

# Ruby micro-piezospectroscopy in $\text{GdAlO}_3/\text{Al}_2\text{O}_3$ ( $/\text{ZrO}_2$ ), $\text{Er}_3\text{Al}_5\text{O}_{12}/\text{Al}_2\text{O}_3$ ( $/\text{ZrO}_2$ ) and $\text{Y}_3\text{Al}_5\text{O}_{12}/\text{Al}_2\text{O}_3$ ( $/\text{ZrO}_2$ ) binary and ternary directionally solidified eutectics

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## Abstract

The fluorescence from (naturally present)  $\text{Cr}^{3+}$  impurities was used to measure the residual stress in the alumina phase of six melt-grown ceramic eutectic composites associating gadolinium aluminum perovskite (GAP), erbium aluminum garnet (EAG) or yttrium aluminum garnet (YAG) with  $\alpha$ -alumina and cubic zirconia. Such measurements are reported for the first time in the GAP containing eutectics.

In the usual hydrostatic assumption, we conclude to a residual compression in the range of  $\sim 70$ – $400$  MPa depending on the sample composition. The validity of the hydrostatic assumption is questioned when a microscope is used for the measurements.

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## 1. Introduction

Directionally solidified eutectic (DSE) ceramic oxides are high melting point interlocking distributions of oxidation resistant single crystals, exhibiting remarkable strength and creep resistance.<sup>1–3</sup> They are developed in view of high-temperature structural applications such as turbine blades and reliability will strongly depend on the initial level of residual stress. In DSEs incorporating a ruby phase (*i.e.* a chromium-doped  $\alpha$ -alumina single crystal),  $R_1$  and  $R_2$  fluorescence bands can be used to monitor this stress, with the advantage of precise and easy impact point selection.<sup>2</sup> These bands shift under stress as a result of  $\text{Cr}^{3+}$  ligand field modification and have been used since 1986 for pressure calibration in diamond anvil cells.<sup>4</sup> If the stress is expressed in an arbitrary orthogonal frame and does not exceed

20 GPa, then the wavenumber shifts can be approximated with the following relation<sup>5,6</sup>:

$$\Delta \bar{\nu}_{R_n} = \sum_{i,j=1}^3 (\Pi_{ij}^{R_n} \sigma_{ij}); \quad R_n = R_1 \text{ or } R_2 \quad (1)$$

In Eq. (1),  $\sigma_{ij}$  and  $\Pi_{ij}$  terms are the stress components and the so-called piezospectroscopic coefficients, respectively. The equation simplifies if the reference orthogonal frame is chosen so that its axes coincide with the  $a$ ,  $m$  and  $c$  axes of the reference hexagonal lattice<sup>2,6</sup>:

$$\Delta \bar{\nu}_{R_n} = \sum_{i=1}^3 (\Pi_i^{R_n} \sigma_i) \quad (2)$$

In Eq. (2), the engineer notation ( $i=1, 2$  and  $3$  for  $11, 22$  and  $33$  indexes, respectively) has been adopted for simplicity and we shall use it from now on. He and Clarke<sup>6</sup> calibrated Eq. (2) (see Table 1) and confirmed the absence of shear stress wavenumber sensitivity in the specified frame. Their results have been widely used for *in situ* stress measurements in alumina-containing materials, including in DSEs.<sup>2,7</sup>

