

## Frequency dependence of dielectric properties of metallodielectric SrTiO<sub>3</sub>–Pt composites

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Available online 5 January 2007

### Abstract

The frequency dependence of dielectric properties of SrTiO<sub>3</sub>–Pt (platinum) composites has been investigated. The SrTiO<sub>3</sub>–Pt composites sintered at 1300 °C for 2 h was prepared by using conventional ceramic fabrication method. The dense metallodielectric composites without chemical reaction between SrTiO<sub>3</sub> and Pt during sintering process were obtained. The relative permittivity ( $\epsilon_r$ ) of SrTiO<sub>3</sub>–Pt composites was increased with increase of amount of Pt. The maximum  $\epsilon_r$  of 2150 at 1 MHz was obtained for the composite of SrTiO<sub>3</sub>–27 vol.% Pt. Moreover, the SrTiO<sub>3</sub>–Pt composites exhibited high values of  $\epsilon_r$  at low frequencies than at high frequencies due to space charge polarization. The loss tangent ( $\tan \delta$ ) of SrTiO<sub>3</sub>–Pt composites increased with increasing amount of Pt, and decreased with increasing frequency up to 1 MHz. However, the  $\tan \delta$  of SrTiO<sub>3</sub>–Pt composites was significantly increased at microwave frequency due to abrupt increase of ac conductivity of composite.

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**Keyword:** Dielectric properties

### 1. Introduction

Paraelectric ceramics have been playing as key components of dielectric resonator for microwave communication application in the microwave circuits because of their low dielectric loss relative to ferroelectric.<sup>1</sup> In particular, paraelectric ceramics with high permittivity ( $\epsilon_r$ ) are useful for miniaturization of electronic components such as dielectric resonator, antennas, and other devices. Moreover, It is expected that paraelectric ceramics with giant  $\epsilon_r$  should be useful candidate as passive components in capacitors instead of ferroelectric due to no phase transition. In order to obtain high  $\epsilon_r$ , many methods have been reported such as formations of solid solution, texture engineering and mixing rule.<sup>2–4</sup> However, by these methods it was difficult to enhance  $\epsilon_r$  of paraelectric ceramics by a factor of several times.

On the other hand, percolative phenomenon is a useful method to achieve a high  $\epsilon_r$ . In general, the behavior occurs in materials filled with inclusions such as highly conducting fibers distributed randomly in a host, which demon-

strates a insulator–metal transition with increasing metal concentration.<sup>5–7</sup> According to percolation theory, the electric properties such as  $\epsilon_r$ , electrical conductivity changes significantly with composition when one phase in the mixture is approaching its percolation threshold.<sup>8</sup> Recently, ferroelectric BaTiO<sub>3</sub> with giant  $\epsilon_r$  has been reported by Pecharrroman et al. which used percolative phenomena where the microscopic average electric field inside matrix is increased.<sup>9</sup> However, to the best of our knowledge, there are no reports of paraelectric with giant  $\epsilon_r$ . To fabricate a paraelectric with giant  $\epsilon_r$ , we choose paraelectric SrTiO<sub>3</sub> (ST) as host material due to its advantages of relatively high  $\epsilon_r$ .

In this study, the sintering properties of SrTiO<sub>3</sub>–Pt dual composites are investigated. In addition, the frequency independence of dielectric properties and conductivity of ST–Pt composites as a function of Pt particle concentration is presented.

### 2. Experimental procedures

Reagent-grade SrCO<sub>3</sub> (99.5%), TiO<sub>2</sub> (99.97%) and Pt (99.9%) were used as raw materials. To prepare strontium titanate ceramic SrTiO<sub>3</sub>, SrCO<sub>3</sub> and TiO<sub>2</sub> were mixed according to the stoichiometry of SrTiO<sub>3</sub> in an ethanol with zirconia balls for 24 h. After drying, the powder mixture was calcined at

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1050 °C for 18 h. The calcined SrTiO<sub>3</sub> powder again mixed with Pt powders in a mortar with ethanol and pestle for 1 h according to the composites of the SrTiO<sub>3</sub>–xPt, where  $x = 5, 15, 25, 26$  and 27 vol.%. Subsequent to above process, polyvinyl alcohol was added to the reground powder. The powder was pressed into cylindrical shape under a uni-axial pressure of 7.84 MPa and then was again subjected to cold isostatic pressing (CIP) at a pressure of 200 MPa. The prepared pellets were sintered at 1300 °C for 2 h in air. Then silver electrodes were pasted on both the side of the pellets for measurement of impedance analyzer.

