

# Effect of $\text{Zn}^{2+}$ substitution on the microwave dielectric properties of $\text{LiMgPO}_4$ and the development of a new temperature stable glass free LTCC

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## Abstract

The  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ceramics have been prepared by the solid state ceramic route. The  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ceramic retains the orthorhombic structure up to  $x = 0.2$ . The compositions with  $0.3 \leq x \leq 0.8$  exist as a mixture of orthorhombic and monoclinic phases. When  $\text{Mg}^{2+}$  is fully replaced with  $\text{Zn}^{2+}$  ( $x = 1.0$ ) complete transition to monoclinic phase occurs. The ceramic with  $x = 0.1$  ( $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$ ) sintered at  $925^\circ\text{C}$  exhibits low relative permittivity ( $\epsilon_r$ ) of 6.7, high quality factor ( $Q_u \times f$ ) of 99,700 GHz with a temperature coefficient of resonant frequency ( $\tau_f$ ) of  $-62 \text{ ppm}/^\circ\text{C}$ . The slightly large  $\tau_f$  is adjusted nearly to zero with the addition of  $\text{TiO}_2$ .  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4\text{-TiO}_2$  composite with 0.12 volume fraction  $\text{TiO}_2$  sintered at  $950^\circ\text{C}$  shows good microwave dielectric properties:  $\epsilon_r = 10.1$ ,  $Q_u \times f = 52,900 \text{ GHz}$  and  $\tau_f = -5 \text{ ppm}/^\circ\text{C}$ . The ceramic is found to be chemically compatible with silver.

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## 1. Introduction

The past two decades have witnessed revolutionary changes in wireless communication which stimulated the development of new technologies. Low temperature co-fired ceramic (LTCC) technology has emerged as the paramount technology for the production of miniaturized microwave devices at a relatively low cost. LTCC technology offers high level of passive integration, performance stability and reliability. The ceramic system used for LTCC applications should meet the requirements such as low relative permittivity, low dielectric loss, temperature stability of dielectric properties, low coefficient of thermal expansion and high thermal conductivity. Most importantly the ceramic should be chemically compatible with silver and its sintering temperature must be less than the melting point of silver ( $961^\circ\text{C}$ ) which is the most commonly used electrode material.<sup>1</sup> Low bulk density of the ceramic is also desirable for the production of light weight electronic modules. These stringent requirements limit the number of materials available for practical applications.

Most of the conventional ceramics with good microwave dielectric properties have very high sintering temperature which is unsuitable for LTCC applications. However, the sintering temperature can be lowered by the liquid phase sintering through the addition of glasses with low melting point.<sup>1</sup> Another method to produce LTCC is through the glass-ceramic route.<sup>2</sup> In both the above mentioned approaches, presence of amorphous phase in the system may degrade the microwave dielectric properties and enhance the possibility of chemical reaction between the substrate and metal electrode.<sup>3</sup> The presence of glass phase may also reduce the ease of processing while tape casting. It is also possible to lower the sintering temperature by using fine powders prepared through wet chemical processing. However, the chemical synthesis is complicated and expensive.<sup>4</sup> Therefore a glass free ceramic with good microwave dielectric properties is desirable for LTCC applications.

Large number of glass free ceramics has been reported in the literature for LTCC applications. Among them Te and Bi based ceramics are found to have very low sintering temperature ( $<850^\circ\text{C}$ ).<sup>4–13</sup> However, most of the Te-based systems are reactive with silver which limits their practical applications. It should also be noted that any densification of ceramics below  $800^\circ\text{C}$  may prevent the complete evaporation of organics added for tape casting and leave