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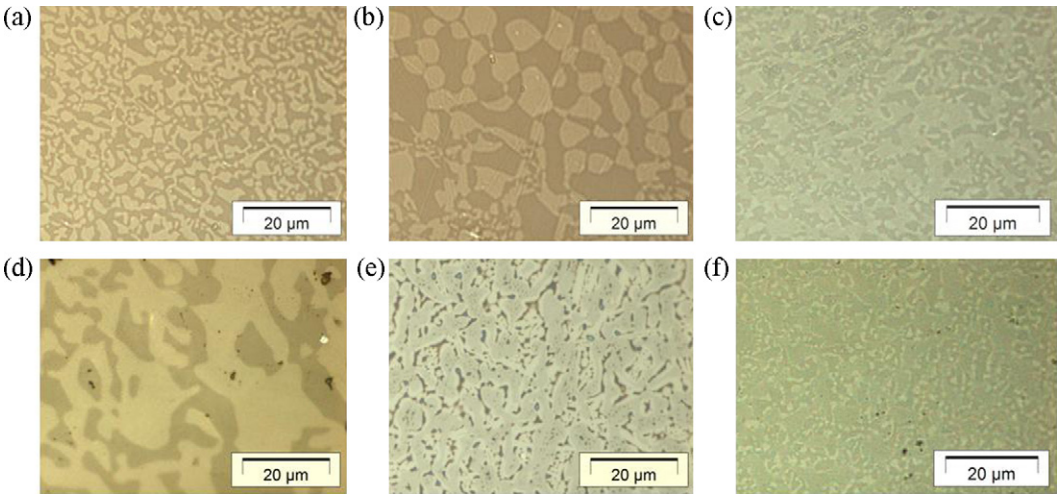


Fig. 1. Optical micrographs of polished cross sections from (a) AG sample (center of the rod), (b) AG (periphery of the rod), (c) AGZ, (d) AE, (e) AY and (f) AYZ. Alumina appears as the darkest phase.<sup>30</sup> Cubic zirconia is not clearly visible but was evidenced by XRD and EDX chemical cartography.<sup>47</sup> Refer to Table 2 for sample details.

This paper presents ruby fluorescence-based residual stress measurements in DSEs associating  $\alpha$ -alumina with either  $\text{GdAlO}_3$  perovskite (GAP),  $\text{Er}_3\text{Al}_5\text{O}_{12}$  garnet (EAG) or  $\text{Y}_3\text{Al}_5\text{O}_{12}$  garnet (YAG). Ternary eutectic compositions adding a cubic zirconia phase for increased flexural strength and fracture toughness<sup>8,9</sup> were also investigated. The present work being the first to study as many as six different DSEs at once, it gives a good insight on the intrinsic accuracy of the technique. Note that ruby Raman spectra exhibit stress sensitivity<sup>10,11</sup> (combined Raman and fluorescence piezospectroscopic studies have even been reported<sup>12,13</sup>) but the fluorescence is much easier to detect, specially in multiphased samples.  $\text{Y}^{3+}$ ,  $\text{Er}^{3+}$  and  $\text{Gd}^{3+}$  ions fluorescence could in theory be used to measure stress in YAG, EAG and GAP phases, but rare-earth ions have a much lower stress sensitivity than transition elements.<sup>6</sup> The stress sensitivity of  $\text{Cr}^{3+}$  impurities fluorescence has been measured in GAP<sup>14</sup> but we could not detect a nice enough fluorescence signal to use it.

2. Materials and methods

2.1. The samples of the study

The acronyms for the samples are given in Table 2. The synthesis started with a 150 MPa isostatic pressing of cylinders (approximately 40 mm in length and 8 mm in diameter) formed with mixed 99.9% purity polycrystalline powders of

$\text{Al}_2\text{O}_3$  (Baikowski Chimie, France),  $\text{Gd}_2\text{O}_3$  (Rhodia, France),  $\text{Er}_2\text{O}_3$  (Rhodia),  $\text{Y}_2\text{O}_3$  (Rhodia) and  $\text{ZrO}_2$  (Th. Goldschmidt Industriechemikalien, Germany). Two cylinders were then sintered for 10 h at 1673 K and later set in an arc image furnace operating with a 6 kW xenon lamp. As soon as a liquid droplet was obtained at the focal point of two elliptic mirrors, the cylinders were driven down at the constant speed of  $10\text{ mm h}^{-1}$ . 3 mm-sided cubes were cut in the as-prepared rod centers and one face corresponding to the rod cross section was polished to  $0.25\text{ }\mu\text{m}$  using diamond paste and colloidal silica. SEM and optical pictures show an interconnected structure<sup>15</sup> (Fig. 1) and  $\alpha$ -alumina preferential orientation was revealed through TEM and electron backscattering diffraction<sup>15,16</sup> (Fig. 2). Like in most DSE rods, the cross sections exhibit a radial phase distribution (resulting from thermal gradients during synthesis) and a