The microstructures of the sintered samples were observed by scanning electron microscopy (SEM) and energy dispersive spectroscopy (EDS). The crystalline phase of the sintered samples were characterized by X-ray power diffraction (XRD) using Cu K $\alpha$  radiation (Philips X'Pert MPD, Kanagawa, Japan). The bulk density was determined by the Archimedes method. The dielectric properties and ac conductivity of the samples up to 1 MHz were measured by using an impedance analyzer. In addition, the microwave dielectric properties were measured by the modified Hakki and Coleman's method in the TE<sub>011</sub><sup>10,11</sup> mode using a network analyzer.

### 3. Results and discussion

The XRD patterns of the SrTiO<sub>3</sub>–xPt composites (where  $x = 0, 15$  and 25 vol.%) sintered at 1300 °C for 2 h are shown in Fig. 1. The patterns of both SrTiO<sub>3</sub> and SrTiO<sub>3</sub>–Pt composites agree very well with ICDD card 79-0174 (SrTiO<sub>3</sub>: short stick) and 70-2057 (Pt: long stick), respectively. The intensity of SrTiO<sub>3</sub> is decreased with increase of amount of Pt. The maximum XRD peak was changing from 32.39° (maximum XRD peak of ST) to 39.79° (maximum XRD peak of Pt) with increase of Pt. In addition, secondary phases were not observed in the XRD patterns. This suggests that chemical reaction has not occurred between ST and Pt during the sintering process.

Fig. 2 shows the measured density of SrTiO<sub>3</sub>–Pt composites. The apparent density of SrTiO<sub>3</sub>–Pt composites increased with

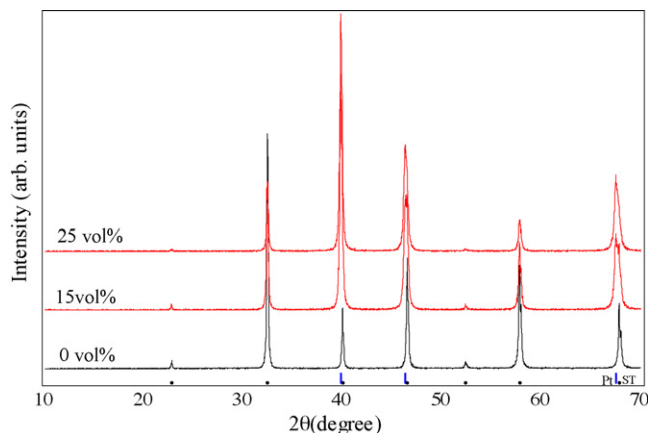


Fig. 1. X-ray diffraction patterns of SrTiO<sub>3</sub>–xPt composites sintered at 1300 °C for 2 h: (a)  $x = 0$ , (b)  $x = 0.15$  and (c)  $x = 0.25$ . The short and long sticks at the bottom of XRD patterns represent ST and Pt peaks according to the ICDD cards, respectively.

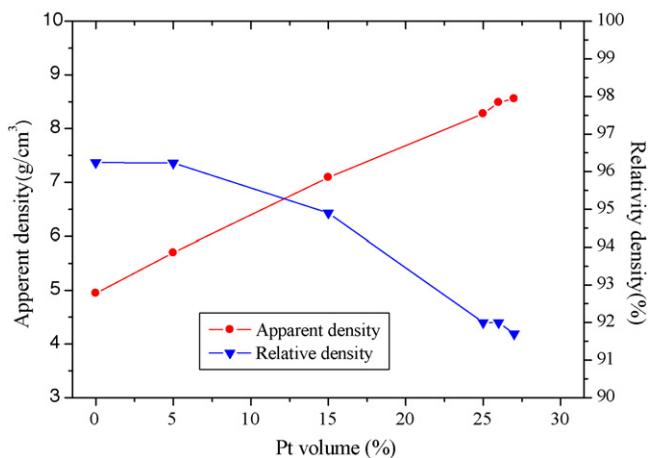


Fig. 2. Apparent and relative density of SrTiO<sub>3</sub>–Pt composites sintered at 1300 °C for 2 h.

increasing amount of Pt. This is because Pt (21.461 g/cm<sup>3</sup>) has a higher a theoretical density than SrTiO<sub>3</sub> (5.118 g/cm<sup>3</sup>). On the other hand, the relative density of one decreased with increasing amount of Pt.