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out residual carbon which is detrimental to the microwave dielectric properties.<sup>2</sup>  $\text{Li}_3\text{NbO}_4$  ceramic sintered at  $930^\circ\text{C}$  is found to have good microwave dielectric properties ( $\epsilon_r = 15.8$ ,  $Q_u \times f = 55,009$  GHz and  $\tau_f = -49$  ppm/ $^\circ\text{C}$ ). The ceramic is also found to be chemically compatible with silver (Ag).<sup>14</sup> Recently, Bian et al. reported the microwave dielectric properties of  $(\text{La}_{0.5}\text{Na}_{0.5})_{1-x}(\text{Li}_{0.5}\text{Nd}_{0.5})_x\text{WO}_4$  ceramics. The composition with  $x = 0.3$  sintered at  $800^\circ\text{C}$  has remarkable dielectric properties:  $\epsilon_r = 12.7$ ,  $Q_u \times f = 23,500$  GHz and  $\tau_f = -1.4$  ppm/ $^\circ\text{C}$  at microwave frequency. However, the ceramic is found to be reactive with Ag.<sup>3</sup>  $\text{Ca}_{1-x}(\text{Li}_{0.5}\text{Nd}_{0.5})_x\text{WO}_4$  scheelites constitute another class of glass-free LTCC.  $\text{Ca}_{0.8}(\text{Nd}_{0.5}\text{Li}_{0.5})_{0.2}\text{WO}_4$  has an  $\epsilon_r$  of 11.7,  $Q_u \times f$  of 36,700 GHz, and  $\tau_f$  of 5.4 ppm/ $^\circ\text{C}$  and is chemically compatible with Ag.<sup>15</sup>

A few glass free phosphates are also reported to be suitable for LTCC applications. Bian et al.<sup>16</sup> studied the microwave dielectric properties of  $\text{AMP}_2\text{O}_7$  ( $A = \text{Ca}, \text{Sr}; M = \text{Zn}, \text{Cu}$ ). The ceramics can be sintered at a low temperature ( $\leq 950^\circ\text{C}$ ) and possess low relative permittivity ( $\epsilon_r < 8$ ).  $\text{SrCuP}_2\text{O}_7$  sintered at  $925^\circ\text{C}$  has the highest  $Q_u \times f$  greater than 100,000 GHz and lowest  $\tau_f$  of  $-62$  ppm/ $^\circ\text{C}$ . Nevertheless all the compositions react with silver. Cho et al. reported the microwave dielectric properties of  $\text{BiPO}_4$  which has a low sintering temperature of  $950^\circ\text{C}$ . The ceramic has an  $\epsilon_r$  of 22,  $Q_u \times f$  of 32,500 GHz and a  $\tau_f$  of  $-79$  ppm/ $^\circ\text{C}$ .<sup>17</sup> The value of  $\tau_f$  is large and the reactivity with silver has not been reported. In our previous paper we reported the microwave dielectric properties of olivine type  $\text{LiMgPO}_4$ . The ceramic sintered at  $950^\circ\text{C}$  shows an  $\epsilon_r$  of 6.6,  $Q_u \times f$  of 79,100 GHz and  $\tau_f$  of  $-55$  ppm/ $^\circ\text{C}$ .<sup>18</sup>  $\text{LiMgPO}_4$  sintered at  $950^\circ\text{C}$  with 0.12 volume fraction  $\text{TiO}_2$  has good microwave dielectric properties:  $\epsilon_r = 10$ ,  $Q_u \times f = 26,900$  GHz and  $\tau_f = +1.2$  ppm/ $^\circ\text{C}$ .

In the present paper we report the effect of  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$  on the microwave dielectric properties of  $\text{LiMgPO}_4$  with an objective to develop new low cost, light weight, glass free ceramics having excellent microwave dielectric properties for LTCC applications.

## 2. Experimental

$\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ceramics were prepared by the solid state ceramic route. High purity  $\text{Li}_2\text{CO}_3$  (99+%, Sigma–Aldrich, St. Louis, MO),  $(\text{MgCO}_3)_4 \cdot \text{Mg}(\text{OH})_2 \cdot 5\text{H}_2\text{O}$  (99%, Sigma–Aldrich),  $\text{ZnO}$  (99.9%, Sigma–Aldrich) and  $\text{NH}_4\text{H}_2\text{PO}_4$  (98+%, Sigma–Aldrich) were used as raw materials. Stoichiometric amounts of the oxides were weighed and ball milled in ethanol for 24 h with yttria stabilized zirconia balls. The slurry was then dried overnight in hot air oven and pre-heated at  $500^\circ\text{C}$  for 4 h. The powder was then ground and calcined at temperatures in the range  $700$ – $750^\circ\text{C}$  for 4 h. Calcined powder was ground into fine powder. The fine powder obtained was mixed with different volume fractions ( $V_f$ ) of  $\text{TiO}_2$  (99.8%, Sigma–Aldrich) in ethanol using an agate mortar and pestle. It was then mixed with 4 wt% PVA (molecular weight 22,000, BDH Lab suppliers, Poole, U.K.). The powder was again dried and ground well. Cylindrical disks having 11 mm diameter and 5–6 mm thickness were prepared by applying a