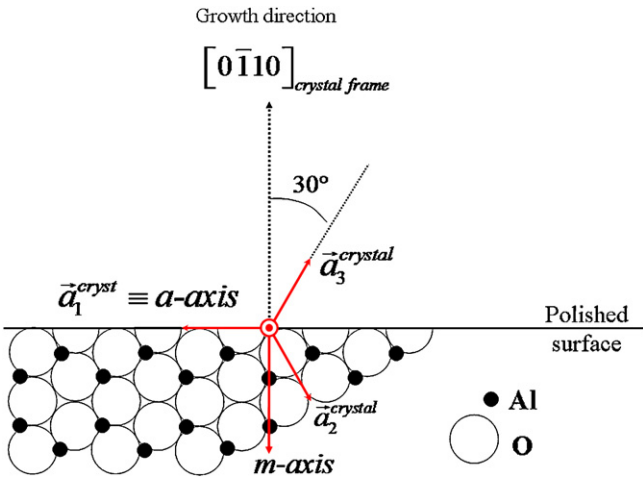


Fig. 2.  $\alpha$ - $\text{Al}_2\text{O}_3$  preferential growth direction in all samples, as obtained through electron backscattering diffraction (EBSD) and transmission electron microscopy (TEM).<sup>15,16</sup> The polished surface is a cross-section of the eutectic rod. The  $a$ - and  $m$ -axes are the first two axes of the orthogonal frame used for ruby piezospectroscopy.

Table 1  
Alumina piezospectroscopy coefficients obtained by linear regression of data collected up to 0.9 GPa.<sup>6</sup> The original values were rounded to the first decimal place.  $\Pi_{11}^{R_1}$  corresponds to the best linear fit of  $\Delta\bar{\nu}_{\text{cm}^{-1}} = -2.56\sigma_{\text{GPa}} - 0.8\sigma_{\text{GPa}}^2$  relationship.<sup>6</sup>

Ruby line	$\Pi_{11}$ ( $\text{cm}^{-1}\text{ GPa}^{-1}$ )	$\Pi_{22}$ ( $\text{cm}^{-1}\text{ GPa}^{-1}$ )	$\Pi_{33}$ ( $\text{cm}^{-1}\text{ GPa}^{-1}$ )
$R_1$	3.1	3.5	1.5
$R_2$	2.7	2.8	2.2

Table 2

The directionally solidified eutectic (DSE) samples of the study.<sup>15,29,46,47</sup>

Sample code	Starting batch	Melting temperature	X-ray phase analysis
AE	82 mol% Al <sub>2</sub> O <sub>3</sub> 18 mol% Er <sub>2</sub> O <sub>3</sub>	1810 °C	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + Er <sub>3</sub> Al <sub>5</sub> O <sub>12</sub> (EAG)
AG	77 mol% Al <sub>2</sub> O <sub>3</sub> 23 mol% Gd <sub>2</sub> O <sub>3</sub>	1720 °C	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + GdAlO <sub>3</sub> (GAP)
AY	81 mol% Al <sub>2</sub> O <sub>3</sub> 19 mol% Y <sub>2</sub> O <sub>3</sub>	1825 °C	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + Y <sub>3</sub> Al <sub>5</sub> O <sub>12</sub> (YAG)
AEZ	65.9 mol% Al <sub>2</sub> O <sub>3</sub> 15.5 mol% Er <sub>2</sub> O <sub>3</sub> 18.6 mol% ZrO <sub>2</sub>	–	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + EAG + cubic ZrO <sub>2</sub>
AGZ	58 mol% Al <sub>2</sub> O <sub>3</sub> 19 mol% Gd <sub>2</sub> O <sub>3</sub> 23 mol% ZrO <sub>2</sub>	1700 °C	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + GAP + cubic ZrO <sub>2</sub>
AYZ	65 mol% Al <sub>2</sub> O <sub>3</sub> 16 mol% Y <sub>2</sub> O <sub>3</sub> 19 mol% ZrO <sub>2</sub>	1715 °C	$\alpha$ -Al <sub>2</sub> O <sub>3</sub> + YAG + cubic ZrO <sub>2</sub>