The SEM images of composites with different volumes of Pt and their EDS image are shown in Fig. 3. It is seen in Fig. 3(b)–(d) that light gray particles are uniformly distributed on the surface of matrix. Fig. 3(e) represents the region framed in Fig. 3(d) at a higher magnification, showing that the light gray particles which was identified as Pt by EDS analysis (Fig. 3(f)). In addition, the Pt agglomerated with increasing amount of Pt. The coalescence of Pt may be caused by pores. These pores also contributes to the decrease of relative density of SrTiO<sub>3</sub>–Pt composites with increasing amount of Pt.

Fig. 4 shows the frequency dependence of  $\epsilon_r$  of the SrTiO<sub>3</sub>–Pt composites. The  $\epsilon_r$  of SrTiO<sub>3</sub>–Pt composites increased with increasing amount of Pt. The SrTiO<sub>3</sub>–27 vol.% Pt composite exhibited maximum value  $\epsilon_r$  of 2150 at 1 MHz. The  $\epsilon_r$  of SrTiO<sub>3</sub>–Pt shows a high value at low frequency compared with one at high frequency due to space charge polarization, which occurs at interfaces of two materials with different conductivity. In addition, in the range of low frequency from 100 Hz to 1 kHz, the SrTiO<sub>3</sub> with high Pt concentrations exhibit relatively high dielectric dispersion with frequency compared with the SrTiO<sub>3</sub> with low Pt concentrations because of large amount of space charge polarization.

The frequency dependence of loss tangent ( $\tan \delta$ ) of SrTiO<sub>3</sub>–Pt composites are shown in Fig. 5. The  $\tan \delta$  of SrTiO<sub>3</sub>–Pt composites increased with increasing amount of Pt. It shows high  $\tan \delta$  at lower frequencies due to space charge polarization. As increasing frequency up to 1 MHz, the  $\tan \delta$  of one rapidly decreased since space charge polarization does not affect significantly a  $\tan \delta$  in the range of high frequency. Also, it can be interpreted as following the expression:

$$\epsilon''(f) = \frac{\sigma(f)}{\omega \epsilon_0} \quad (1)$$

where  $\epsilon''$  is the imaginary part of permittivity,  $\sigma$  the conductivity of composite, and  $\omega (=2\pi f)$  is the angular frequency. According