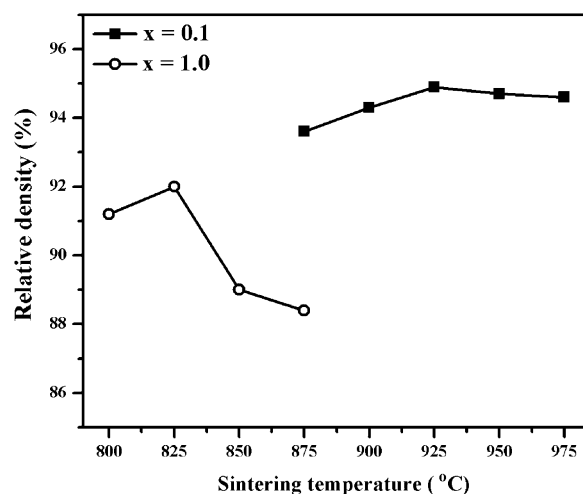


Fig. 1. Variation of relative density with sintering temperature.

pressure of 100 MPa using a uniaxial press. The samples were then sintered at temperatures in the range  $800$ – $1000^\circ\text{C}$  for 4 h with an intermediate soaking at  $600^\circ\text{C}$  for binder (PVA) burn out. In order to study the chemical compatibility of the ceramic with Ag, the  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4 + 0.12 V_f \text{TiO}_2$  composite was further mixed with 20 wt% Ag powder ( $< 45 \mu\text{m}$ , 99.99+%, Sigma–Aldrich) and sintered at  $950^\circ\text{C}$  for 6 h. The bulk density of the sintered samples was measured using the Archimedes method and the sintering temperatures were optimized for maximum densification.

The crystal structure of the ceramics was studied by recording the X-ray diffraction (XRD) pattern of sintered and powdered samples using  $\text{Cu K}\alpha$  radiation (Philips X'Pert PRO MPD X-ray diffractometer; Philips, Almelo, The Netherlands). The surface morphology of the sintered and thermally etched samples was analyzed using a scanning electron microscope (SEM) (JOEL-JSM 5600 LV, Tokyo, Japan). The microwave dielectric properties were measured with a Vector Network Analyzer (Model No. E8362B; Agilent Technologies, Santa Clara, CA). The relative permittivity and the unloaded quality factor ( $Q_u$ ) of the samples were measured by Hakki–Coleman method modified by Courtney and cavity methods respectively.<sup>19</sup> The  $\tau_f$  was measured in the temperature range  $25$ – $70^\circ\text{C}$  by noting the temperature at regular intervals while heating and using the equation

$$\tau_f = \frac{f_2 - f_1}{f_1(T_2 - T_1)} \quad (1)$$

where  $f_1$  is the resonant frequency at temperature  $T_1$  and  $f_2$  at temperature  $T_2$ .

## 3. Results and discussion

Fig. 1 shows the variation of relative density with sintering temperature for the compositions with  $x = 0.1$  and  $1.0$ . The relative density increases with sintering temperature due to grain growth and removal of porosity and reaches a maximum value. Further increase in sintering temperature results in exaggerated grain growth and the relative density decreases as a consequence

of entrapped porosity.<sup>20</sup> For  $x=0.1$ , maximum relative density of 94.8% is obtained on sintering at 925 °C and for  $x=1.0$  the sample sintered at 825 °C shows the maximum relative density of 92%.