 $\alpha$ -Al<sub>2</sub>O<sub>3</sub>: trigonal alumina, EAG and YAG: cubic erbium and yttrium aluminum garnets and GAP: orthorhombic gadolinium aluminum perovskite.

number of structural imperfections occurring every few tens of micrometers.<sup>12,17–20</sup>

## 2.2. Ruby piezospectroscopy

Ruby fluorescence was observed with Raman microspectrometers, in air-conditioned rooms (for temperature stability) and using the 514.529 nm excitation of an Ar<sup>+</sup> ion laser. Cr<sup>3+</sup> substitution by alumina soluble impurities is known to affect R-lines wavenumber<sup>21</sup> but we shall assume Cr<sup>3+</sup> concentration to be the same in the alumina phase of all samples. Most spectra were collected on an “XY” model (Horiba-JY, formerly Dilor, France) equipped with a double monochromator as a filter and a back-illuminated 2000 × 800 pixels CCD detector cooled down to 140 K in liquid nitrogen. Because of a temporary unavailability of the XY model, AEZ sample was studied with a Labram-HR (Horiba-JY) spectrometer. We systematically used 100× objectives (~1  $\mu$ m diameter lateral probing) to select perfectly homogeneous domains and avoid the structural disturbances described in Section 2.1. The emission from a neon lamp was used to serve as an external reference and we will refer to the 703.24 and 692.95 nm lines<sup>22</sup> as Ne<sub>1</sub> and Ne<sub>2</sub>, respectively. “Raman shifts” measuring the wavenumber difference between the photons collected from a laser-illuminated sample and those from the source, R<sub>1</sub> ( $\lambda$  = 694.2 nm) and R<sub>2</sub> ( $\lambda$  = 692.8 nm) lines show around 5000 cm<sup>−1</sup> with a 514.5 nm laser (Fig. 3).

## 3. Results and discussion

All the tested DSEs have R<sub>1</sub> and R<sub>2</sub> fluorescence bands peaking at lower absolute wavenumber (higher Raman shift) than in a stress-free ruby (Fig. 3), revealing an overall compression of alumina phase.<sup>6</sup> A preliminary fitting of a large series of neon spectra such as the one shown in Fig. 3 established that Ne<sub>1</sub> and Ne<sub>2</sub> lines have a Gaussian shape, that Ne<sub>2</sub> has a width of 1.95 cm<sup>−1</sup> and that its intensity is 30% that of Ne<sub>1</sub>. We used these parameters to fit a large number of fluorescence spectra

twice, with or without taking Ne<sub>2</sub> component into consideration. There was no consequence on R<sub>1</sub> pinpointing and R<sub>2</sub> wavenumber changed by less than 0.1 cm<sup>−1</sup> whenever R<sub>1</sub> intensity was at least 6 times that of Ne<sub>1</sub> (Fig. 4). From now on, we shall therefore restrict our study to spectra recorded with  $I(R_1)/I(Ne_1) \geq 6$  (i.e.  $I(R_2)/I(Ne_2) \geq 12.5$ ) and fitted without Ne<sub>2</sub> component.