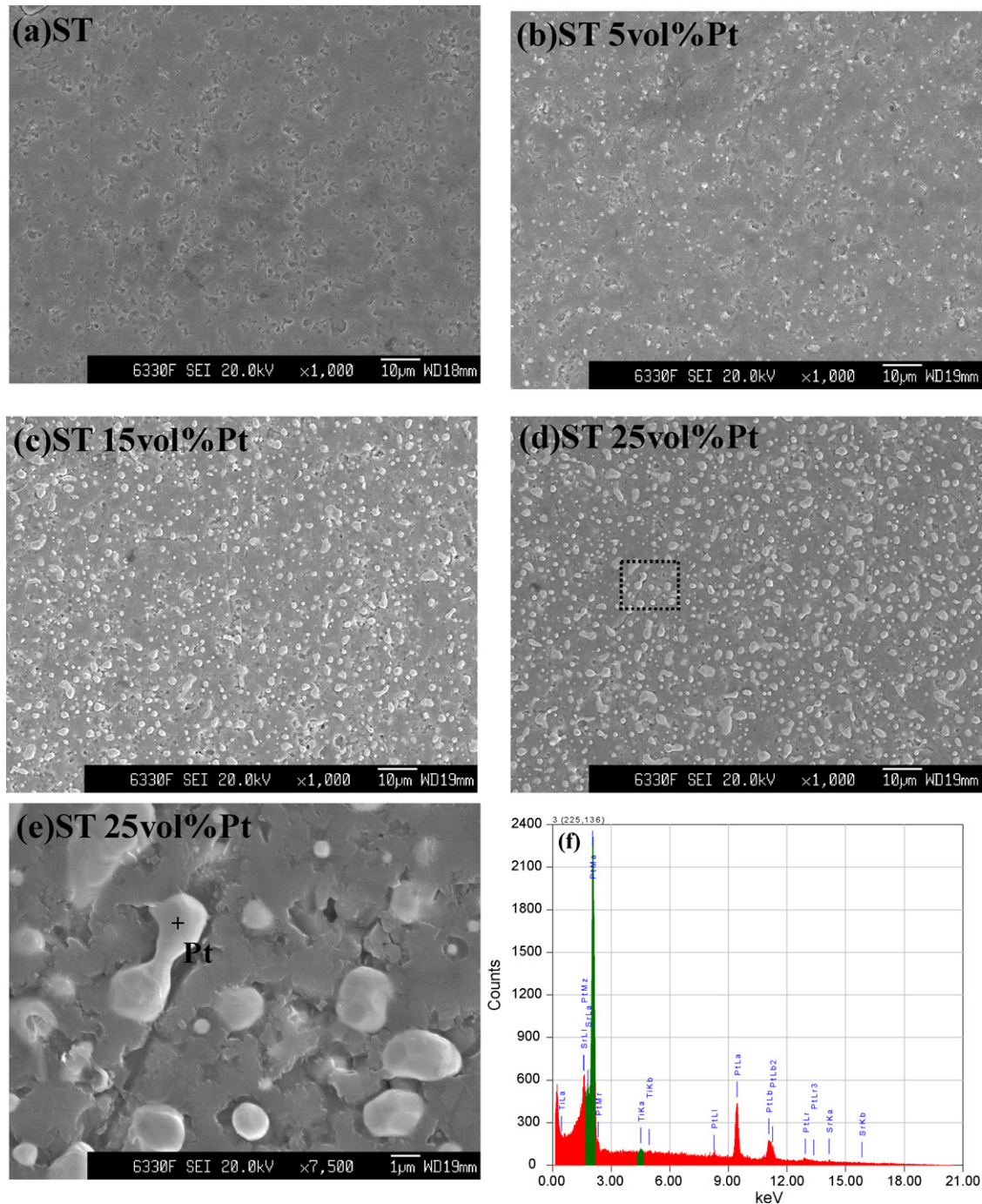


Fig. 3. SEM images of SrTiO<sub>3</sub>-xPt composites sintered at 13:00 h for 2 h: (a)  $x=0$ , (b)  $x=0.05$ , (c)  $x=0.15$ , (d)  $x=0.25$ , and (e and f) enlarged SEM image and EDS spectra of  $x=0.25$ .

to Eq. (1),  $\varepsilon''$  is decreased as increasing frequency. On the other hands, the  $\tan \delta$  of one at microwave shows again a high  $\tan \delta$ , which is observed in composites with high Pt concentration more clearly. It can be expected that such significant increase of  $\tan \delta$  at microwave results from the increase of  $\sigma(f)$ . In order to verify the behavior, we measured the ac conductivity of SrTiO<sub>3</sub>-Pt composites.

The measured ac conductivity of SrTiO<sub>3</sub>-Pt composites is shown in Fig. 6. The ac conductivity of SrTiO<sub>3</sub>-Pt compos-

ites increased with increasing amount of Pt as well as the increase of frequency. Particularly, the variation rate of the ac conductivity with frequency at above 100 kHz is higher than one in the range of low frequency. Although, the ac conductivity of SrTiO<sub>3</sub>-Pt composites at microwave could not measure in this study, large increase of ac conductivity can be expected in the microwave range. Such exponential increase of ac conductivity with increasing frequency affects a high  $\tan \delta$  at microwave.