Fig. 2a–g shows the powder XRD patterns of  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ( $x=0.1$ –1.0) ceramics. The peaks corresponding to  $x=0.1$  are indexed using the standard JCPDS file for  $\text{LiMgPO}_4$  (file no: 32-0574) with orthorhombic structure and belonging to  $Pmn2_1$  space group. Similarly the peaks corresponding to the composition with  $x=1.0$  can be well indexed using the JCPDS file for  $\text{LiZnPO}_4$  (file no: 84-2136) with monoclinic structure and  $Cc$  space group. From Fig. 2, it is obvious that the compositions up to  $x=0.2$  form solid solutions having orthorhombic structure. However, for the compositions from  $x=0.3$  onwards, a new peak starts growing at  $2\theta \sim 22^\circ$  which corresponds to the major intensity peak of  $\text{LiZnPO}_4$ . As  $x$  increases, the peaks of the orthorhombic phase weaken and that of the monoclinic phase becomes stronger. For  $x=0.3$ –0.8, the ceramics exist as a mixture of orthorhombic and monoclinic phases and transform completely to monoclinic at  $x=1.0$

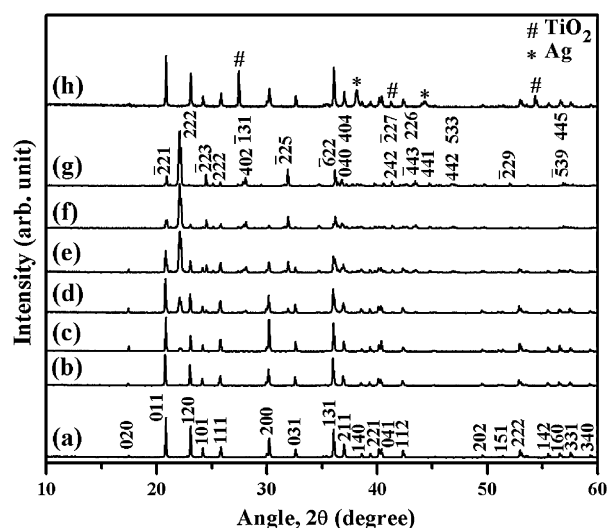


Fig. 2. Powder XRD patterns of  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ceramics with (a)  $x=0.1$ , (b)  $x=0.2$ , (c)  $x=0.3$ , (d)  $x=0.4$ , (e)  $x=0.6$ , (f)  $x=0.8$ , (g)  $x=1.0$  and (h)  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4 + 0.12 V_f \text{TiO}_2 + 20 \text{ wt\% Ag}$ .