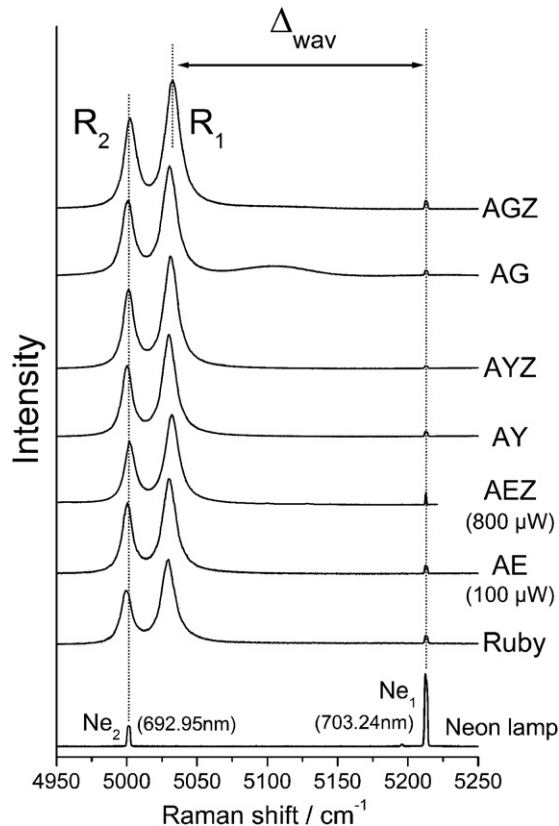


Fig. 3. Ruby fluorescence (R<sub>1</sub> and R<sub>2</sub> bands) excited with a 514,529 nm laser. Unless stated, the power of illumination was 6 mW. Neon lines Ne<sub>1</sub> and Ne<sub>2</sub> are used as absolute references.

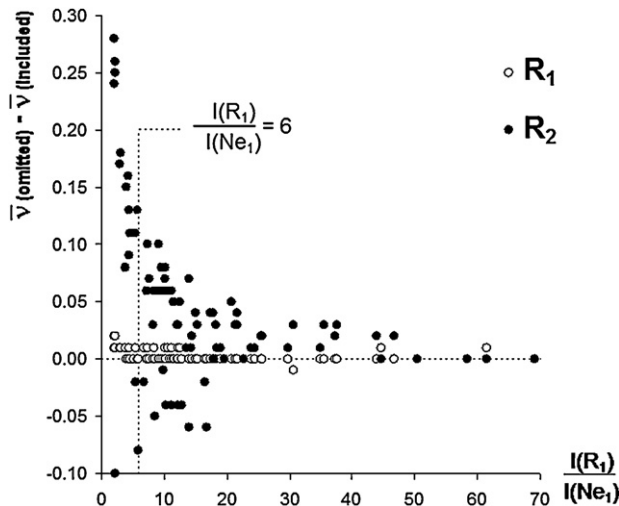


Fig. 4. Variation of  $R_1$  and  $R_2$  fitted wavenumber (in  $\text{cm}^{-1}$  unit) depending on whether  $\text{Ne}_2$  line is included or omitted in the fitting procedure.  $I(R_1)/I(\text{Ne}_1)$  is the intensity ratio of  $R_1$  and  $\text{Ne}_1$  lines.

A  $\sim 0.15 \text{ cm}^{-1} \text{ K}^{-1}$  thermal shift was measured on ruby samples probed at different temperatures.<sup>6,23–25</sup> A preliminary testing of our DSE samples showed no shift of R-lines for any laser power below 1 mW (measured on the sample) and less than  $0.5 \text{ cm}^{-1}$  overall shift for a power of 20 mW. Laser illumination thus provokes almost no heating. We limited the incident power (as measured on the sample) to 6 mW or less and Fig. 5 confirms the limited influence of the actual value on  $R_1$  and  $R_2$  pinpointing. With the possible exception of AGZ (only two powers were tested), there is indeed no systematic drift with a power change. The scattering of  $\Delta_{\text{wav}}$  (as defined in Fig. 3) is above the precision of  $R_1$  pinpointing (reaching about  $1.3 \text{ cm}^{-1}$  when AG sample is probed at 0.5 or 6 mW). There is therefore some variability from one point of a sample to another (not to mention the distribution of stress throughout each alumina grain, as was

observed with near field setups in alumina polycrystals<sup>26</sup> and  $\text{Al}_2\text{O}_3/\text{ZrO}_2$  eutectics<sup>19</sup>).

