and  $\beta$ -Si<sub>3</sub>N<sub>4</sub>

Material	Slope $A' \text{ (m}^{-2} \text{ s K}^{-1})$	θ (Κ)	n	$\tilde{\theta}$ (K)	Intercept (b=2) (K)
MgSiN <sub>2</sub> AlN	400–430 80–90	900 <sup>55</sup> 940 <sup>55</sup>	16 <sup>63</sup> 4 <sup>57</sup>	357 592	89 148
β-Si <sub>3</sub> N <sub>4</sub>	100–130	955 <sup>55</sup> 1156 <sup>56</sup>	14 <sup>64</sup>	396 480	99 120

Data from Ref. 55 are for  $\theta_0$ , data from Ref. 56 are for  $\theta^A$ .

were used to calculate  $\tilde{\theta}$  (Table 4). The number of atoms per primitive unit cell n can be obtained from crystallographic data (Table 4). This results in reduced Debye temperatures ( $\tilde{\theta}_0$ ) of 357, 592 and 396 K for MgSiN<sub>2</sub>, AlN and Si<sub>3</sub>N<sub>4</sub>, respectively. For Si<sub>3</sub>N<sub>4</sub> Morelli and Heremans<sup>56</sup> recently calculated  $\tilde{\theta}_{\infty}^A = 480$  K. As shown in Table 5, the use of  $\tilde{\theta}_0 = 396$  K instead of 480 K for Si<sub>3</sub>N<sub>4</sub> leads to a 10% lower conductivity at 300 K and only 3% at 600 K.

The value of b for describing the temperature dependence of the thermal diffusivity is not exactly known. Based on the simple Debye theory it can be argued that  $b = 2^{16,17,23,25}$ . However, b may differ somewhat from 2 and vary from substance to substance  $^{16}$ . Leibfried and Schlömann  $^{19}$  suggest that for a FCC lattice  $b = \sqrt{5/3} = 1.29$ . However, the scarce experimental results confirm the value of  $b \approx 2$  (2.3, 2.7 and 2.1 for solid helium, diamond and sapphire, respectively  $^{17}$ ). Taking b = 2 results in theoretically calculated intercepts of 89, 148 and 99 K for pure, defect free MgSiN<sub>2</sub>, AlN and Si<sub>3</sub>N<sub>4</sub> ceramics, respectively (Table 4).

# 5.2.2. Comparison between theoretical and experimental intercept with the T-axis

The theoretical intercept with the T-axis of MgSiN<sub>2</sub> is as expected higher than the experimentally observed value. However, for  $\beta$ -Si<sub>3</sub>N<sub>4</sub> and AlN, particularly for the anisotropic samples, this is not always the case. Moreover,

for AlN phonon dispersion curves indicate that also optic phonons contribute to the heat conduction resulting in an underestimation of the reduced Debye temperature<sup>57</sup>. When using the  $a^{-1}$  versus T method, both the slope A' and the (theoretical) intercept with the T-axis are related to  $\tilde{\theta}$ . However, especially at high temperatures the influence of  $\tilde{\theta}$  on the estimate is limited as  $a^{-1} = A'T + B' \approx A'T$  and A' is determined experimentally (see Table 5: 600 and 900 K estimates). This makes the estimates for the thermal diffusivity less sensitive for errors induced by not taking optic phonons fully into account.

## 5.2.3. Thermal conductivity estimates

Using the data in Table 4, together with available values of the density and heat capacity, we can estimate the intrinsic thermal conductivity (see Eq. (1)) at temperatures  $T \geq \tilde{\theta}/2$  ( $T \geq 179$ , 296 and 198 K for MgSiN<sub>2</sub>, AlN and  $\beta$ -Si<sub>3</sub>N<sub>4</sub>, respectively). Results at 300, 600 and 900 K are shown in Table 5, together with experimentally obtained values. For these calculations we used the lowest values of the slope since we want to estimate the maximum diffusivity. This is still a conservative estimate since the Debye temperature used in our calculation may be too low due to neglect of optical phonon contributions.