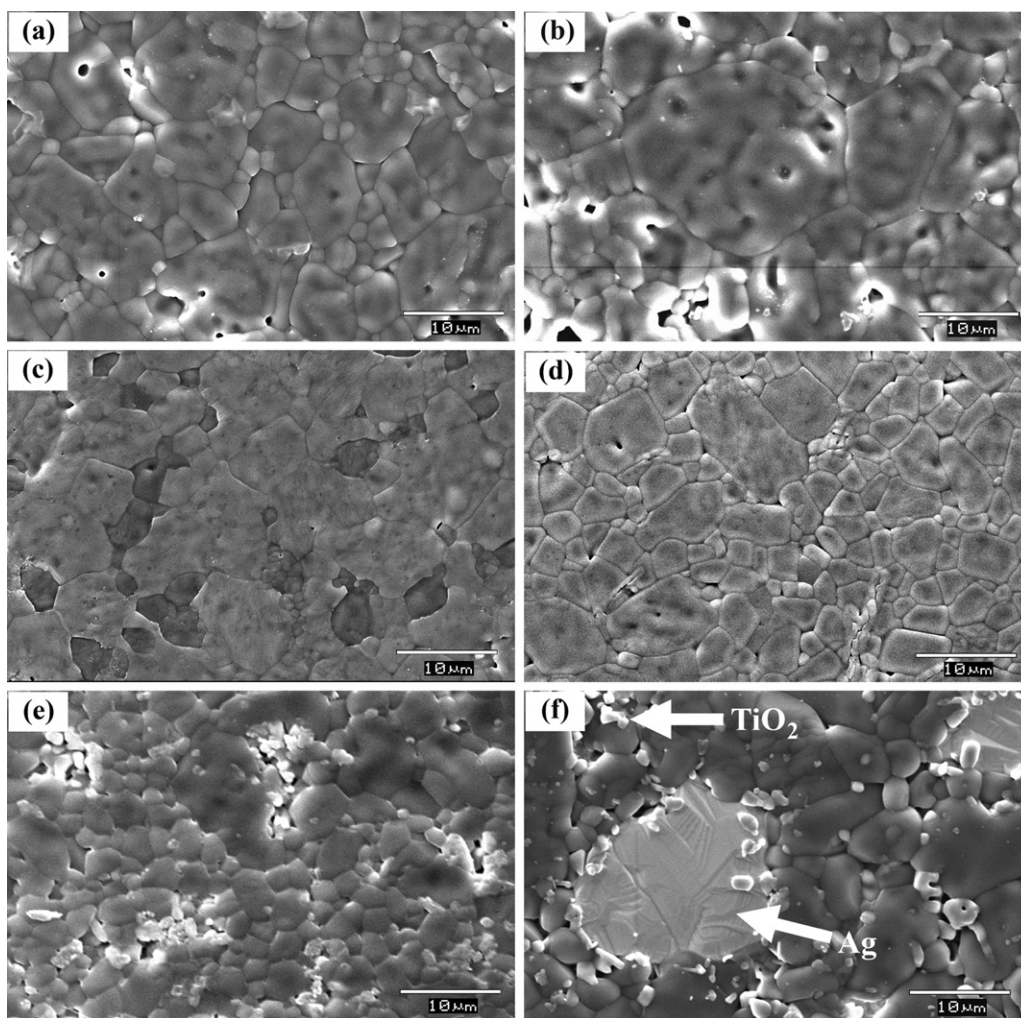


Fig. 3. SEM images of (a)  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  ( $x=0.1$ ) sintered at 925 °C for 4 h, (b)  $\text{LiMg}_{0.8}\text{Zn}_{0.2}\text{PO}_4$  ( $x=0.2$ ) sintered at 900 °C for 4 h, (c)  $\text{LiMg}_{0.2}\text{Zn}_{0.8}\text{PO}_4$  ( $x=0.8$ ) sintered at 850 °C for 4 h, (d)  $\text{LiZnPO}_4$  ( $x=1.0$ ) sintered at 825 °C for 4 h, (e)  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4 + 0.12 V_f \text{TiO}_2$  sintered at 950 °C for 4 h and (f)  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4 + 0.12 V_f \text{TiO}_2 + 20 \text{ wt\% Ag}$  sintered at 950 °C for 6 h.



(LiZnPO<sub>4</sub>). The powder XRD pattern of LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub> ( $x=0.1$ ) co-fired with 0.12 V<sub>f</sub> TiO<sub>2</sub> and 20 wt% Ag at 950 °C for 6 h is shown in Fig. 2h. The peaks corresponding to all the three phases can be well indexed using standard JCPDS files (file no: 21-1276 for TiO<sub>2</sub> and 04-0783 for Ag) and no additional peaks are present.

The SEM images of the sintered and thermally etched surfaces of the ceramics with  $x=0.1$ , 0.2, 0.8 and 1.0 are shown in Fig. 3a–d, respectively. The images reveal a microstructure containing grains of size randomly varying from  $\sim 1\ \mu\text{m}$  to  $>10\ \mu\text{m}$ . From the surface morphology of the composition with  $x=0.8$  (Fig. 3c) it is obvious that the ceramic is mixture of two phases. From Fig. 3d it can be observed that the grain boundaries of LiZnPO<sub>4</sub> are sharper. Fig. 3e shows the microstructure of LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub> co-fired with 0.12 V<sub>f</sub> TiO<sub>2</sub> at 950 °C for 4 h. Large grains of LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub> and small particles of TiO<sub>2</sub> can be observed in the image. The sintering temperature of TiO<sub>2</sub> is very high ( $\sim 1500\ ^\circ\text{C}$ ) and hence no substantial grain growth occurs for TiO<sub>2</sub> at 950 °C. The SEM image of the composite of LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub> with 0.12 V<sub>f</sub> TiO<sub>2</sub> and 20 wt% Ag sintered at 950 °C for 6 h is shown in Fig. 3f. In Fig. 3f, all the constituent phases can be separately identified which indicates that no significant reaction occurs between these phases.