Even though the  $\sigma_1 = \sigma_2 \neq \sigma_3$  stress field hypothesis was tested on occasion,<sup>19,27,28</sup> the assumption that a purely hydrostatic stress  $\sigma_H$  is measured is the most widely used to convert ruby shifts into residual stress:

$$\sigma_H = \frac{\Delta \bar{\nu}_{R_n}}{\Pi_1^{R_n} + \Pi_2^{R_n} + \Pi_3^{R_n}} \quad (3)$$

Such assumption probably makes sense in the bulk of our samples because they are homogeneous (phases alternate every few microns (Fig. 1) when the side of the cubic samples is  $\sim 3 \text{ mm}$ ) and isotropic (longitudinal and transversal cross sections look very much the same<sup>15,29</sup>). However, the possibility for a surface-related disturbance must be discussed. Indeed, even though the samples are translucent (they illuminate under laser irradiation and mixed alumina/rare-earth oxide Raman contributions are systematically observed<sup>30</sup>), the laser is focused through a microscope objective. In air, the depth of focus (classically defined as the distance along the optical axis  $z$  where irradiance remains above 50% of its maximum value) is approximately  $4\lambda/\text{NA}^2$ , NA being the numerical aperture.<sup>31,32</sup> This corresponds to only  $2.5 \mu\text{m}$  in our conditions ( $\lambda = 514.5 \text{ nm}$ ;  $\text{NA} = 0.9$ ). Even though the depth of focus is significantly degraded by refractions (at the air/sample and inner sample interfaces) when light penetrates solids,<sup>31,33–36</sup> it thus appears that most of the collected signal comes from the first  $10 \mu\text{m}$  below the surface of our samples. In such rigid materials as DSEs (ceramics in general), one may argue that stress builds up over limited distances and bulk conditions must extend close to the free surface. Yet, we obtained different wavenumbers in AG periphery (where the domains are the largest (Fig. 1)) depending on whether alumina was probed directly or through GAP (Fig. 5). It therefore seems that there is some surface specific contribution to the ruby fluorescence signal we detected. It has to be limited though since Harlan et al. reported no significant change of ruby lines when a macroscopic setup (parallel beam) was used instead of a microscope (focused beam) to analyze alumina/zirconia eutectics.<sup>28</sup> Besides, their results were in accordance with calculations based on a triaxial stress state hypothesis. Unfortunately we could not test the macroscopic setup alternative on our own samples because they are heterogeneous at the scale of a few tens of micrometers and it would have meant probing different morphologies at once.

In the piezospectroscopy frame of Fig. 2, a purely planar stress field with  $\sigma_2 = 0$  should best describe the vicinity of the sample surface. If we assume isotropy ( $\sigma_1 = \sigma_3 = \sigma_P$ ), Eq. (2) leads to:

$$\sigma_P = \frac{\Delta \bar{\nu}_{R_n}}{\Pi_1^{R_n} + \Pi_3^{R_n}} \quad (4)$$

Fig. 6 and Table 3 give the residual stress calculated using Table 1 values in the hydrostatic (Eq. (3)) and planar equibiaxial (Eq. (4)) stress models. The (average) error bars were calculated using the following uncertainties:

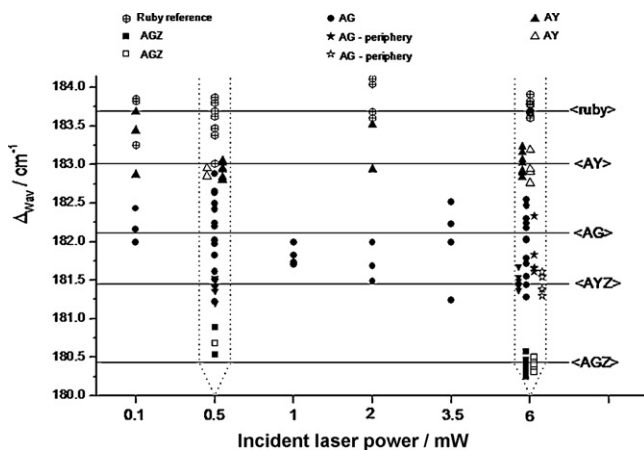


Fig. 5. Fitted values of  $\Delta_{\text{wav}}$  (Fig. 3) as a function of the incident power measured on the sample (some series recorded with 0.5 and 6.0 mW were shifted for better viewing). The fluorescence spectra were recorded with the laser focused on optically dark domains (alumina) except for the series marked with hollow symbols (laser focused on the garnet or perovskite phase). The periphery of AG sample is characterized by a coarser microstructure (see Fig. 1a and b). Horizontal lines indicate each series average value.