For MgSiN<sub>2</sub> ceramics the highest experimentally obtained thermal conductivity at 300 K (Table 5) does not

Table 5
The estimates for the maximum achievable thermal conductivity  $\kappa_{\text{the}}$  at 300, 600 and 900 K, using the data of Table 4 for MgSiN<sub>2</sub>, AlN and β-Si<sub>3</sub>N<sub>4</sub> together with the molar density  $\rho_{\text{m}}$  and heat capacity  $C_{\text{p}}$ , compared with corresponding highest experimentally observed thermal conductivity  $\kappa_{\text{exp}}$ 

300  K  MgSiN <sub>2</sub> 1.18 × 10 <sup>-5</sup> 3.90 × 10 <sup>4</sup> 61.7  AlN 8.22 × 10 <sup>-5</sup> 7.94 × 10 <sup>4</sup> 30.6  β-Si <sub>3</sub> N <sub>4</sub> 4.52 × 10 <sup>-5</sup> 2.29 × 10 <sup>4</sup> 90.6	28 200 94 105	23 246–266 107
AlN 8.22 × $10^{-5}$ 7.94 × $10^4$ 30.6 β-Si <sub>3</sub> N <sub>4</sub> 4.52 × $10^{-5}$ 2.29 × $10^4$ 90.6	200 94	246–266
$\beta$ -Si <sub>3</sub> N <sub>4</sub> 4.52 × 10 <sup>-5</sup> 2.29 × 10 <sup>4</sup> 90.6	94	
		107
	105	
$5.05 \times 10^{-5}$		
600 K		
$MgSiN_2$ 0.49 × 10 <sup>-5</sup> 3.88 × 10 <sup>4</sup> 88.1	17	15
AIN $2.77 \times 10^{-5}$ $7.91 \times 10^{4}$ 44.0	96	96
$\beta$ -Si <sub>3</sub> N <sub>4</sub> 1.81 × 10 <sup>-5</sup> 2.28 × 10 <sup>4</sup> 144.5	60	76
$1.89 \times 10^{-5}$	62	
900 K		
MgSiN <sub>2</sub> $0.31 \times 10^{-5}$ $3.86 \times 10^4$ 95.6	11	11
AlN $1.66 \times 10^{-5}$ $7.87 \times 10^4$ 47.7	62	55
$\beta$ -Si <sub>3</sub> N <sub>4</sub> 1.13 × 10 <sup>-5</sup> 2.27 × 10 <sup>4</sup> 157.0	40	45
$1.17 \times 10^{-5}$	42	

exceed 25 W m<sup>-1</sup> K<sup>-1</sup> despite the fact that already considerable effort has been made to improve the thermal conductivity<sup>9,33,34,55,58,59</sup>. As the predicted value of 28 W m<sup>-1</sup> K<sup>-1</sup> is close to this value, it can be concluded that the highest experimentally observed value is close to the intrinsic one. From Tables 1 and 5 and Fig. 2 it is obvious that a further reduction of the defect concentration in the MgSiN<sub>2</sub> lattice will not result in a significant increase of the thermal diffusivity, because for the best samples the intercept with the *T*-axis of 45 K (Table 1 and Fig. 2) is already very close to the theoretical value of 89 K (Table 4).

For AlN the highest experimental value for a ceramic sample is 266 W m<sup>-1</sup> K<sup>-160</sup>, higher than our estimate of about  $200 \,\mathrm{W}\,\mathrm{m}^{-1}\,\mathrm{K}^{-1}$ . A problem with the comparison of the experimental value is that optimisation of the microstructure leads to anisotropic grains and therefore higher values than can be expected from our calculations since we then underestimate the intercept with the T-axis (see Section 5.2.2). For the estimates at 600 and 900 K the agreement between estimated and experimental values improves as the exact value of the intercept with the T-axis is of less importance as  $a^{-1} = A'T + B' \approx A'T$  (at high temperature). The value of 319 W m<sup>-1</sup> K<sup>-1</sup> reported in Ref. 40 is based on extrapolation of the single crystal data obtained for the c-axis and therefore cannot be compared to our isotropic value. Our estimation also agrees better with the experimental data than the value calculated from the Slack formula (Table 6), which is more sensitive for errors in the reduced Debye temperature.

The estimates for  $\beta$ -Si<sub>3</sub>N<sub>4</sub> at 300, 600 and 900 K are close to the experimentally observed values (Table 5), but

as mentioned earlier room temperature values higher than  $100 \, \mathrm{W \, m^{-1} \, K^{-1}}$  are all obtained on anisotropic samples. From the conductivity data measured along the a- and c-axes in a single grain<sup>54</sup>, one can estimate an average isotropic value of about  $106 \, \mathrm{W \, m^{-1} \, K^{-1}}$ , close to our estimation of  $105 \, \mathrm{W \, m^{-1} \, K^{-1}}$ .