The optimized sintering temperature ( $T_s$ ), bulk density and the dielectric properties at 1 MHz of the ceramics are given in Table 1. The sintering temperature decreases gradually from 950 °C to 825 °C as the value of  $x$  increases from 0.0 to 1.0. The relative densities of the compositions from  $x=0.3$  to  $x=0.8$  are not calculated as they are found to contain more than one phase. The relative permittivity at 1 MHz increases gradually from 7.1 at  $x=0$  to 7.4 at  $x=0.2$  and saturates up to  $x=0.4$ , then goes on decreasing from  $x=0.6$  onwards. The initial increase in  $\epsilon_r$  may be attributed to the large ionic polarizability of Zn<sup>2+</sup> ( $2.04\ \text{\AA}^3$ ) compared to Mg<sup>2+</sup> ( $1.32\ \text{\AA}^3$ )<sup>21</sup> and to the fact that Zn<sup>2+</sup> gets partially substituted for Mg<sup>2+</sup> in the orthorhombic lattice. However, as the value of  $x$  increases further the amount of monoclinic phase in the sample also increases and causes to reduce the value of  $\epsilon_r$ . Lowest value of 5.2 is obtained for  $\epsilon_r$  at  $x=1.0$  which is purely monoclinic in structure. The ceramics show very low dielectric loss ( $\tan\delta$ ) of the order of  $10^{-4}$  at 1 MHz (Table 1). It is also noteworthy that the compositions with  $x=0.1$  and 0.2 exhibit lowest dielectric loss ( $\tan\delta = 2 \times 10^{-4}$ ).

Fig. 4 depicts the microwave dielectric properties of LiMg<sub>(1-x)</sub>Zn<sub>x</sub>PO<sub>4</sub> ceramics. The values of  $\epsilon_r$  and  $Q_u \times f$  as a function of  $x$  are shown in Fig. 4a. The variation in  $\epsilon_r$  follows somewhat similar trend as that obtained at 1 MHz. The values of  $\epsilon_r$  obtained at microwave frequencies are slightly lower than that at 1 MHz. This may be due to the fact that some of the polarization mechanisms become inactive as the frequency increases from MHz to GHz range.<sup>22</sup> From Fig. 4a it can be observed that the quality factor ( $Q_u \times f$ ) increases from 79,100 GHz at  $x=0.0$  to 99,700 GHz at  $x=0.1$ . Some of the early reports show such an increase in  $Q_u \times f$  due to Zn<sup>2+</sup> substitution.<sup>23–25</sup> From  $x=0.2$  onwards  $Q_u \times f$  decreases gradually up to  $x=0.8$  and then increases for  $x=1.0$ . The value of  $Q_u \times f$  depends largely on the extrinsic factors like porosity and phase purity.<sup>26</sup> In the present study, the decrease in  $Q_u \times f$  as the value of  $x$  increases from 0.1