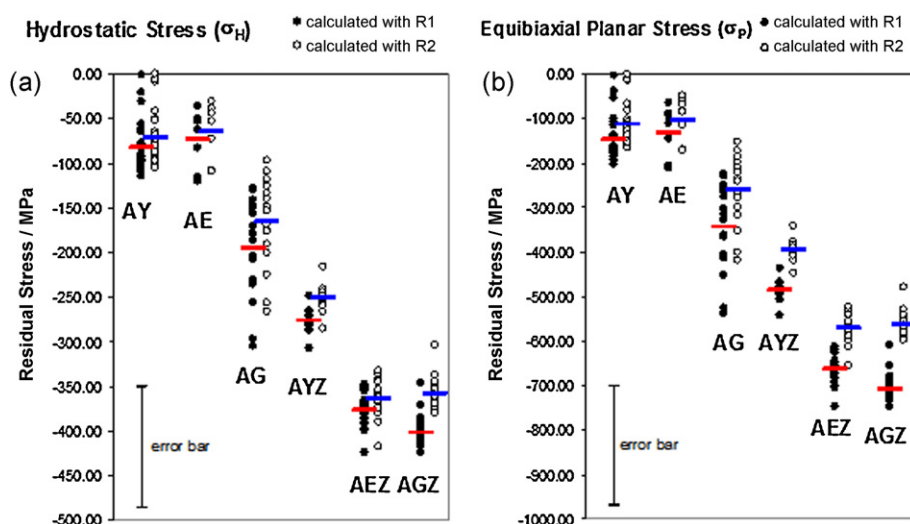


Fig. 6. The residual stress calculated according to Eqs. (3) and (4). The fluorescence spectra were recorded with the laser focused on optically dark domains (alumina). The horizontal bars are average values.

Table 3

Average residual compression calculated in alumina phase based on fluorescence spectra verifying the condition  $(I_{R1}/I_{Ne1}) \geq 6$ . Hydrostatic ( $\sigma_H$ ) and planar equibiaxial ( $\sigma_P$ ) assumptions were tested (see text).

Sample	$\sigma_H$ (MPa)		$\sigma_P$ (MPa)		Prev. $\sigma_H$ (MPa)
	$R_1$	$R_2$	$R_1$	$R_2$	
AE	−75	−65	−130	−105	−135 <sup>48</sup>
AEZ	−375	−365	−665	−570	
AY	−85	−70	−145	−115	−100 <sup>18</sup>
AYZ	−275	−250	−485	−395	−300 <sup>a,49</sup> [−300;−400] <sup>18</sup>
AG	−195	−165	−345	−260	
AGZ	−400	−360	−710	−560	

<sup>a</sup> At a comparable growth rate.

- − 0.1 cm<sup>−1</sup> GPa<sup>−1</sup> for all piezospectroscopic coefficients except  $\Pi_{11}^{R1}$ . For the latter we took 0.4 cm<sup>−1</sup> GPa<sup>−1</sup> uncertainty since the slopes letting He and Clarke experimental data points<sup>6</sup> above and below a straight line would be −2.6 and −3.3 cm<sup>−1</sup> GPa<sup>−1</sup>, respectively.
- − 0.2 cm<sup>−1</sup> for  $R_1$  and  $R_2$  wavenumber shifts. Each line was indeed positioned with the  $\sim 0.1$  cm<sup>−1</sup> fitting-related uncertainty evidenced in Fig. 4, the use of Ne<sub>1</sub> reference compensating for the uncertainty on the spectrometer positioning.