In general the theoretical estimates are in good agreement (within 20%) with the best experimentally observed values (Table 5). If the intercept with the T-axis is underestimated (like in the case of AlN due to optic phonons contributing substantially to the heat conduction) the maximum achievable thermal conductivity is underestimated. However, at higher temperatures ( $T > 3 \times (1/4)\tilde{\theta}_0$ ) the exact value of the intercept with the T-axis becomes less important. At high temperatures the accuracy of the estimate is consequently determined by the error in the slope A'. As for most applications the thermal conductivity at elevated temperature (>300 K) is of importance, the estimate of the intercept is considered sufficiently accurate.

#### 5.3. Limitations, accuracy and reliability

It should be noted that the new estimation method based on Eq. (5) was obtained by approximating an already simple description of the (temperature dependence of the) thermal diffusivity (Eq. (4)) of a pure phonon conductor. Furthermore the values of b=2 and  $\theta$  used to calculate the intercept with the T-axis are somewhat arbitrary. For practical use the choice of b=2 and  $\theta=\theta_0$  seems to work out reasonably well as  $\theta_0$  can be easily obtained from elastic constants and reasonable, somewhat conservative, estimates for the

Table 6 Estimates of the thermal conductivity for MgSiN<sub>2</sub>, AlN and  $\beta$ -Si<sub>3</sub>N<sub>4</sub> ceramics at 300 K, based on different theoretical approximations

	Estimated value (W m <sup>-1</sup> K <sup>-1</sup> )	Reference	Estimation method based on
	MgSiN <sub>2</sub>	14	$\kappa_{\rm exp} = 23 \mathrm{W  m^{-1}  K^{-1}}$
	28	This work	$a^{-1}$ vs. T
	34	65	Standard Slack equation
	$26 \pm 4$	14	Thermal diffusivity measurements
	35–50	58	Defect scattering
	40–70	58	Slack equation
	75	66	Slack equation
Time↑	120	8	Not specified*
	AIN		$\kappa_{\rm exp} = 266  {\rm W  m^{-1}  K^{-160}}$
	200	This work	$a^{-1}$ vs. T
	128	65	Slack equation
	319**	40	Defect scattering
Time↑	320	2	Scaling factor $\bar{M}\delta\theta^3$
	$\beta$ -Si <sub>3</sub> N <sub>4</sub>		$\kappa_{\rm exp} = 106  {\rm W  m^{-1}  K^{-154}}$
	105	This work	$a^{-1}$ vs. $T$
	260	67	Molecular dynamics
	250	56	Slack formula
	124	65	Slack formula
	177**	7	Two-phase composite model
Time↑	200–320	5	Slack equation

For comparison the highest measured values ( $\kappa_{\rm exp}$ ) are also given (\*probably based on  $n^{-2/3}$  dependence of the Slack equation  $^{10}$  and the estimate of the intrinsic thermal conductivity of about 300 W m<sup>-1</sup> K<sup>-1</sup> for AlN; \*\*anisotropic values).

theoretical thermal conductivity are obtained. As shown for  $Si_3N_4$  even better agreement is obtained if values for the  $\tilde{\theta}_{\infty}^A$  are available.

The presented estimation method seems to be more reliable than the theoretical Slack equation  $^{10}$  (Table 6). This can be explained in view of the influence of the accuracy of the reduced Debye temperature on the resulting estimate. The (more complicated) Slack equation is very sensitive for relatively small deviations in the input parameters, whereas the here presented method is relatively easy applicable and less sensitive for small deviations in slope and intercept. In general, the Slack equation is especially useful when no samples for thermal diffusivity measurements are available, whereas the  $a^{-1}$  versus T plots give a more accurate indication of the maximum achievable thermal conductivity and additionally can be used to guide processing optimisation in order to obtain the desired thermal conductivity.

## 6. Conclusions

A new, simple method for estimating the achievable (intrinsic) thermal conductivity of non-metallic compounds was presented, based on temperature dependent thermal diffusivity measurements. Its strength is that non-optimised samples can be used to provide a good impression of the intrinsic thermal conductivity. It was successfully applied to MgSiN<sub>2</sub>, AlN and β-Si<sub>3</sub>N<sub>4</sub> providing some evidence for its general applicability. For AlN at 300 K a too low estimate was obtained due to the fact that the intercept with the T-axis was underestimated as optic phonons, which are not considered, contribute substantially to the heat conduction. In general the estimates are accurate within 20% and become more accurate with increasing temperature, independent of the fact whether or not optic phonons contribute substantially to the heat conduction. Furthermore, the method is a useful tool for optimising the processing as it enables discrimination between the lattice characteristics, defects and microstructure.

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