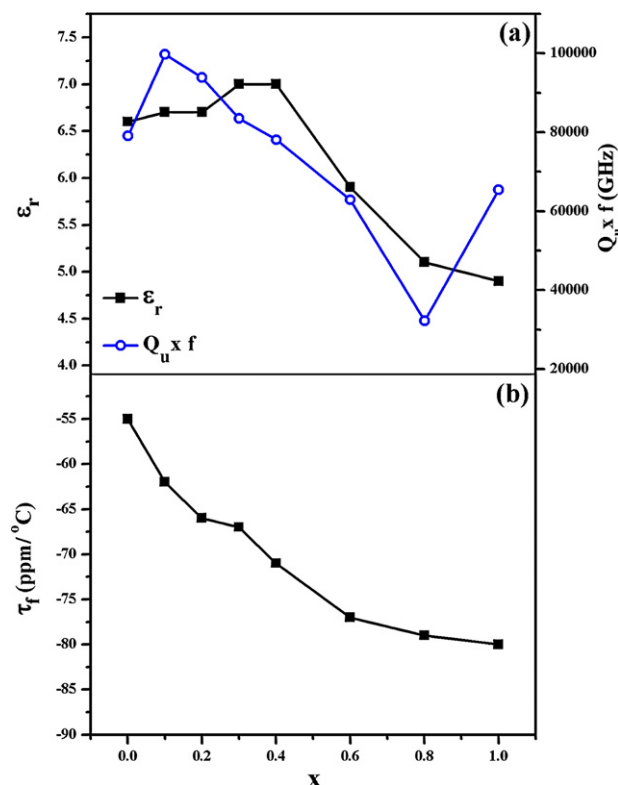


Fig. 4. Variation of (a)  $\epsilon_r$  and  $Q_u \times f$  and (b)  $\tau_f$  of LiMg<sub>(1-x)</sub>Zn<sub>x</sub>PO<sub>4</sub> ceramics with the value of  $x$ .

to 0.2 may be due to the decrease in relative density (Table 1). Further, as the value of  $x$  increases from 0.2 to 0.8, the amount of secondary phase (monoclinic phase) in the sample also increases which is evident from the XRD patterns as well as SEM images (Figs. 2 and 3) and this may be the reason for the decrease in  $Q_u \times f$  up to  $x=0.8$ . At  $x=1.0$ , the material becomes purely monoclinic LiZnPO<sub>4</sub> and hence  $Q_u \times f$  increases. Highest  $Q_u \times f$  of 99,700 GHz is obtained for  $x=0.1$  (LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub>) which is greatly appreciable for microwave applications. The variation of  $\tau_f$  with  $x$  is shown in Fig. 4b. The value of  $\tau_f$  increases steadily from  $-55\ \text{ppm}/^\circ\text{C}$  for  $x=0.0$  to  $-80\ \text{ppm}/^\circ\text{C}$  for  $x=1.0$ .

The ceramics developed in the present study have good microwave dielectric properties suitable for LTCC applications. The composition with  $x=0.1$  (LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub>) is interesting since it has very high quality factor ( $Q_u \times f = 99,700\ \text{GHz}$ ). However the temperature stability of resonant frequency is poor ( $\tau_f = -62\ \text{ppm}/^\circ\text{C}$ ) for practical applications. The value of  $\tau_f$  can be tuned nearly to zero by making composite with a suitable ceramic having large positive  $\tau_f$  like TiO<sub>2</sub> ( $\tau_f = +450\ \text{ppm}/^\circ\text{C}$ ). In the present study, rutile type TiO<sub>2</sub> is used since it has been reported more effective in improving the microwave dielectric properties compared to the anatase.<sup>27</sup> The microwave dielectric properties of LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub>–TiO<sub>2</sub> composites are given in Table 2. With the addition of TiO<sub>2</sub>, the sintering temperature increases slightly due to the high sintering temperature of TiO<sub>2</sub> ( $\approx 1500\ ^\circ\text{C}$ ). The sintering temperature for the composite with 0.15 V<sub>f</sub> TiO<sub>2</sub> is 975 °C which is not suitable for LTCC applications. On the other hand, composites containing up to 0.12 V<sub>f</sub> TiO<sub>2</sub> can be well sintered below the melting

Table 1

Sintering temperature, density and dielectric properties at 1 MHz of  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ceramics.

$x$	$T_s$ (°C)	Bulk density ( $\text{g cm}^{-3}$ )	Relative density (%)	$\epsilon_r$	$\tan \delta$
0.0	950	2.825	95.0	7.1	$7 \times 10^{-4}$
0.1	925	2.916	94.9	7.3	$2 \times 10^{-4}$
0.2	900	2.968	93.9	7.4	$2 \times 10^{-4}$
0.3	900	3.075	–	7.4	$6 \times 10^{-4}$
0.4	875	3.129	–	7.4	$7 \times 10^{-4}$
0.6	850	3.116	–	6.1	$7 \times 10^{-4}$
0.8	850	2.986	–	5.6	$9 \times 10^{-4}$
1.0	825	3.050	92.0	5.2	$7 \times 10^{-4}$

Table 2

Microwave dielectric properties of  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$ – $\text{TiO}_2$  composites.