In Fig. 6b, the  $\sigma_P$  values derived from  $R_1$  and  $R_2$  lines agree to within error bars. The use of Eq. (4) to assess the non hydrostatic component of the stress field is thus probably legitimate. Unfortunately, the “random” distribution of alumina precludes the testing of hypothesized depth-dependent combinations of  $\sigma_H$  and  $\sigma_P$  to simulate the experimental ruby shifts.<sup>37,38</sup> The best way to assess at which depth the stress field becomes purely hydrostatic would be to close the confocal hole of the Raman microscope (thus reducing the depth of field) and progressively lower laser focus into the sample down to the level where the ruby lines would show no variation. This is far beyond the original scope of this study because a thorough statistical approach would be mandatory to smooth the effect of the random alumina distribution across the sample thickness, not to mention the problem of refraction altering the actual probing depth.<sup>31,33–36</sup>

There is little agreement between our  $\sigma_H$  values and those previously reported in AY, AYZ and AEZ samples (Table 3). Yet, there is no way of being sure that the samples and conditions of analysis were strictly equivalent. We obtain small residual stresses in AE and AY binary eutectics, as expected from the close thermal expansion coefficients of the garnet and alumina phases (Table 4). Values below 250 MPa were already found in Al<sub>2</sub>O<sub>3</sub>/Y<sub>3</sub>Al<sub>5</sub>O<sub>12</sub> eutectics based on X-ray diffraction experiments (triaxial stress field)<sup>39,40</sup> and indentation fracture tests (hydrostatic hypothesis)<sup>41</sup>. In AG sample, the stress level is higher and a compression of alumina is ascertained, even

Table 4

Thermal expansion coefficients (in units of 10<sup>−6</sup> K<sup>−1</sup>) as obtained from dilatometry<sup>30</sup> and X-ray diffraction<sup>29</sup> experiments for temperatures up to 1000 K. (s): single crystal; (p): polycrystalline.

Trigonal Al <sub>2</sub> O <sub>3</sub> (s)	Dilato.: $\alpha_a = 8.7/\alpha_c = 9.3$ XRD: $\alpha_a = 7.8/\alpha_c = 8.7$
Er <sub>3</sub> Al <sub>5</sub> O <sub>12</sub> garnet (p)	$\alpha_{\text{dilato.}} = 9.0$ $\alpha_{\text{XRD}} = 7.9$
Y <sub>3</sub> Al <sub>5</sub> O <sub>12</sub> garnet (p)	$\alpha_{\text{dilato.}} = 8.8$ $\alpha_{\text{XRD}} = 8.5$
GdAlO <sub>3</sub> perovskite (p)	$\alpha_{\text{dilato.}} = 7.7$ XRD: $\alpha_a = 10.1/\alpha_b = 3.9/\alpha_c = 8.0$

taking the error bars into account. Again regardless of the model, the residual compression is at least doubled in each ternary sample by comparison with the zirconia-free counterpart. The high CTE of yttria-stabilized cubic zirconia (between  $11.2$  and  $12.9 \times 10^{-6} \text{ K}^{-1}$  according to Refs. 42–44, cited in Brewer et al.<sup>45</sup>) is a logical explanation for this behavior.

#### 4. Conclusions

Ruby fluorescence was used to measure the residual compression of the alumina phase in melt-grown directionally solidified eutectic composites associating gadolinium aluminum perovskite (GAP), erbium aluminum garnet (EAG) or yttrium aluminum garnet (YAG) with  $\alpha$ -alumina and cubic zirconia. Alumina residual compression depends on the second phase with  $\sigma(\text{Al}_2\text{O}_3\text{--GAP}) > \sigma(\text{Al}_2\text{O}_3\text{--YAG}) \sim \sigma(\text{Al}_2\text{O}_3\text{--EAG})$  and raises when cubic-zirconia is added as a third phase. Our results suggest that the stress field that is probed with microscopes is not purely hydrostatic because of a surface specific planar contribution in the probed volume.

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