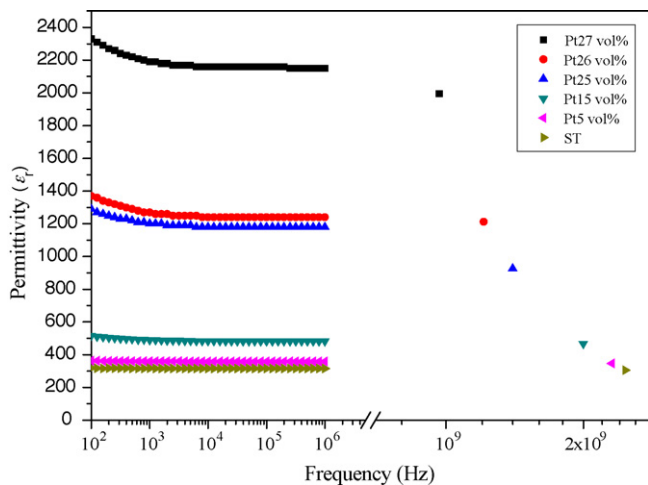


Fig. 4. Frequency dependence of real part of permittivity ( $\epsilon_r$ ) of SrTiO<sub>3</sub>-Pt composites.

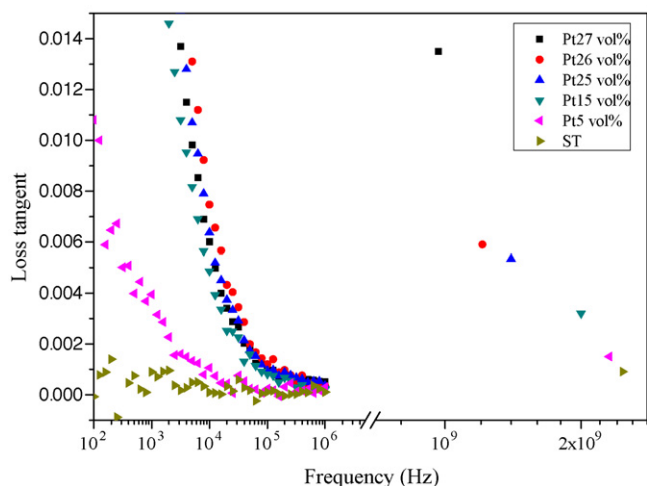


Fig. 5. Frequency dependence of loss tangent of SrTiO<sub>3</sub>-Pt composites.

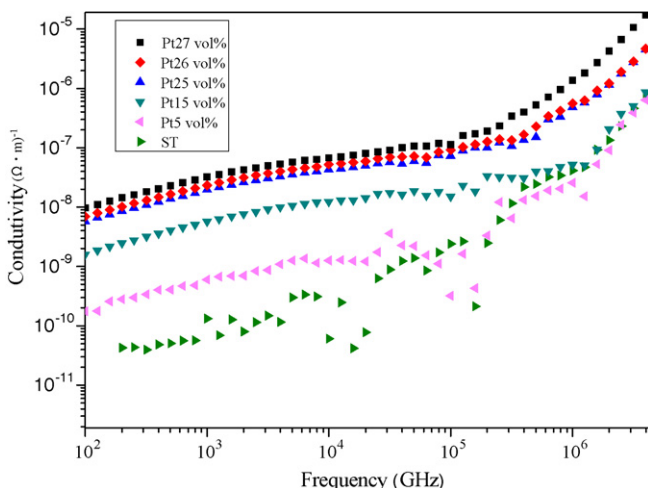


Fig. 6. Frequency dependence of conductivity of SrTiO<sub>3</sub>-Pt composites.

#### 4. Conclusion

The dielectric properties of SrTiO<sub>3</sub>-Pt dual composites with frequency have been investigated. The dense SrTiO<sub>3</sub>-Pt composites sintered at 1300 °C for 2 h, without chemical reaction between SrTiO<sub>3</sub> and Pt during sintering process, were obtained. The  $\epsilon_r$  and  $\tan \delta$  were increased with increase of amount of Pt. The SrTiO<sub>3</sub>-Pt composites exhibit high dielectric dispersion and high  $\tan \delta$  in low frequency areas due to the amount of large space charge polarization. On the other hand, the  $\tan \delta$  of SrTiO<sub>3</sub>-Pt composites were decreased with increasing frequency up to 1 MHz, and then it was significantly increased at microwave possibly because of exponential increase of ac conductivity.

#### Acknowledgements

One of the authors (W.W. Cho) acknowledges Prof. H. Ogawa and A. Kan of Meijo University for their assistance with the observation of the microstructures, and the Japan Society for Promotion of Science (JSPS) for fellowship and financial assistance. This work was supported by a grant from NITECT 21st century COE program “World Ceramics Center for Environment Harmony”.

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