Volume fraction of $\text{TiO}_2$	$T_s$ (°C)	Bulk density ( $\text{g cm}^{-3}$ )	Relative density (%)	$\epsilon_r$	$Q_u \times f$ (GHz)	Experimental $\tau_f$ (ppm/°C)	Calculated $\tau_f$ (ppm/°C)
0.00	925	2.916	94.9	6.7	99,700	–62	–62
0.05	925	3.009	96.0	8.2	80,200	–39	–36
0.10	950	3.051	95.6	9.5	69,500	–15	–11
0.12	950	3.072	95.5	10.1	52,900	–5	–1
0.15	975	3.097	95.3	11.7	49,800	17	15

point of Ag. From Table 2 it is clear that the relative densities of the composites are higher than the pure  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  ceramic. It has been reported earlier that  $\text{TiO}_2$  acts as a sintering aid to improve the sinterability of the ceramic co-fired with it.<sup>26</sup> The value of  $\epsilon_r$  increases with the volume fraction of  $\text{TiO}_2$  due to the large relative permittivity of  $\text{TiO}_2$  ( $\epsilon_r \approx 100$ ). The quality factor decreases gradually from 99,700 GHz for  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  to 49,800 GHz for the composite with 0.15  $V_f$   $\text{TiO}_2$ . The observed reduction in  $Q_u \times f$  may be mainly attributed to the low quality factor ( $Q_u \times f < 30,000$  GHz)<sup>28</sup> of  $\text{TiO}_2$  compared to  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$ . Inhomogeneity in mixing may also be deleterious to  $Q_u \times f$ . The value of  $\tau_f$  varies from –62 ppm/°C to +17 ppm/°C as the  $V_f$  of  $\text{TiO}_2$  increases from 0 to 0.15. The values of  $\tau_f$  for the composites can be theoretically calculated using the mixture rule<sup>29</sup>

$$\tau_{f \text{ mixture}} = V_{f1}\tau_{f1} + V_{f2}\tau_{f2} \quad (2)$$

where  $V_{f1}$  and  $V_{f2}$  are the volume fractions of  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  and  $\text{TiO}_2$  and  $\tau_{f1}$  and  $\tau_{f2}$  are their respective temperature coefficients of resonant frequency. The calculated values of  $\tau_f$  are given in Table 2. The experimentally observed values of  $\tau_f$  are found to be in agreement with the theoretical ones.  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  co-fired with 0.12  $V_f$   $\text{TiO}_2$  at 950 °C shows the best microwave dielectric properties with  $\epsilon_r = 10.1$ ,  $Q_u \times f = 52,900$  GHz and  $\tau_f = -5$  ppm/°C. The excellent microwave dielectric properties and the glass-free nature make this composition competitive with the commercially available LTCC substrates.<sup>1</sup>

#### 4. Conclusions

The effect of  $\text{Zn}^{2+}$  substitution on the microwave dielectric properties of  $\text{LiMg}_{(1-x)}\text{Zn}_x\text{PO}_4$  ( $x = 0.0$ – $1.0$ ) have been investigated. The compositions with  $x \geq 0.3$  show a mixture

of orthorhombic and monoclinic phases. As the value of  $x$  increases, the amount of monoclinic phase increases. At  $x = 1.0$ , the structure is completely transformed from orthorhombic to monoclinic.  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$  has  $\epsilon_r = 6.7$ ,  $Q_u \times f = 99,700$  GHz and  $\tau_f = -62$  ppm/°C. The  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$ – $\text{TiO}_2$  composite containing 0.12  $V_f$   $\text{TiO}_2$  has got good microwave dielectric properties with  $\epsilon_r = 10.1$ ,  $Q_u \times f = 52,900$  GHz and  $\tau_f = -5$  ppm/°C. The analysis of XRD pattern and microstructure reveals the chemical compatibility between the composite and the commonly used electrode material Ag. The excellent microwave dielectric properties of  $\text{LiMg}_{0.9}\text{Zn}_{0.1}\text{PO}_4$ – $\text{TiO}_2$  composite developed in the present study makes it a potential candidate for LTCC applications. The glass-free nature and low bulk density makes the composite more attractive.

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